

**BEFORE THE PUBLIC UTILITIES COMMISSION
OF THE STATE OF CALIFORNIA**

Order Instituting Rulemaking on the
Commission's Own Motion to Adopt New
Safety and Reliability Regulations for Natural
Gas Transmission and Distribution Pipelines
and Related Ratemaking Mechanisms

R.11-02-019
(Filed February 24, 2011)

**REQUEST FOR APPROVAL OF COMPLIANCE PLAN
AND SUPPLEMENT TO
REPORT OF PACIFIC GAS AND ELECTRIC COMPANY
ON RECORDS AND MAXIMUM ALLOWABLE
OPERATING PRESSURE VALIDATION**

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March 21, 2011

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At Pacific Gas and Electric Company (PG&E), safety is our highest responsibility. We empower our employees to take all appropriate actions to make our system safe and to help improve the safety of our operations at every stage.

Our approach to the Commission's January 3, 2011 directives to validate our gas transmission records and the MAOPs of our HCA pipelines reflects our commitment to safety. When we are done, we will exceed the scope called for by the Commission.

The March 16, 2011 letter from Executive Director Paul Clanon and the draft Order to Show Cause, however, made us realize that our March 15th report failed to communicate both our commitment to safety and, more importantly, the full extent of the work we have done and are continuing to do to assure the public and ourselves that our pipelines are operating at safe MAOPs. That work goes far beyond merely complying with the law. We have endorsed the Commission's efforts in this Rulemaking to eliminate the "grandfathering" of pipeline MAOPs, and we do so again. We hope that our words and our actions demonstrate to our customers, the Commission and the industry at large that there are workable alternatives to the current

“grandfathering” approach that, when implemented, will improve the safety of our natural gas pipelines.

This supplement is intended to clarify our prior filing by providing additional information about four subjects: (1) what we have done and where we are in the process of gathering all the records needed to validate the MAOPs of our HCA pipelines; (2) what we are still doing and how rapidly we will complete the remaining work validating the MAOPs of all our pipelines (not just HCA pipelines where the MAOP was not established by pressure testing), starting with those for which we do not have pressure test records; (3) what near-term actions to enhance public safety we are taking based on our records review; and (4) what longer-term actions to enhance public safety we are going to take.

Four elements of our plan deserve emphasis:

- This year we will hydro test or replace 152 miles of HCA pipe without pressure test records that are most similar to the San Bruno pipe.
- We are prioritizing for field action another 435 miles of HCA pipelines without pressure test records.
- We are empowering our engineers, as part of the MAOP validation process, to raise any safety concerns they identify for immediate action to reduce pressure, pressure test or replace pipe.
- At the end of the process, we will have validated the MAOP for all 1,805 miles of HCA pipelines, including those with pressure test records. We will follow that with a similar validation of the MAOP of the balance of our gas transmission system.

With the clarifications in this supplement to our March 15th report, we request the Commission to approve our plan for full compliance with the Commission's January 3, 2011 directives.

1. What we have done and where we are in the process

The first step in our records and MAOP validation process was, in the words of the Commission's directive, to "aggressively and diligently search" for all relevant records. We have approximately 1,805 miles of Class 3 and 4 locations and Class 1 and 2 HCA gas transmission pipeline included in this effort. The first step was intended to allow us to identify the HCA pipelines for which we have pressure test records so that we could start our further review and analysis, as the Commission directed, with those HCA pipelines where the MAOP was not set based on a pressure test.

Our original pipeline records are primarily contained in what we call job files. As the name implies, job files relate to specific jobs or work projects. Job files typically include pressure test reports and charts where available, pipeline as-built drawings, alignment sheets, other drawings and sketches, bills of materials, and other related records. Any given segment of pipe may have multiple job files, depending on how much work has been done on that segment from its original installation to the present. Conversely, a single job file may contain information about multiple segments.

Based on the information in our Geographical Information System, we initially identified about 2,800 master job folders with underlying job files. We generally maintain our job files in division field offices. A pipeline that traverses more than one division, as most of ours do, will have job files in more than one division office.

Our initial search for records began with our gas transmission office in Walnut Creek, our system-wide division offices and records storage centers, including our Bayshore records storage facility. The initial search included about 20 primary locations. The search soon grew to include additional storage areas in our San Francisco headquarters and a facility in Emeryville. Over the following weeks, our search continued to expand. A team of our mappers and third-party engineers traveled to approximately 50 locations, including some previously searched, where they interviewed personnel about records and went through file cabinets to search for gas transmission records. We wrote to more than 37,000 current and former employees and contractors in an effort to determine whether they had any relevant documents that were not in PG&E's possession. We followed up the letter to contractors with phone calls. Finally, for several days, we had over 1,500 employees from across the company working alternating shifts 24-hours a day at multiple locations, the most prominent of which was the Cow Palace, reviewing over 125,000 boxes of our historical records to see if there were relevant documents that were not appropriately indexed as such. We wanted to "leave no stone unturned."

We hired experts in document management, Iron Mountain and ADS, to scan and index the records collected. The complete contents of the relevant job files were scanned and loaded into an electronic system. Our IT organization developed a database, using our Enterprise Compliance Tracking System (ECTS), to store the scanned images for document review and data input. As of now, we have scanned and loaded more than 10,000 job files, comprised of about 1,250,000 documents (including duplicates).¹ The originals of the scanned documents were boxed, transported from the scanning locations for centralized storage in our Emeryville facility, where they were indexed and bar coded.

¹ The documents we provided to CPSD on DVDs supported the results reported on March 15th, but are a tiny fraction of the universe of documents we have collected and scanned.

Once scanned, the documents needed to be reviewed. To accomplish this, we needed both more physical space and more people. In addition to assigning existing space to this project, we leased 11,000 square feet of new office space in Walnut Creek and brought together a team of over 200 of our employees and contractor personnel to review the scanned documents. Our process included independent quality control. The results of our team's efforts to date and a sample of the documents they reviewed were set out in our March 15th report (pp. 6-14).

That report focused on a fraction of the 1.2 million documents we have collected and scanned because it primarily addressed the first part of the analysis to comply with the Commission's directive. That part was to determine what HCA pipeline miles had their MAOPs established based on "traceable, verifiable and complete" pressure test records. The priority for the engineering review to validate the MAOP, according to the Commission's directive, is the HCA pipelines that have not had their MAOP established based on pressure tests, so we had to define that universe.

As part of the analysis we submitted on March 15th, we also looked at and reported whether our records support the MAOPs of pipelines established by historical operating pressure, even though the Commission had not asked us to do so. We did not intend to rely on this analysis to comply with the Commission's directives. Rather, we did it for two reasons: (1) we wanted to provide added assurance that these MAOPs had been properly set on this basis while we complete the rest of the MAOP validation and the field work described in our report; and (2) as an added measure of safety, we plan to set the MAOPs of these lines at the **lower** of the MAOP derived from our engineering analysis and calculations **or** historical operating pressure. We failed, however, to convey either of these points in our original report.

At this stage of our work, we have collected and scanned over 1.2 million documents. These are the primary documents required to complete the MAOP validation described below. We estimate these records will provide about 70-80% of the information we need for the MAOP validation. The remaining information will come from inspection and maintenance records. These records, which we will be collecting as part of the MAOP validation, include A Forms, which may document the replacement of a small section of pipe or the installation of a sleeve; valve maintenance forms, which may provide supplemental information about valve type, manufacturer, make, ANSI strength; and station drawings, which may contain as-builts and other information about taps off the mainline pipe. We have started to collect these additional records and will continue to do so in the order required to complete the MAOP validation in the priority order we have established, as discussed below.

2. What we are still doing and how rapidly we will complete the remaining work

Our ongoing efforts are focused on validation of the MAOP based on engineering analysis not only of the mainline pipe but also of each component (*e.g.*, valves, sleeves, bends, fittings) to validate the MAOP of the overall pipeline based on its weakest component. At the same time, we are continuing to search for pressure test records and uprate documentation. Completing these records will not reduce the scope of our MAOP validation work, but will allow us to assign lower priorities to those segments where we find pressure test records or uprate documentation.

Although the Commission's directive was to do the MAOP validation only for pipelines where the MAOP was not established by a pressure test, we are not stopping there. Instead, as an added assurance of safety, we are performing the MAOP validation on the entire 1,805 miles of HCA pipelines. Once this is done, as we stated in our March 15th report (p. 13), we are going

to extend this analysis to our remaining Class 1 and 2 gas transmission pipelines – not because it is required, but because we view it as providing an added measure of safety for our system.

The MAOP validation process entails a more comprehensive examination of the records we have already collected and centralized. As mentioned before, our ECTS database includes all collected and scanned job files associated with the HCA lines. Not only do these files have the pressure documentation that was the primary focus of our analysis to date, they also contain records required to calculate MAOP. These include drawings (*e.g.*, construction, as-builts), construction material documentation (*e.g.*, bill of materials, material specifications), job estimate documentation, and pressure test-related documents.

The MAOP validation starts with us matching the collected and scanned documents with the HCA pipeline miles we are examining. This is a time-consuming process as pipeline reference points have changed over the years and the documents were not created with reference to specific HCA segments nor are they presently organized that way. Our contractor, Celerity, has the primary responsibility for this task, which is foundational to the entire MAOP validation.

The following are two examples of the scanned images of the as-built drawings:

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20855

2 OF 3 SHEETS
P.G. & F. CO.
 DRAWING NUMBER
 SP-0-131
 CHANGE

ITEM NO.	QTY	DESCRIPTION	REMARKS
7	1	FLANGE 16" A.S.A. WITH STEEL MOUNTING VARIOUS, T.E.P. 20" X 20" X 12" WELDING.	
8	3	TEES, 12" X 12" X 12" WELDING.	
9	2	TEES, 6" X 6" X 6" WELDING.	
10	1	REDUCER 16" X 12" WELDING.	
11	2	REDUCERS 12" X 8" WELDING.	
12	1	REDUCER 6" X 4" WELDING.	
13	1	ELBOW 12"-90° LONG RADIUS, WELDING.	
14	3	ELBOWS 6"-90° LONG RADIUS, WELDING.	
15	2	FLANGES, 1/6" LAP, F&D. SER. 30 W/STD. NIPPLE.	
16	1	FLANGE, 12" LAP, F&D. SER. 30 W/STD. NIPPLE.	
17	2	FLANGES, 6" LAP, F&D. SER. 60 W/STD. NIPPLE.	
18	6	FLANGES, 6" LAP, F&D. SER. 30 W/STD. NIPPLE.	
19	1	FLANGE, 4" LAP, F&D. SER. 30 W/STD. NIPPLE.	
20	1	SET 16" FLANGE INSULATION 300° A.S.A. MALONEY "F."	
21	1	GASKET, 12 3/8" X 16 5/8" X 1/8" RING, ASBESTOS.	
22	8	GASKETS, 6 3/8" X 9 7/8" X 1/8" RING, ASBESTOS.	
23	1	GASKET, 4 1/2" X 7 7/8" X 1/8" RING, ASBESTOS.	
24	96	BOLTS, 3/4" X 5 1/2" STUDS, W/2 HEX. NUTS.	
25	8	BOLTS, 3/4" X 4 1/2" STUDS, W/2 HEX. NUTS.	
26	20	BOLTS, 1/2" X 8 3/4" STUDS, W/2 HEX. NUTS.	
27	14 FT.	PIPE, 6" A.P.I. - 5 LX-GRADE "B", .280" WALL.	
28	13 FT.	PIPE, 12", SEAMLESS, .375" WALL.	
29	22 FT.	PIPE, 16" O.D. X .375" WALL.	
30	16	BOLTS, 1/2" X 7 1/2" STUDS, W/2 HEX. NUTS.	
			S.P. 2911 & G.M. 161804 DWG. S.P. 4-50 SH. 3 OF 12
E.M.M. 1061	31	1	VALVE, ROCKWELL, FIG. 4249 1/2, A.S.A. 300LBs, BUTT WELDING ENDS, ENDS OF VALVE BORED 23" I.D. LESS GEARING 24"
	32	1	EXTENSION FOR 24" VALVE, ROCKWELL #4249 1/2, A.S.A. 300LBs, ENTIRE MECHANISM (LESS GEARING) AS SHOWN IN SECTIONAL DWG. ON PAGE 66, CAT. # V. 101, DIM. "A" = 7'-6" MINUS DIMENSION OF WORM SHAFT TO TOP MOUNTING FLANGE OF SPOOL



ITEM	DESCRIPTION	QUAN	ITEM	DESCRIPTION	QUAN
REVOLVING STOCK			REVOLVING STOCK		
1	METER, 1" ENCO (specify)	1		Regulator (A) or (B) 3/4" orifice	1
	METER, 250B (specify)	1		Filter (C)	1
	METER, 500B (specify)	1		For primary regulator & relief valve see Dwg. 0489	
Account 1229			Account 1230		
1	Valve, 1" Nerd. #113 Ser. 15	1		A. 2" H or HPH Regulator	
2	Cock, 2" Mueller, #H-11100	1		Flange, Lap. 1" Ser. 15	1
3	Cock, 1-1/4" Mueller, #H-11100	1		Flange, Weld Neck 2" Ser. 15	1
4	Gasket, Ring 1" Ser. 15	3	26	Nipple, Std. 1/4" X 6"	2
5	Nipple, Std. 1/4" X 6"	3	29	Reducer, Welding 1/2" X 2"	1
6	Nipple, Std. 1-1/4" X 5"	1	30	Flange, Steel 5/8" X 3" w/nuts	0
7	Nipple, Std. 2" X 6"	1	31	Bolts, Steel 5/8" X 2-1/2" w/nuts	4
8	Nipple, Std. 1/2" X 1 1/2" (250B) (H Doco)	1	32	Gasket, Ring 2" Ser. 15	1
9	Nipple, Std. 1/2" X 1 1/2" (250B)	1	33	Elbow, Street 1/2" 90° (HPH)	1
10	Caps, Pipe 2"	2	34	Elbow, Street 1" 90° (H)	1
11	Caps, Pipe 1 1/4"	6	35	E. 2" ENCO "1001" Regulator	
12	Plug, Pipe 1-1/4"	1	36	Flange, Weld Neck 2" Ser. 15	1
13	Plug, Pipe 2"	1		Flange, Lap. 1" Ser. 15	1
14	Pipe, Bare Steel 1-1/4" Ft.	5		Reducer, Weld. 1" X 2"	0
15	Foundation Block 20"x30"x3"	on hand	37	Flange, Weld Neck 2" Ser. 15	1
16			38	Flange, Lap. 1" Ser. 15	1
17	Bolts, Steel 5/8" X 3" w/nuts	16	39	Reducer, Weld. 1" X 2"	0
18	Flange, Lap. 1" Ser. 15	1	40	Bolts, Steel 5/8" X 3" w/nuts	4
19	Flange, Weld Neck 1" Ser. 15	2	41	Bolts, Steel 5/8" X 2-1/2" w/nuts	4
20	Plate, Steel (16" X 17" X 1/4") for 250B & 1" flow	1	42	Tee, Screwed 1/4"	1
Account 1228			43	Elbow, Screwed 1/4" 90°	1
BLANKET W.O. FOR APPROPRIATE SERVICE SIZE			44	Nipple, Std. 1/4" X 3"	1
21	Elbow, Welding 2" 90°	1	45	Nipple, Std. 2" X 6"	2
22	Flange, Weld Neck 2" Ser. 15	1	46	Gasket, Ring 2" Ser. 15	1
23	Bolts, Steel 5/8" X 3" w/nuts	4	47	C. 2" Staynew Filter GWP 150#	
24	Gasket, Insulating 2" Ser. 15 w/sleeves & washers (MS 20172)	1 set		Bolts, Steel 5/8" X 2-1/2" w/nuts	4
25	Nipple, Std. 2" X 12"	1		Gasket, Ring 2" Ser. 15	1
26	Reducer, Weld. 2" specify	1			
27	MUeller H-11175 MUELLER H-11175 CODE 03-6191	1		Note: Maximum working pressure of Mueller cocks 50#	
JOB LOCATION <u>RAWSON KILN CORP. OLIVE RD. 5/0 RED BLVD</u>					
EST. NO. <u>30422</u> W.O. or O.M. _____					
APPROVED BY		DESCRIPTION		DATE	
		1-15-62 Chge Items 2 - 3		1-15-62	
		Change accounts, revise drawing			
SUPERV BY		DESCRIPTION		DATE	
DSGN. <u>sch</u>		<u>1" ENCO, 250 & 500 B</u>		<u>1-15-62</u>	
CH. _____		Meter Reg. Set			
O.K. _____		Max. Working Pressure 50 Lb. - Max. Outlet Press 150			
DATE	SCALE	PACIFIC GAS AND ELECTRIC COMPANY		DRAWING LIST	
8-7-62	3/4"=1'	Gas Dept. SAN FRANCISCO, CALIFORNIA Shasta Div.		SUPERSEDED BY	
				SHEET NO. 2 OF 2 SHEETS	
				DRAWING NUMBER	
				1052	
				CHANGE	
				2	

The calculation of MAOP requires knowledge of detailed attributes of the pipeline and its components. These attributes include the following:

- project data
 - mile point
 - field stationing
 - pipe stationing
 - project stationing
 - class location
 - design factor
 - year installed
- pipe data
 - length
 - wall thickness
 - grade
 - seam type
 - coating type
- sleeve data
 - type
 - length
- tap data
 - size
 - type
 - insertion
- bend data
 - type
 - radius
 - angle
 - wall thickness
 - orientation
 - spacing
- tee data
 - branch size
 - wall thickness
 - barred
- valve data
 - type
 - full port
- casing data
 - size
 - length
- reducer data
 - type
 - length
 - size

The following slides, taken from the training materials for our MAOP validation team, illustrate what is involved in extracting the information from the existing records. Where the data are not explicitly listed on the source documents, the MAOP validation team needs to

calculate the information from what is available (e.g., using a protractor to estimate the degree of bend where not specified on the drawing).

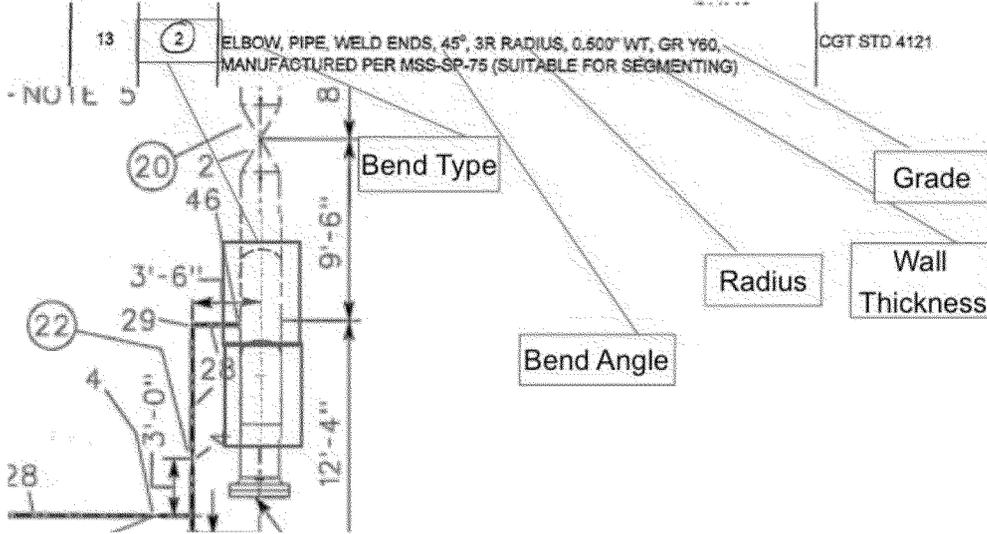


Project Data from Sources

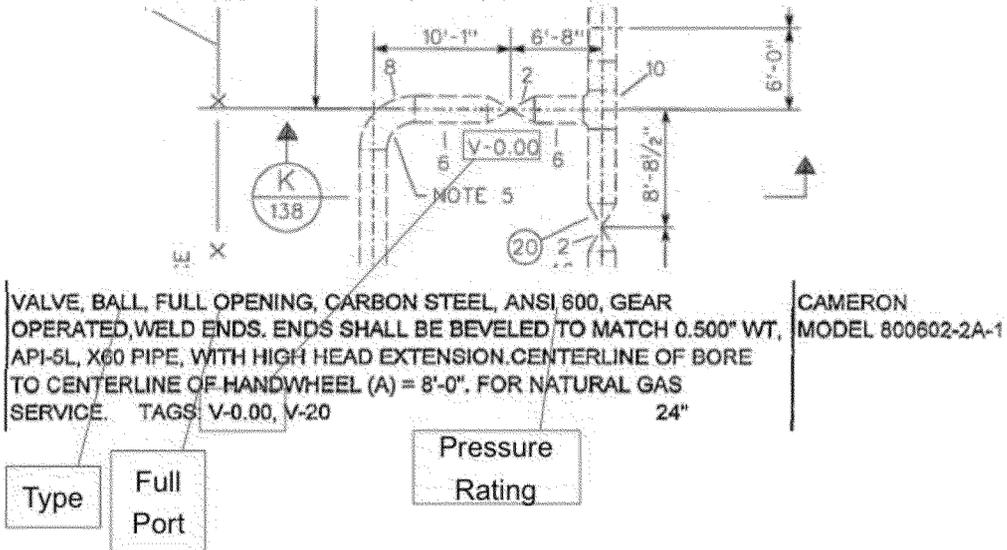
B/M ITEM NO.	6
DESIGN CRITERIA	
LOCATION CLASS	1
DESIGN FACTOR	0.5
D.P.	1040 x SMYS 4160
MAOP	1040 x SMYS 4160
STRENGTH TEST PRESSURE	
MAX.	1760 PSIG 70.40 x SMYS
MIN.	1560 PSIG 62.40 x SMYS
	2250 PSIG-90% SMYS
TEST FLUID WATER	
PIPE SPEC API-5L, X-60 DSAW	
O.D.	24.00"
W.T.	0.500"
WELD INSPECTION (GAS STD.D-40)	
<input checked="" type="checkbox"/> RADIOGRAPHIC	<input type="checkbox"/> 20% MIN.
	<input checked="" type="checkbox"/> 100%
*VISUALLY INSPECT 100% OF ALL WELDS NOT RADIOGRAPHICALLY INSPECTED (APPLIES EVEN IF NO RADIOGRAPHIC INSPECTION IS REQUIRED).	



Determine Bend Type

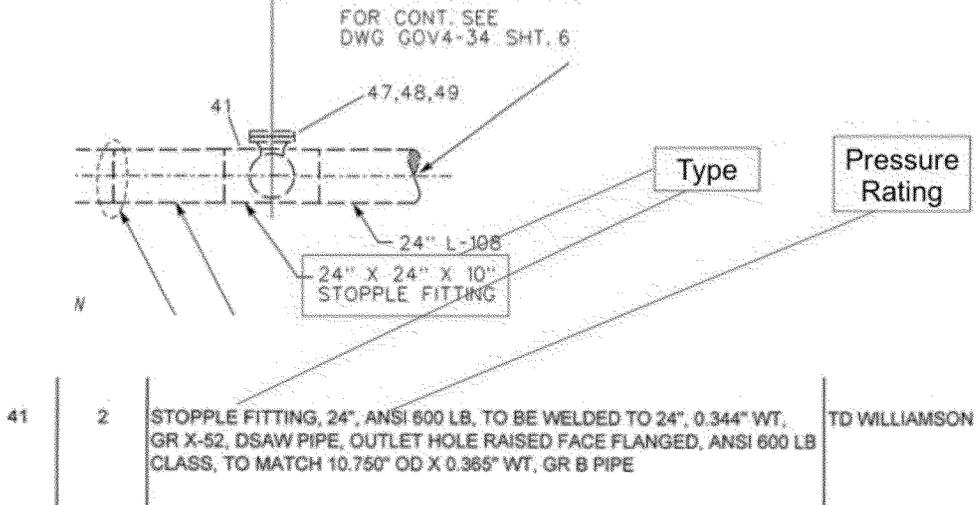


Determine the Valve Attributes





Determine the PCF Attributes



Typically, the information needed to calculate the MAOP comes from as-built drawings, bills of materials, and other related documentation from the job files. In addition to all the job files already collected and scanned, we may have to review additional non-HCA transmission line and selected distribution job files to accurately account for all pipeline features within a given segment boundary. We are also reviewing pipeline inspection and operations records to ensure all potentially relevant documents are included in the analysis. To the extent these documents are not currently in our ECTS database, we will perform additional document searches from our newly-established centralized gas transmission records repository in Emeryville and elsewhere across our system as needed.

Our “grandfathered” pipelines were constructed 40 or more years ago. For many of these pipelines, we do not believe we will find “traceable, verifiable and complete” records of every component. Instead, we are making assumptions about certain components, such as fittings and elbows, based on the material specifications at the time those materials were procured, sound

engineering judgment, and conducting excavation and field testing of pipeline systems as appropriate. We will determine what field testing to use on a case-by-case basis from such techniques as X-ray or camera inspection of welds and measuring yield strength using Advanced Technology Corporation's Automated Ball Indentation technique.

Such field testing also goes beyond what the Commission's directives call upon us to do to validate the MAOP of our pipelines. Again, however, our objective is safety, and we believe that such field testing provides an additional measure of confidence in our MAOPs.

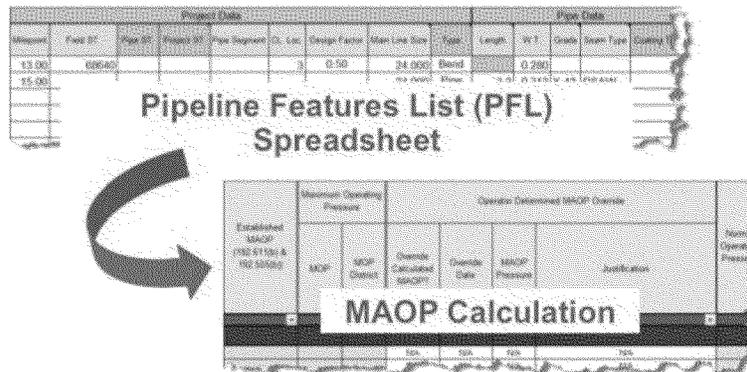
The information from the document review, engineering analysis and field-testing gets compiled into a document known as a pipeline features list (PFL). Based on the recent effort on our Peninsula gas transmission lines, we estimate it will take 50 to 60 person-hours (or more) per mile to build each PFL (this does not include the time to collect, scan, assemble the source documents needed for PFL build, oversight, field work, the MAOP calculation, or quality assurance). Extrapolating from this experience, building the PFLs for the 1,805 HCA miles we are validating will take about 100,000 person-hours or 12,500 person-days.

The completed PFLs feed directly into the engineering calculation of the MAOP:



PFL Spreadsheet to MAOP Calculation

“...determine the valid maximum allowable operating pressure, based on the weakest section of the pipeline or component to ensure safe operation...”



To perform the calculation of the MAOP based upon the weakest component, we plan to use a proprietary MAOP calculation tool developed by a third-party gas pipeline engineering firm that specializes in MAOP calculations.

To help ensure the quality of data obtained from this effort, we are continuing a separate quality assurance (QA) team to review the defined processes and the output from our work. As we move further into the MAOP validation effort, the QA team will build on the knowledge that the team has already gained about our data systems, gas transmission records practices, and the relevant document types. The quality assurance review will be tracked and reported. If the QA testing produces any “failures” (specific errors), the QA team will ensure that the information is passed along to the appropriate team members and documented. To the extent the quality assurance team believes it is necessary to ensure quality for the ongoing production process, we will implement process changes.

As this description shows, we have designed and are implementing a rigorous process to use engineering analysis to calculate the MAOP of our pipelines based on the weakest component. The following table shows how we have prioritized our MAOP validation work and the schedule on which we expect to complete it this year:

Priority	Description	Miles	Planned Completion
1	Pipe similar in specification to that involved in the San Bruno incident, or similar to the way in which it was recorded <ul style="list-style-type: none"> • DSAW; and 24-36" outside diameter; and installed prior to 1962 • Seamless; and >24" outside diameter; and installed prior to 1974 	152 ²	Q2 2011
2	Certain other seams and joint efficiencies <ul style="list-style-type: none"> • ERW, SSAW, Flash and Lap Welded and all pipe with Joint Efficiency < 1; and installed prior to 1970 	295	Q2-Q3 2011
3	All remaining 619(c) documented pipe and pipe installed prior to 7/1/1970 with records still under review	206	Q3 2011
4	All pipe installed after 7/1/1970 with records still under review	52	Q3 2011
5	All remaining pipe with partial pressure test records and pressure test records from the 1968 CPUC Filing	83	Q3 2011
6	Pipe with verified pressure test documentation, but where the STPR footage tested does not equal the pipeline HCA footage	270	Q3 2011
7	Pipe with verified pressure test documentation	748	Q3-Q4 2011
TOTAL		1,805*	

* Figures do not sum due to rounding.

We believe this schedule, while aggressive, is realistic. We have completed this process for the 375-psig MOP sections of the three Peninsula pipelines, Lines 101, 109 and 132. We did

² Although we have prioritized this pipe for the MAOP validation, we are still going ahead with hydro testing or replacement this year, as discussed further below.

the validation of the approximately 135 miles of Peninsula pipelines in about 45 days with 25 people (not counting personnel involved in the field work). Based on that experience, we believe we can complete the remaining HCA miles by year-end with 100 to 125 people (again, not including personnel needed for field work).

We currently have 50 members of this team on board. Thirty of them have completed training for the MAOP validation, and the remaining 20 are being trained Monday and Tuesday of this week. These 50 individuals – from PG&E’s ranks and three contractors, Exponent, Celerity and Gas Transmission Services – will be fully engaged in the MAOP validation by mid-week. The 50 are the first half of the team of over 100 engineers, estimators, and mappers (from contracting firms and from our own gas engineering group) we are assembling to review all the collected documentation and extract the necessary data to complete the PFLs. This is an extremely detailed and painstaking process requiring forensic analysis of all relevant documents associated with a pipeline to identify the location, characteristics and qualities of all pipeline components that are part of the existing pipeline configuration. To do it right, we must use people with specialized skills in pipeline engineering, construction, and mapping. We then train them carefully and thoroughly so they are able to determine the necessary information from different sources dating back 60 or more years, and to ensure a standardized process and methodology with appropriate controls is followed by all personnel throughout the project. To secure the additional 50-75 team members, we are actively looking at third party contractors to supplement these resources and are in discussions with third parties who may have the capacity to provide turnkey PFL builds.

We attach a copy of the PFL completed for Line 101 (Attachment 1) as well as the draft MAOP validation report for Line 101 and Line 132-A (Attachment 2) that we shared with the

Commission's staff two days after we received the January 3, 2011 directive. The PFL and draft report provide concrete illustrations of the application of our process to validate the pipeline MAOP through the records review and supplemental field investigation.

If our MAOP validation work identifies any safety concerns or we encounter any pipeline segments for which we cannot validate the MAOP as planned, we will take immediate action. These actions may include one or more of the following: pressure reduction, pressure testing or replacement of the section of pipe in question.

We will provide the Commission monthly reports on the progress of our MAOP validation work.

3. What near-term actions we are taking based on our records review

As described in our March 15th report (pp. 14-17), this year we are going to hydro test or replace 152 miles of HCA pipelines based on the results of our record review to date. These 152 miles – 699 pipeline segments – meet the following criteria: (1) we have not located pressure test records and (2) our records indicate the segments contain either: (a) pre-1962 24 to 36 inch double submerged arc welded (DSAW) pipe or (b) pre-1974 seamless pipe greater than 24 inches in diameter. We selected these criteria for this year's field actions because they are most similar to the ruptured segment of Line 132.

Even though, as described above, we expect to complete the MAOP validation of these pipeline segments based on our records review and limited field work in the second quarter of this year, we are not satisfied with that level of MAOP validation. We want to provide added assurance of the safety of these pipelines by hydro testing or replacing them. And, we will do that this year. In fact, the contracting, engineering planning, and permit application preparation for this work are already under way.

Because the miles of each pipeline segment are not contiguous and are not always located near valves, our work will extend over more than 250 miles on 24 separate pipelines, as detailed on page 16 of our March 15th report.

4. What longer-term actions we are going to take

Beyond this work, we have prioritized for further physical assessment approximately 435 miles of HCA pipelines for which we have not yet located pressure test records and that meet the following criteria (in priority order): 1) pipelines containing low frequency electric resistance weld (ERW), single-submerged arc weld (SSAW), lap weld or flash pipe installed prior to 1970; 2) pipelines installed prior to 1970; and 3) pipelines installed after 1970.³

As described in more detail in our March 15th filing (pp. 17-19), our field action program on these additional miles of HCA pipelines will be based on further analysis of, and tailored to the unique characteristics of each pipeline. These actions will include one or more of the following: in-line inspections with so-called “smart pigs” equipped with special “crack” tools capable of examining weld seams; pressure testing; use of other emerging technologies, such as advanced camera inspection; and/or pipe replacement.⁴

As we committed in our report, we will work with state and local government agencies and officials, emergency responders and customers in the areas where we intend to perform these field actions, and will submit periodic progress reports to the Commission updating our progress and the latest schedule of field actions.

³ Priorities 2 – 4 of our MAOP validation, as set out in the table on page 16, are similar to but broader than these categories because the MAOP priorities include pipe with pressure test records.

⁴ See Kiefner & Associates, Inc., “The Benefits and Limitations of Hydrostatic Testing” by J. Kiefner and W. Maxey, pp 5-6. <http://www.kiefner.com/downloads/apihydro.pdf>.

Conclusion

We hope this supplement has clarified both our commitment to safety beyond requirements and our intent to exceed the scope of the Commission's January 3, 2011 directives. While we wish we could have completed all this work by now, the fact is that the magnitude of the task is enormous. We have dedicated and continue to dedicate resources commensurate with the task and are proceeding as quickly as we can. We ask the Commission to approve our plan for full compliance with its directives.

We look forward to continuing to work with the Commission and other stakeholders to enhance the safety of our natural gas transmission system and to adopt new, higher safety standards applicable to all pipelines.

Respectfully submitted,

/s/ Jonathan D. Pendleton

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March 21, 2011

Attachment 1

DRAFT L-101 MP 0.00 - 33.79 PIPELINE FEATURES LIST
Privileged and Confidential

Project Data				Pipe Data				Sleeve Data				Tap Data				Bend Data				Tee Data				Valve Data				Casing Data				Reducer Data				Date Data				
Ident Number	Milepost	Pipe Segment	C. Use	Design Factor	Main Line Size	Type	Length	WT	Grade	Beam Type	Coating Type	Type	WT	Grade	Length	Size	Type	Radius	Angle	WT	Grade	Orient	branch Size	WT	Grade	Beam	Type	Full Port	Size	Length	Reducer Size	Length	WT	Grade	Size	Year Installed	Job Number	Unit Factor		
53			3	0.50	36.0000	Bend																														1/1/1965	162548	1.0		
54			3	0.50	36.0000	Tap																														1/1/1965	162548	1.0		
55			3	0.50	36.0000	Bend																													1/1/1965	162548	1.0			
56			3	0.50	36.0000	Reducer																													1/1/1965	162548	1.0			
437	14.9600	132	3	0.50	20.0000	Pipe	1466	0.312	X-42	DSAW	HAA																								1/1/1965	131961	1.0			
58			3	0.50	34.0000	Bend																													1/1/1965	162548	1.0			
459	15.6963	136	3	0.50	20.0000	Pipe	2646	0.312	X-42	SMLS	HAA																								1/1/1967	138865	1.0			
60			3	0.50	34.0000	Bend																													1/1/1967	137560	1.0			
61	2.4700	104.6C	3	0.50	34.0000	Casing																													1/1/1967	137560	1.0			
479	16.0574	137.5	3	0.50	20.0000	Pipe	25	0.312	X-42	SMLS	TAPE																								1/1/1967	138865	1.0			
63			3	0.50	34.0000	Bend																													1/1/1965	160041	1.0			
480	16.8670	137.8	3	0.50	20.0000	Pipe	88	0.312	X-42	SMLS	HAA																								1/1/1967	138865	1.0			
491	16.8823	139	3	0.50	20.0000	Pipe	845	0.312	X-42	SMLS	HAA																								1/1/1967	138865	1.0			
66			3	0.50	34.0000	Reducer																														1/1/1965	156741	1.0		
59	2.4500	104.6	3	0.50	34.0000	Pipe	204	0.344	X-52	DSAW	HAA																								1/1/1967	137560	1.0			
68			3	0.50	34.0000	Reducer																														1/1/1965	156741	1.0		
64	2.4500	105.2	3	0.50	34.0000	Pipe	120	0.344	X-52	DSAW	HAA																								1/1/1967	137560	1.0			
70	2.5400	106.4	3	0.50	34.0000	Pipe	225	0.375	X-46	DSAW	HAA																								1/1/1967	137560	1.0			
71			3	0.50	36.0000	Reducer																													1/1/1965	160041	1.0			
112	3.3900	111.6	1	0.72	34.0000	Pipe	430	0.375	X-46	DSAW	HAA																									1/1/1967	137560	1.0		
74			3	0.50	34.0000	Bend																														1/1/1965	160041	1.0		
75			3	0.50	36.0000	Bend																														1/1/1965	160041	1.0		
240.2	10.4000	118	3	0.50	30.0000	Pipe	600	0.312	X-42	DSAW	HAA																								1/1/1969	143347	1.0			
76.2			3	0.50	36.0000	Sleeve						Type B	UNK	UNK	12"	36"																			1/1/1965	160041	1.0			
316	12.4000	123	3	0.50	20.0000	Pipe	280	0.312	GRB	SMLS	TAPE																								1/1/1969	144674	1.0			
78			3	0.50	36.0000	Bend																													1/1/1965	156741	1.0			
79			3	0.50	36.0000	Bend																													1/1/1965	156741	1.0			
80			3	0.50	36.0000	Bend																													1/1/1965	156741	1.0			
81			3	0.50	36.0000	Bend																													1/1/1965	156741	1.0			
321	12.4495	123.2	3	0.50	20.0000	Pipe	918	0.312	GRB	SMLS	TAPE																								1/1/1969	144674	1.0			
83			1	0.72	36.0000	Bend																													1/1/1965	162548	1.0			
84			1	0.72	36.0000	Bend																													1/1/1965	162548	1.0			
332	12.6120	123.4	3	0.50	20.0000	Pipe	215	0.312	GRB	SMLS	TAPE																								1/1/1969	144674	1.0			
86		108.5C	1	0.72	36.0000	Casing																													1/1/1965	162548	1.0			
1129	31.3600	185	4	0.40	20.0000	Pipe	3194	0.312	X-42	DSAW	HAA																								1/1/1969	145815	1.0			
88			1	0.72	36.0000	Tap																													1/1/1965	162548	1.0			
89	3.0400	109.4C	1	0.72	36.0000	Casing		0.438																										42	144	1/1/1965	162548	1.0		
90			1	0.72	36.0000	Bend																													1/1/1965	162548	1.0			
90.1			1	0.72	36.0000	Tap																													2	Inneci	No	1/1/1990	4835203	1.0
1136	31.9500	186	4	0.40	20.0000	Pipe	1090	0.312	X-42	DSAW	HAA																								1/1/1969	145815	1.0			
92			3	0.50	36.0000	Reducer																														1/1/1990	4835203	1.0		
92.1			3	0.50	36.0000	Bend																														1/1/1990	4835203	1.0		
93			3	0.50	36.0000	Bend																														1/1/1990	4835203	1.0		
94	16.0091	136.3	3	0.50	20.0000	Pipe	41	0.312	X-42	DSAW	HAA																									1/1/1990	148791	1.0		
95			3	0.50	30.0000	Bend																														1/1/1990	4835203	1.0		
96			3	0.50	30.0000	Bend																														1/1/1990	4835203	1.0		
97			3	0.50	30.0000	Bend																														1/1/1990	4835203	1.0		
98		</																																						

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Project Data				Pipe Data				Sleeve Data				Tap Data				Bend Data				Tee Data				Valve Data				Casing Data				Reducer Data				Date Data			
Ident. Number	Milepost	Pipe Segment	Cl. Use	Design Factor	Mean Line Size	Type	Length	WT.	Grade	Beam Type	Coating Type	Type	WT.	Grade	Length	Size	Type	Radius	Angle	WT.	Grade	Chart	Branch Size	WT.	Grade	Barrel	Type	Full Port	Size	Length	Reducer Size	Length	WT.	Grade	Size	Year Installed	Job Number	Joint Factor	
162			1	0.72	36.0000	Casing																														1/1/1965	162548	1.0	
163			1	0.72	36.0000	Casing																														1/1/1965	162548	1.0	
164			1	0.72	36.0000	Bend																														1/1/1965	162548	1.0	
165			1	0.72	36.0000	Bend																														1/1/1965	162548	1.0	
166			1	0.72	36.0000	Tap																														1/1/1965	162548	1.0	
42.2	0.8509	103.2	3	0.50	36.0000	Pipe	1245	0.350	X-52	DSAW	HAA																								1/1/1965	162548	1.0		
168			3	0.50	36.0000	Bend																														1/1/1965	162548	1.0	
169			3	0.50	36.0000	Bend																														1/1/1965	162548	1.0	
170			3	0.50	36.0000	Bend																														1/1/1965	162548	1.0	
170.1			3	0.50	36.0000	Tap																														1/1/1965	162548	1.0	
48	1.0000	103.5	3	0.50	36.0000	Pipe	5280	0.350	X-52	DSAW	HAA																									1/1/1965	162548	1.0	
172			3	0.50	36.0000	Bend																														1/1/1965	162548	1.0	
52	2.0000	104	3	0.50	36.0000	Pipe	2398	0.350	X-52	DSAW	HAA																									1/1/1965	162548	1.0	
174			1	0.72	36.0000	Bend																														1/1/1965	162548	1.0	
175			1	0.72	36.0000	Bend																														1/1/1965	162548	1.0	
176			1	0.72	36.0000	Bend																														1/1/1965	162548	1.0	
177			1	0.72	36.0000	Bend																														1/1/1965	162548	1.0	
178			1	0.72	36.0000	Bend																														1/1/1965	162548	1.0	
178.1			1	0.72	36.0000	Bend																														1/1/1965	162548	1.0	
179	7.8600		1	0.72	36.0000	Tap																														1/1/1965	162548	1.0	
180			1	0.72	36.0000	Bend																														1/1/1965	162548	1.0	
57	2.4500	104.3	3	0.50	36.0000	Pipe	2	0.500	X-52	DSAW	HAA																									1/1/1965	162548	1.0	
182			3	0.50	36.0000	Pipe	528	0.350	X-52	DSAW	HAA																									1/1/1965	162548	1.0	
183			1	0.72	36.0000	Bend																														1/1/1965	162548	1.0	
184			1	0.72	36.0000	Bend																														1/1/1965	162548	1.0	
185			1	0.72	36.0000	Bend																														1/1/1965	162548	1.0	
186			1	0.72	36.0000	Bend																														1/1/1965	162548	1.0	
187			1	0.72	36.0000	Casing																														1/1/1965	162548	1.0	
82	2.7100	108	3	0.50	36.0000	Pipe	396	0.350	X-52	DSAW	HAA																									1/1/1965	162548	1.0	
189			1	0.72	36.0000	Bend																															1/1/1965	162548	1.0
190			1	0.72	36.0000	Bend																															1/1/1965	162548	1.0
86	2.7775	108.5	1	0.72	36.0000	Pipe	1176	0.350	X-52	DSAW	HAA																									1/1/1965	162548	1.0	
87	3.0000	109.4	1	0.72	36.0000	Pipe	528	0.350	X-52	DSAW	HAA																									1/1/1965	162548	1.0	
193			3	0.50	36.0000	Tap																														1/1/1965	162548	1.0	
193.1			3	0.50	36.0000	Bend																														1/1/1965	162548	1.0	
193.2			3	0.50	36.0000	Bend																														1/1/1965	162548	1.0	
127	3.5300	112	1	0.72	36.0000	Pipe	3693	0.350	X-52	DSAW	HAA																									1/1/1965	162548	1.0	
134	4.3108	112.09	1	0.72	36.0000	Pipe	483	0.350	X-52	DSAW	HAA																									1/1/1965	162548	1.0	
135	4.4128	112.1	1	0.72	36.0000	Pipe	216	0.350	X-52	DSAW	HAA																									1/1/1965	162548	1.0	
136	4.4589	112.2	3	0.50	36.0000	Pipe	2559	0.350	X-52	DSAW	HAA																									1/1/1965	162548	1.0	
198	9.5400		1	0.72	36.0000	Tap																														1/1/1965	162548	1.0	
198.1			1	0.72	36.0000	Bend																														1/1/1965	162548	1.0	
198			1	0.72	36.0000	Bend																														1/1/1965	162548	1.0	
200			1	0.72	36.0000	Bend																														1/1/1965	162548	1.0	
200.1			1	0.72	36.0000	Bend																														1/1/1965	162548	1.0	
201			1	0.72	36.0000	Bend																														1/1/1965	162548	1.0	
140	5.0000	112.3	3	0.50	36.0000	Pipe	198	0.350	X-52	DSAW	HAA																									1/1/1965	162548	1.0	
203			1	0.72	36.0000	Tap																														1/1/1965	162548	1.0	
203.1			1	0.72	36.0000	Tap																														1/1/1965	162548	1.0	
141.1		112.4	3	0.50	36.0000	Pipe	4	0.500	X-52	DSAW	Unknown																									1/1/1965	162548	1.0	
160.1		112.5	1	0.72	36.0000	Pipe	13	0.500	X-52	DSAW	Unknown																									1/1/1965	162548	1.0	
205			1	0.72	36.0000	Bend																														1/1/1965	162548	1.0	
151.1		112.6	1	0.72	36.0000	Pipe	8	0.500	X-52	DSAW	Unknown																									1/1/1965	162548	1.0	
207			1	0.72	36.0000	Tee																														1/1/1965	162548	1.0	
207.1			1	0.72	36.0000	Tap																														1/1/1965	162548	1.0	
208			1	0.72	36.0000	Tee																														1/1/1965	162548	1.0	
152.1	5.0300	113																																					

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Project Data				Pipe Data				Sleeve Data				Tap Data				Bend Data				Tee Data				Valve Data				Casing Data				Reducer Data				Date Data								
Line Number	Milepoint	Pipe Segment	GI Use	Design Factor	Main Line Size	Type	Length	WT	Grade	Beam Type	Coating Type	Type	WT	Grade	Length	Size	Type	Radius	Angle	WT	Grade	Orient	Branch Size	WT	Grade	Beam	Type	Full Port	Size	Length	Reducer Size	Length	WT	Grade	Size	Year Installed	Job Number	Joint Factor						
377			3	0.50	24.0000	Bend												Forged	5 D (L)	90	0.375	X-60	Right															10/23/2001	7039567	1.0				
1169	33.4200	167.6	3	0.50	30.0000	Pipe	100	0.312	X-52	DSAW	TAPE																											1/1/1970	456043	1.0				
383			3	0.50	24.0000	Bend												Forged	5 D (L)	45	0.375	X-60	Left																1/1/1966	1947340	1.0			
384			3	0.50	24.0000	Bend												Forged	5 D (L)	45	0.375	X-60	Left																1/1/1966	1947340	1.0			
385			3	0.50	24.0000	Bend												Forged	5 D (L)	30	0.375	X-60	Combo																1/1/1966	1947340	1.0			
386			3	0.50	24.0000	Bend												Forged	5 D (L)	48	0.375	X-60	OB																	1/1/1966	1947340	1.0		
387			3	0.50	24.0000	Bend												Forged	5 D (L)	4	0.375	X-60	Sag																	1/1/1966	1947340	1.0		
388			3	0.50	24.0000	Bend												Forged	5 D (L)	6	0.375	X-60	Sag																	1/1/1966	1947340	1.0		
389			3	0.50	24.0000	Bend												Miter	Other	3	0.312	X-60	Combo																	1/1/1966	1947340	1.0		
1176	33.4400	167.9	3	0.50	20.0000	Pipe	3	0.312	X-52	DSAW	TAPE																											1/1/1970	456043	1.0				
391			3	0.50	24.0000	Bend												Forged	5 D (L)	5	0.375	X-60	Sag																	1/1/1966	1947340	1.0		
392			3	0.50	24.0000	Bend												Forged	5 D (L)	11	0.375	X-60	Right																		1/1/1966	1947340	1.0	
393			3	0.50	24.0000	Bend												Forged	5 D (L)	11	0.375	X-60	Right																		1/1/1966	1947340	1.0	
394			3	0.50	24.0000	Bend												Forged	5 D (L)	4	0.375	X-60	Sag																		1/1/1966	1947340	1.0	
495	16.6200	139.6	3	0.50	20.0000	Pipe	2	0.375	GRB	SMLS	XTRUPL																											1/1/1985	1937188	1.0				
396			3	0.50	24.0000	Bend												Forged	5 D (L)	89	0.375	X-60	Left																		1/1/1966	1947340	1.0	
397	14.1388	127.3C	3	0.50	24.0000	Casing																																	1/1/1966	196774	1.0			
497	16.8300	140	3	0.50	24.0000	Pipe	15584	0.375	X-60	DSAW	XTRUPL																												1/1/1985	1937188	1.0			
399			3	0.50	24.0000	Bend												Forged	5 D (L)	50	0.375	X-60	Combo																		1/1/1966	1947340	1.0	
400			3	0.50	24.0000	Bend												Forged	5 D (L)	28	0.375	X-60	Right																		1/1/1966	1947340	1.0	
401			3	0.50	24.0000	Bend												Forged	5 D (L)	90	0.375	X-60	Right																		1/1/1966	1947340	1.0	
572	18.6800	140.3	3	0.50	34.0000	Pipe	5	0.380	X-60	DSAW	XTRUPL																												1/1/1985	1937188	1.0			
403			3	0.50	24.0000	Tap												B	Innecation																				1/1/1966	1947340	1.0			
404			3	0.50	24.0000	Tap												B	ake-off																				1/1/1966	1947340	1.0			
405			3	0.50	24.0000	Tap												1	Innecation																					1/1/1966	1947340	1.0		
406			3	0.50	24.0000	Valve																						Ball	Yes											1/1/1966	1947340	1.0		
407			3	0.50	24.0000	Tap												1	Innecation																					1/1/1966	1947340	1.0		
408			3	0.50	24.0000	Tap												B	ake-off																					1/1/1966	1947340	1.0		
409			3	0.50	24.0000	Tap												B	Innecation																					1/1/1966	1947340	1.0		
1007	28.8300	161.9	3	0.50	20.0000	Pipe	9	0.375	X-52	DSAW	TAPE																												1/1/1966	1941186	1.0			
1009	28.8300	163	3	0.50	24.0000	Pipe	8482	0.375	X-60	DSAW	TAPE																													1/1/1966	1941186	1.0		
414			3	0.50	20.0000	Bend												Forged	5 D (L)	90	0.375	X-60	Right																	1/1/1987	4565099	1.0		
417			3	0.50	20.0000	Bend												Forged	5 D (L)	90	0.375	X-60	Left																		1/1/1987	4565099	1.0	
418			3	0.50	20.0000	Reducer																																		1/1/1967	4565099	1.0		
1042	30.4100	163.5	3	0.50	24.0000	Pipe	5789	0.375	X-60	DSAW	TAPE																													1/1/1966	1941186	1.0		
1116	31.1600	164	4	0.40	24.0000	Pipe	1152	0.375	X-60	DSAW	TAPE																													1/1/1966	1941186	1.0		
421.1			3	0.50	20.0000	Bend												Forged	5 D (L)	UNK	0.375	GRB	OB																		1/1/1955	131961	1.0	
421.2			3	0.50	20.0000	Bend												Forged	5 D (L)	UNK	0.375	GRB	Sag																		1/1/1955	131961	1.0	
421.3			3	0.50	20.0000	Bend												Forged	5 D (L)	UNK	0.375	GRB	OB																		1/1/1955	131961	1.0	
421.4			3	0.50	20.0000	Bend												Forged	5 D (L)	90	0.375	GRB	Right																			1/1/1955	131961	1.0
422			3	0.50	20.0000	Bend												Forged	5 D (L)	65	0.375	GRB	Left																			1/1/1955	131961	1.0
422.1			3	0.50	20.0000	Bend												Forged	5 D (L)	UNK	0.375	GRB	OB			</																		

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Project Data				Pipe Data				Sleeve Data				Tap Data				Bend Data				Toe Data			Valve Data			Casing Data			Reducer Data			Date Data									
Ident Number	Milepost	Pipe Segment	CL Use	Design Factor	Min Line Size	Type	Length	WT	Grade	Beam Type	Coating Type	Type	WT	Grade	Length	Size	Type	Radius	Angle	WT	Grade	Orient	branch size	WT	Grade	Beam	Type	Full Port	Size	Length	Reducer Size	Length	WT	Grade	Size	Year Installed	Job Number	Joint Factor			
429				3	0.50	24.0000	Bend											Forged	D (LL	12	0.375	X-60	Left													1/1/1989	4701553	1.0			
430				3	0.50	24.0000	Bend											Forged	S D (LL	12	0.375	X-60	Left														1/1/1989	4701553	1.0		
431				3	0.50	24.0000	Bend											Forged	S D (LL	12	0.375	X-60	Left															1/1/1989	4701553	1.0	
432				3	0.50	24.0000	Bend											Forged	S D (LL	45	0.375	X-60	Right															1/1/1989	4701553	1.0	
433				3	0.50	24.0000	Bend											Forged	S D (LL	50	0.375	X-60	Left																1/1/1989	4701553	1.0
434				3	0.50	24.0000	Reducer																															1/1/1989	4701553	1.0	
1145		166.1		3	0.50	20.0000	Pipe	2	0.312	X-52	DSAW	HAA																									1/1/1986	1941186	1.0		
1146	32.1685	166.3		3	0.50	20.0000	Pipe	9	0.312	X-52	DSAW	TAPE																										1/1/1986	1941186	1.0	
438				3	0.50	20.0000	Tap									3.5	take-off																					1/1/1955	131961	1.0	
438.1				3	0.50	20.0000	Bend											Forged	S D (LL	UNK	0.375	GRB	OB															1/1/1955	131961	1.0	
438.2				3	0.50	20.0000	Bend											Forged	S D (LL	UNK	0.375	GRB	Sag																1/1/1955	131961	1.0
438.3				3	0.50	20.0000	Bend											Forged	S D (LL	UNK	0.375	GRB	Unknown																1/1/1955	131961	1.0
438.4				3	0.50	20.0000	Tap									3	injection																						1/1/1955	131961	1.0
438.5				3	0.50	20.0000	Tap									4	injection																						1/1/1955	131961	1.0
438.6				3	0.50	20.0000	Bend											Forged	S D (LL	UNK	0.375	GRB	OB																1/1/1955	131961	1.0
438.7				3	0.50	20.0000	Bend											Forged	S D (LL	UNK	0.375	GRB	Unknown																1/1/1955	131961	1.0
438.8				3	0.50	20.0000	Bend											Forged	S D (LL	UNK	0.375	GRB	OB																1/1/1955	131961	1.0
1147		166.4		3	0.50	20.0000	Pipe	13	0.375	X-52	DSAW	Unknown																										1/1/1986	1941186	1.0	
440				3	0.50	20.0000	Reducer																															1/1/1989	4701553	1.0	
845	24.7300	151.3		3	0.50	20.0000	Pipe	5	0.375	X-52	DSAW	TAPE																										1/1/1986	1944834	1.0	
442				3	0.50	24.0000	Bend											Forged	S D (LL	45	0.375	X-60	Left																1/1/1989	4701553	1.0
443				3	0.50	24.0000	Bend											Forged	S D (LL	45	0.375	X-60	Right																1/1/1989	4701553	1.0
727	22.7800	148.3		3	0.50	24.0000	Pipe	16	0.312	X-60	DSAW	TAPE																										1/1/1986	1944834	1.0	
733	22.7900	148.6		3	0.50	24.0000	Pipe	23	0.312	X-60	DSAW	TAPE																										1/1/1986	1944834	1.0	
445.1				3	0.50	24.0000	Bend											Forged	S D (LL	UNK	0.375	X-60	Left															1/1/1989	4701553	1.0	
445.2				3	0.50	24.0000	Bend											Forged	S D (LL	UNK	0.375	X-60	Right															1/1/1989	4701553	1.0	
736	22.7900	147		3	0.50	24.0000	Pipe	1482	0.312	X-60	DSAW	TAPE																										1/1/1986	1944834	1.0	
447				3	0.50	24.0000	Tap									8	injection																						1/1/1989	4701553	1.0
448				3	0.50	24.0000	Tap									8	take-off																						1/1/1989	4701553	1.0
449				3	0.50	24.0000	Tap									1	injection																						1/1/1989	4701553	1.0
450				3	0.50	24.0000	Valve																															1/1/1989	4701553	1.0	
451				3	0.50	24.0000	Tap									1	injection																						1/1/1989	4701553	1.0
452				3	0.50	24.0000	Tap									8	take-off																						1/1/1989	4701553	1.0
453				3	0.50	24.0000	Tap									8	injection																						1/1/1989	4701553	1.0
768	23.1400	147.6		3	0.50	24.0000	Pipe	112	0.312	X-60	DSAW	TAPE																										1/1/1986	1944834	1.0	
454.1				3	0.50	24.0000	Bend											Forged	S D (LL	45	0.375	X-60	Right															1/1/1989	4701553	1.0	
454.2				3	0.50	24.0000	Bend											Forged	S D (LL	45	0.375	X-60	Left															1/1/1989	4701553	1.0	
455				3	0.50	24.0000	Bend											Forged	S D (LL	45	0.375	X-60	Right																1/1/1989	4701553	1.0
456				3	0.50	24.0000	Bend											Forged	S D (LL	45	0.375	X-60	Left																1/1/1989	4701553	1.0
764	23.1600	149		3	0.50	24.0000	Pipe	4660	0.312	X-60	DSAW	TAPE																										1/1/1986	1944834	1.0	
458				3	0.50	20.0000	Reducer																															1/1/1989	4701553	1.0	
796	24.0500	150		3	0.50	24.0000	Pipe	601	0.375	X-60	DSAW	TAPE																										1/1/1986	1944834	1.0	
462				3	0.50	20.0000	Bend											Forged	S D (LL	45	0.375	GRB	Combo															1/1/1957	136865	1.0	
463				3	0.50	20.0000	Bend											Forged	S D (LL	45	0.375	GRB	Combo																1/1/1957	136865	1.0
464				3	0.50	20.0000	Bend											Forged	S D (LL	45	0.375	GRB	Combo																1/1/1957	136865	1.0
465				3	0.50	20.0000	Bend											Forged	S D (LL	45	0.375	GRB	Combo																1/1/1957	136865	1.0
465.1				3	0.50	20.0000	Bend											Forged	S D (LL	UNK	0.375	GRB	Left																1/1/1957	136865	1.0
465.2				3	0.50	20.0000	Bend											Forged	S D (LL	UNK	0.375	GRB	Right																1/1/1957	136865	1.0
466				3	0.50	20.0000	Bend											Forged	S D (LL	45	0.375	GRB	Left																1/1/1957	136865	1.0
467				3	0.50	20.0000	Bend											Forged	S D (LL	45	0.375	GRB	Right																1/1/1957	136865	1.0
468	16.6496	136C		3	0.50	20.0000	Casing																															1/1/1957	136865	1.0	
469				3	0.50	20.0000	Bend																																		

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Project Data				Pipe Data				Sleeve Data				Tap Data				Bend Data				Tree Data				Valve Data				Cleaning Data				Reducer Data				Date Data						
Line Number	Milepost	Pipe Segment	C. Loc.	Design Factor	Min Line Size	Type	Length	W.T.	Grade	Beam Type	Coating Type	Type	W.T.	Grade	Length	Size	Type	Isobore	Radius	Angle	W.T.	Grade	Draw	Branch Size	W.T.	Grade	Barrel	Type	Full Port	Size	Length	Reducer Size	Length	W.T.	Grade	Size	Year Installed	Job Number	User Factor			
523			3	0.50	24.0000	Bend																																	1/1/1985	1937168	1.0	
524	18.5900	140.1C	3	0.50	24.0000	Casing																																	1/1/1985	1937168	1.0	
526			3	0.50	24.0000	Bend																																	1/1/1985	1937168	1.0	
528			3	0.50	24.0000	Bend																																	1/1/1985	1937168	1.0	
527			3	0.50	24.0000	Bend																																	1/1/1985	1937168	1.0	
528			3	0.50	24.0000	Bend																																	1/1/1985	1937168	1.0	
528.1			3	0.50	24.0000	Bend																																	1/1/1985	1937168	1.0	
529			3	0.50	24.0000	Bend																																	1/1/1985	1937168	1.0	
530			3	0.50	24.0000	Bend																																	1/1/1985	1937168	1.0	
531			3	0.50	24.0000	Bend																																	1/1/1985	1937168	1.0	
532			3	0.50	24.0000	Bend																																	1/1/1985	1937168	1.0	
533	18.8900	140.2C	3	0.50	24.0000	Casing																																	1/1/1985	1937168	1.0	
534			3	0.50	24.0000	Bend																																	1/1/1985	1937168	1.0	
536			3	0.50	24.0000	Bend																																	1/1/1985	1937168	1.0	
537			3	0.50	24.0000	Bend																																	1/1/1985	1937168	1.0	
538			3	0.50	24.0000	Bend																																	1/1/1985	1937168	1.0	
539			3	0.50	24.0000	Bend																																	1/1/1985	1937168	1.0	
540			3	0.50	24.0000	Bend																																	1/1/1985	1937168	1.0	
541			3	0.50	24.0000	Bend																																	1/1/1985	1937168	1.0	
542			3	0.50	24.0000	Bend																																	1/1/1985	1937168	1.0	
543			3	0.50	24.0000	Bend																																	1/1/1985	1937168	1.0	
544			3	0.50	24.0000	Bend																																	1/1/1985	1937168	1.0	
545			3	0.50	24.0000	Bend																																	1/1/1985	1937168	1.0	
546			3	0.50	24.0000	Bend																																	1/1/1985	1937168	1.0	
547		140.3C	3	0.50	24.0000	Casing																																	1/1/1985	1937168	1.0	
548			3	0.50	24.0000	Bend																																	1/1/1985	1937168	1.0	
549			3	0.50	24.0000	Bend																																	1/1/1985	1937168	1.0	
550			3	0.50	24.0000	Tap																																	1/1/1985	1937168	1.0	
551			3	0.50	24.0000	Valve																																		1/1/1985	1937168	1.0
552			3	0.50	24.0000	Tap																																		1/1/1985	1937168	1.0
553			3	0.50	24.0000	Bend																																	1/1/1985	1937168	1.0	
554			3	0.50	24.0000	Bend																																	1/1/1985	1937168	1.0	
555			3	0.50	24.0000	Bend																																	1/1/1985	1937168	1.0	
556			3	0.50	24.0000	Bend																																	1/1/1985	1937168	1.0	
557			3	0.50	24.0000	Tap																																	1/1/1985	1937168	1.0	
558			3	0.50	24.0000	Bend																																	1/1/1985	1937168	1.0	
559			3	0.50	24.0000	Bend																																	1/1/1985	1937168	1.0	
560			3	0.50	24.0000	Bend																																	1/1/1985	1937168	1.0	
561			3	0.50	24.0000	Bend																																	1/1/1985	1937168	1.0	
562			3	0.50	24.0000	Bend																																	1/1/1985	1937168	1.0	
563			3	0.50	24.0000	Bend																																	1/1/1985	1937168	1.0	
564			3	0.50	24.0000	Bend																																	1/1/1985	1937168	1.0	
565			3	0.50	24.0000	Bend																																	1/1/1985	1937168	1.0	
566			3	0.50	24.0000	Bend																																	1/1/1985	1937168	1.0	
567			3	0.50	24.0000	Bend																																	1/1/1985	1937168	1.0	
568			3	0.50	24.0000	Bend																																	1/1/1985	1937168	1.0	
569			3	0.50	24.0000	Bend																																	1/1/1985	1937168	1.0	
570			3	0.50	24.0000	Bend																																	1/1/1985	1937168	1.0	
571			3	0.50	24.0000	Reducer																																	1/1/1985	1937168	1.0	
410	14.2400	128.2	3	0.50	24.0000	Pipe	20	0.312	X-60	DSAW	XTRUPL																											1/1/1986	1947340	1.0		
653	21.5200	143.3	3	0.50	24.0000	Pipe	91	0.312	X-60	DSAW	XTRUPL																											1/1/1988	1947977	1.0		
655	21.5400	143.6	3	0.50	24.0000	Pipe	7	0.312	X-60	DSAW	XTRUPL																											1/1/1988	1947977	1.0		
574			3	0.50	34.0000	Reducer																																1/1/1988	1949668	1.0		
659	21.5450	143.8	3	0.50	24.0000	Pipe	7	0.312	X-60	DSAW	XTRUPL																											1/1/1988	1947977	1.0		
662	21.5500	144	3	0.50	24.0000	Pipe	2492																																			

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Project Data					Pipe Data				Sleeve Data				Tap Data				Bend Data				Tee Data			Valve Data			Casing Data			Reducer Data			Date Data																	
Item Number	Milepost	Pipe Segment	C.I. Use	Design Factor	Min Line Size	Type	Length	WT	Grade	Seam Type	Coating Type	Type	WT	Grade	Length	Size	Type	Isobore	Type	Radius	Angle	WT	Grade	Orient	Branch Size	WT	Grade	Barrel	Type	Full Port	Size	Length	Reducer Size	Length	WT	Grade	Size	Year Installed	Job Number	User Factor										
633				3	0.50	24.0000	Bend													Forged	D (LL)	45	0.375	X-60	Sag																1/1/1987	1949668	1.0							
634				3	0.50	24.0000	Bend													Forged	D (LL)	45	0.375	X-60	Sag																	1/1/1987	1949668	1.0						
635				3	0.50	24.0000	Bend													Forged	D (LL)	45	0.375	X-60	OB																		1/1/1987	1949668	1.0					
636				3	0.50	24.0000	Bend													Forged	D (LL)	45	0.375	X-60	unknown																			1/1/1987	1949668	1.0				
637				3	0.50	24.0000	Bend													Forged	D (LL)	45	0.375	X-60	unknown																				1/1/1987	1949668	1.0			
638				3	0.50	24.0000	Bend													Forged	D (LL)	45	0.375	X-60	OB																				1/1/1987	1949668	1.0			
639				3	0.50	24.0000	Bend													Forged	D (LL)	45	0.375	X-60	Sag																					1/1/1987	1949668	1.0		
640	21.1500	143.12C		3	0.50	24.0000	Casing																												30	38									1/1/1988	1949668	1.0			
641				3	0.50	24.0000	Bend														Forged	D (LL)	45	0.375	X-60	Sag																				1/1/1987	1949668	1.0		
642				3	0.50	24.0000	Bend														Forged	D (LL)	45	0.375	X-60	OB																				1/1/1987	1949668	1.0		
643				3	0.50	24.0000	Bend														Forged	D (LL)	45	0.375	X-60	OB																				1/1/1987	1949668	1.0		
644				3	0.50	24.0000	Bend														Forged	D (LL)	45	0.375	X-60	Sag																					1/1/1987	1949668	1.0	
645				3	0.50	24.0000	Bend														Forged	D (LL)	45	0.375	X-60	Sag																					1/1/1987	1949668	1.0	
646				3	0.50	24.0000	Bend														Forged	D (LL)	45	0.375	X-60	OB																					1/1/1987	1949668	1.0	
852	24.8900	152.6		3	0.50	24.0000	Pipe	66	0.312	X-60	DSAW	TAPE																																		1/1/1988	1947993	1.0		
648				3	0.50	24.0000	Bend														Forged	D (LL)	45	0.375	X-60	OB																					1/1/1987	1949668	1.0	
649				3	0.50	24.0000	Bend														Forged	D (LL)	45	0.375	X-60	Sag																					1/1/1987	1949668	1.0	
650	21.5000	143.21C		3	0.50	24.0000	Casing																													30	55									1/1/1987	1949668	1.0		
651				3	0.50	24.0000	Bend														Forged	D (LL)	45	0.375	X-60	Sag																					1/1/1987	1949668	1.0	
652				3	0.50	24.0000	Bend														Forged	D (LL)	45	0.375	X-60	OB																					1/1/1987	1949668	1.0	
655	24.9000	153		3	0.50	24.0000	Pipe	3229	0.312	X-60	DSAW	TAPE																																			1/1/1988	1947993	1.0	
654				3	0.50	24.0000	Tap													8	take-off	No																									1/1/1988	1947977	1.0	
854	25.5100	154		3	0.50	24.0000	Pipe	6211	0.312	X-60	DSAW	TAPE								8	in-natch	No																									1/1/1988	1947993	1.0	
656				3	0.50	24.0000	Tap													8	in-natch	No																									1/1/1988	1947977	1.0	
657				3	0.50	24.0000	Tee																				24	0.375	Unknown	No																		1/1/1988	1947977	1.0
658				3	0.50	24.0000	Valve																																								1/1/1988	1947977	1.0	
901	26.7200	154.3		3	0.50	24.0000	Pipe	45	0.312	X-52	DSAW	TAPE																																		1/1/1988	1947993	1.0		
660				3	0.50	24.0000	Tee																				24	0.375	Unknown	No																		1/1/1988	1947977	1.0
661				3	0.50	24.0000	Tap													8	in-natch	No																									1/1/1988	1947977	1.0	
972	28.2500	158.3		3	0.50	20.0000	Pipe	4	0.375	X-52	DSAW	TAPE																																			1/1/1988	1947993	1.0	
663				3	0.50	24.0000	Bend														Forged	D (LL)	43	0.375	X-60	Sag																					1/1/1988	1947977	1.0	
664				3	0.50	24.0000	Bend														Forged	D (LL)	22	0.375	X-60	OB																					1/1/1988	1947977	1.0	
665				3	0.50	24.0000	Bend														Forged	D (LL)	90	0.375	X-60	Combo																						1/1/1988	1947977	1.0
666				3	0.50	24.0000	Bend														Forged	D (LL)	45	0.375	X-60	Combo																						1/1/1988	1947977	1.0
667				3	0.50	24.0000	Bend														Forged	D (LL)	45	0.375	X-60	Combo																					1/1/1988	1947977	1.0	
668	21.7100	144C		3	0.50	24.0000	Casing																														30	151									1/1/1987	1947977	1.0	
669				3	0.50	24.0000	Bend														Forged	D (LL)	22	0.375	X-60	OB																					1/1/1987	1947977	1.0	
670				3	0.50	24.0000	Bend														Forged	D (LL)	22	0.375	X-60	Sag																					1/1/1987	1947977	1.0	
671				3	0.50	24.0000	Bend														Forged	D (LL)	22	0.375	X-60	Sag																					1/1/1987	1947977	1.0	
672				3	0.50	24.0000	Bend														Forged	D (LL)	22	0.375	X-60	OB																					1/1/1987	1947977	1.0	
673				3	0.50	24.0000	Bend														Forged	D (LL)	22	0.375	X-60	OB																					1/1/1987	1947977	1.0	
674				3	0.50	24.0000	Bend														Forged	D (LL)	22	0.375	X-60	Sag																					1/1/1987	1947977	1.0	
675				3	0.50	24.0000	Bend														Forged	D (LL)	22	0.375	X-60	Sag																					1/1/1987	1947977	1.0	
676				3	0.50	24.0000	Bend														Forged	D (LL)	22	0.375	X-60	OB																					1/1/1987	1947977	1.0	
677				3	0.50	24.0000	Tap														Forged	D (LL)	22	0.375	X-60	OB																								

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Project Data				Pipe Data				Sleeve Data				Tap Data				Bend Data				Tee Data				Valve Data				Casing Data				Reducer Data				Date Data									
Isent Number	Milepost	Pipe Segment	Cl. Loc.	Design Factor	Main Line Size	Type	Length	WT	Grade	Beam Type	Coating Type	Type	WT	Grade	Length	Size	Type	Isent No.	Type	Radius	Angle	WT	Grade	Orient	Branch Size	WT	Grade	Beam	Type	Full Port	Size	Length	Reducer Size	Length	WT	Grade	Size	Year Installed	Job Number	User Factor					
690			3	0.50	24.0000	Bend													Forged	D (L)	45	0.375	X-60	Sag															1/1/1965	1947907	1.0				
691			3	0.50	24.0000	Bend													Forged	D (L)	45	0.375	X-60	Sag																1/1/1965	1947907	1.0			
692			3	0.50	24.0000	Bend													Forged	D (L)	90	0.375	X-60	Combo																	1/1/1965	1947907	1.0		
886	28.2600	158.9	3	0.50	24.0000	Pipe	6	0.312	X-60	DSAW	TAPE																													1/1/1968	1947993	1.0			
694			3	0.50	24.0000	Bend													Forged	S (L)	22.5	0.375	X-60	OB																	1/1/1967	1947977	1.0		
695			3	0.50	24.0000	Bend													Forged	S (L)	45	0.375	X-60	Sag																	1/1/1967	1947977	1.0		
696			3	0.50	24.0000	Bend													Forged	S (L)	22.5	0.375	X-60	OB																		1/1/1967	1947977	1.0	
697			3	0.50	24.0000	Bend													Forged	S (L)	45	0.375	X-60	Combo																		1/1/1967	1947977	1.0	
698			3	0.50	24.0000	Bend													Forged	S (L)	45	0.375	X-60	Combo																		1/1/1967	1947977	1.0	
699			3	0.50	24.0000	Bend													Forged	S (L)	22.5	0.375	X-60	OB																		1/1/1967	1947977	1.0	
700			3	0.50	24.0000	Bend													Forged	S (L)	45	0.375	X-60	Sag																		1/1/1967	1947977	1.0	
701			3	0.50	24.0000	Bend													Forged	S (L)	22.5	0.375	X-60	OB																		1/1/1967	1947977	1.0	
702			3	0.50	24.0000	Bend													Forged	S (L)	22	0.375	X-60	Right																		1/1/1967	1947977	1.0	
703			3	0.50	24.0000	Bend													Forged	S (L)	22	0.375	X-60	Left																		1/1/1967	1947977	1.0	
704			3	0.50	24.0000	Bend													Forged	S (L)	22	0.375	X-60	OB																		1/1/1967	1947977	1.0	
705			3	0.50	24.0000	Bend													Forged	S (L)	22	0.375	X-60	Sag																		1/1/1967	1947977	1.0	
706			3	0.50	24.0000	Bend													Forged	S (L)	22	0.375	X-60	Sag																		1/1/1967	1947977	1.0	
707			3	0.50	24.0000	Bend													Forged	S (L)	22	0.375	X-60	OB																		1/1/1967	1947977	1.0	
708			3	0.50	24.0000	Bend													Forged	S (L)	45	0.375	X-60	OB																		1/1/1967	1947977	1.0	
709			3	0.50	24.0000	Bend													Forged	S (L)	45	0.375	X-60	Sag																		1/1/1967	1947977	1.0	
710			3	0.50	24.0000	Bend													Forged	S (L)	45	0.375	X-60	Sag																		1/1/1967	1947977	1.0	
711			3	0.50	24.0000	Bend													Forged	S (L)	45	0.375	X-60	OB																		1/1/1967	1947977	1.0	
712			3	0.50	24.0000	Bend													Forged	S (L)	45	0.375	X-60	OB																		1/1/1967	1947977	1.0	
713			3	0.50	24.0000	Bend													Forged	S (L)	45	0.375	X-60	Sag																		1/1/1967	1947977	1.0	
714			3	0.50	24.0000	Bend													Forged	S (L)	45	0.375	X-60	Sag																		1/1/1967	1947977	1.0	
715			3	0.50	24.0000	Bend													Forged	S (L)	45	0.375	X-60	OB																		1/1/1967	1947977	1.0	
716			3	0.50	24.0000	Bend													Forged	S (L)	45	0.375	X-60	Combo																		1/1/1967	1947977	1.0	
717			3	0.50	24.0000	Bend													Forged	S (L)	45	0.375	X-60	Combo																		1/1/1967	1947977	1.0	
718			3	0.50	24.0000	Bend													Forged	S (L)	45	0.375	X-60	Combo																		1/1/1967	1947977	1.0	
719			3	0.50	24.0000	Bend													Forged	S (L)	45	0.375	X-60	Combo																		1/1/1967	1947977	1.0	
720			3	0.50	24.0000	Bend													Forged	S (L)	45	0.375	X-60	OB																		1/1/1967	1947977	1.0	
721			3	0.50	24.0000	Bend													Forged	S (L)	45	0.375	X-60	Sag																		1/1/1967	1947977	1.0	
722			3	0.50	24.0000	Bend													Forged	S (L)	45	0.375	X-60	Sag																		1/1/1967	1947977	1.0	
723			3	0.50	24.0000	Bend													Forged	S (L)	45	0.375	X-60	OB																		1/1/1967	1947977	1.0	
724			3	0.50	24.0000	Bend													Forged	S (L)	63	0.375	X-60	Combo																			1/1/1967	1947977	1.0
725			3	0.50	24.0000	Bend													Forged	S (L)	15	0.375	X-60	Sag																		1/1/1967	1947977	1.0	
726			3	0.50	24.0000	Bend													Forged	S (L)	60	0.375	X-60	Combo																			1/1/1967	1947977	1.0
987	28.2600	159.2	3	0.50	24.0000	Pipe	63	0.312	X-60	DSAW	TAPE																														1/1/1968	1947993	1.0		
728			3	0.50	24.0000	Tap										8	Insect	No																							1/1/1966	1944834	1.0		
729			3	0.50	24.0000	Tap										8	ake-of	No																							1/1/1966	1944834	1.0		
730			3	0.50	24.0000	Valve																																			1/1/1966	1944834	1.0		
731			3	0.50	24.0000	Tap										8	ake-of	No																							1/1/1966	1944834	1.0		
732			3	0.50	24.0000	Tap										8	Insect	No																							1/1/1966	1944834	1.0		
995	28.2600	159.5	3	0.50	20.0000	Pipe	4	0.375	X-52	DSAW	TAPE																													1/1/1968	1947993	1.0			
734			3	0.50	24.0000	Bend													Forged	S (L)	4	0.375	X-60	OB																	1/1/1966	1944834	1.0		
735			3	0.50	24.0000	Bend													Miter	Other	3	0.312	X-60	OB																	1/1/1966	1944834	1.0		
573.1	0.0000	141.2	3	0.50	34.0000	Pipe	6	0.380	X-60	DSAW	Unknown																													1/1/1988	1949898	1.0			
737	22.8400	147C	3	0.50	24.0000	Casing																																		1/1/1966	1944834	1.0			
738			3	0.50	24.0000	Bend		</																																					

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Project Data				Pipe Data				Sleeve Data				Tap Data				Bend Data				Tee Data				Valve Data				Casing Data				Reducer Data				Date Data							
Item Number	Milepost	Pipe Segment	C.I. Use	Design Factor	Min Line Size	Type	Length	WT	Grade	Seam Type	Coating Type	Type	WT	Grade	Length	Size	Type	Isobore	Type	Radius	Angle	WT	Grade	Orientation	Branch Size	WT	Grade	Barrier	Type	Full Port	Size	Length	Reducer Size	Length	WT	Grade	Size	Year Installed	Job Number	Unit Factor			
858				3	0.50	24.0000	Bend													Forged	D (LL)	45	0.375	X-60	OB															1/1/1988	1947993	1.0	
859				3	0.50	24.0000	Bend													Forged	D (LL)	12	0.375	X-60	Combo																1/1/1988	1947993	1.0
860				3	0.50	24.0000	Bend													Forged	D (LL)	45	0.375	X-60	Combo																1/1/1988	1947993	1.0
861				3	0.50	24.0000	Bend													Forged	D (LL)	45	0.375	X-60	Left																1/1/1988	1947993	1.0
862				3	0.50	24.0000	Bend													Forged	D (LL)	45	0.375	X-60	Sag																1/1/1988	1947993	1.0
863				3	0.50	24.0000	Bend													Forged	D (LL)	41	0.375	X-60	OB																1/1/1988	1947993	1.0
291.1	12.0000	122		3	0.50	24.0000	Pipe	1800	0.312	X-52	DSAW	TAPE																											1/1/1987	4593331	1.0		
865				3	0.50	24.0000	Bend													Forged	D (LL)	45	0.375	X-60	Combo																1/1/1988	1947993	1.0
866				3	0.50	24.0000	Bend													Forged	D (LL)	12	0.375	X-60	Right																1/1/1988	1947993	1.0
867				3	0.50	24.0000	Bend													Forged	D (LL)	45	0.375	X-60	Combo																1/1/1988	1947993	1.0
868				3	0.50	24.0000	Bend													Forged	D (LL)	45	0.375	X-60	OB																1/1/1988	1947993	1.0
869				3	0.50	24.0000	Bend													Forged	D (LL)	45	0.375	X-60	Sag															1/1/1988	1947993	1.0	
870	25.7500	154C		3	0.50	24.0000	Casing																													30	97			1/1/1988	1947993	1.0	
871				3	0.50	24.0000	Bend														Forged	D (LL)	45	0.375	X-60	Sag														1/1/1988	1947993	1.0	
872				3	0.50	24.0000	Bend														Forged	D (LL)	45	0.375	X-60	OB														1/1/1988	1947993	1.0	
873				3	0.50	24.0000	Tap																																	1/1/1988	1947993	1.0	
874				3	0.50	24.0000	Bend																																	1/1/1988	1947993	1.0	
875				3	0.50	24.0000	Bend														Miter	Other	2	0.312	X-60	Left														1/1/1988	1947993	1.0	
876				3	0.50	24.0000	Bend														Miter	Other	3	0.312	X-60	Left														1/1/1988	1947993	1.0	
877				3	0.50	24.0000	Bend														Miter	Other	1.5	0.312	X-60	Left														1/1/1988	1947993	1.0	
878				3	0.50	24.0000	Bend														Miter	Other	1	0.312	X-60	Combo															1/1/1988	1947993	1.0
879				3	0.50	24.0000	Bend														Miter	Other	1.5	0.312	X-60	Left														1/1/1988	1947993	1.0	
880				3	0.50	24.0000	Bend														Forged	D (LL)	5	0.375	X-60	Unknown															1/1/1988	1947993	1.0
881				3	0.50	24.0000	Bend														Forged	Unknown	5	0.375	X-60	Left															1/1/1988	1947993	1.0
882				3	0.50	24.0000	Bend														Miter	Other	3	0.312	X-60	OB															1/1/1988	1947993	1.0
883				3	0.50	24.0000	Bend														Miter	Other	2	0.312	X-60	Combo															1/1/1988	1947993	1.0
884				3	0.50	24.0000	Bend														Forged	Unknown	5.5	0.375	X-60	Left															1/1/1988	1947993	1.0
885				3	0.50	24.0000	Bend														Forged	Unknown	8	0.375	X-60	Left															1/1/1988	1947993	1.0
886				3	0.50	24.0000	Bend														Forged	Unknown	7.5	0.375	X-60	Combo															1/1/1988	1947993	1.0
887				3	0.50	24.0000	Bend														Forged	Unknown	7.5	0.375	X-60	Combo															1/1/1988	1947993	1.0
888				3	0.50	24.0000	Bend														Forged	D (LL)	45	0.375	X-60	OB														1/1/1988	1947993	1.0	
889				3	0.50	24.0000	Bend														Forged	D (LL)	45	0.375	X-60	Sag														1/1/1988	1947993	1.0	
890				3	0.50	24.0000	Bend														Forged	D (LL)	45	0.375	X-60	OB														1/1/1988	1947993	1.0	
891				3	0.50	24.0000	Bend														Forged	D (LL)	45	0.375	X-60	Sag														1/1/1988	1947993	1.0	
892				3	0.50	24.0000	Bend														Forged	D (LL)	45	0.375	X-60	OB															1/1/1988	1947993	1.0
893				3	0.50	24.0000	Tap																																	1/1/1988	1947993	1.0	
894				3	0.50	24.0000	Bend																																	1/1/1988	1947993	1.0	
895				3	0.50	24.0000	Bend																																	1/1/1988	1947993	1.0	
896				3	0.50	24.0000	Bend																																	1/1/1988	1947993	1.0	
897				3	0.50	24.0000	Bend																																	1/1/1988	1947993	1.0	
898				3	0.50	24.0000	Bend																																	1/1/1988	1947993	1.0	
899				3	0.50	24.0000	Bend																																	1/1/1988	1947993	1.0	
900				3	0.50	24.0000	Bend																																	1/1/1988	1947993	1.0	
314	12.4000	122.3		3	0.50	20.0000	Pipe	2	0.375	X-52	DSAW	TAPE																										1/1/1987	4593331	1.0			
902				3	0.50	24.0000	Tap																																	1/1/1988	1947993	1.0	
903				3	0.50	24.0000	Tap																																	1/1/1988	1947993	1.0	
904				3	0.50	24.0000	Valve																																	1/1/1988	1947993	1.0	
905				3	0.50	24.0000	Tap																																	1/1/1988	1947993	1.0	
906				3	0.50	24.0000	Tap																																	1/1/1988	1947993	1.0	
907				3	0.50	24.0000	Bend																																	1/1/1988	1947993	1.0	
880	20.0100	142		3	0.50	24.0000	Pipe	2361	0.312	X-52	DSAW	XTRUPL																															

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Project Data				Pipe Data				Sleeve Data				Tap Data				Bend Data				Tee Data				Valve Data				Casing Data				Reducer Data				Date Data						
Line Number	Milepost	Pipe Segment	CL Use	Design Factor	Min Line Size	Type	Length	WT	Grade	Seam Type	Casing Type	Type	WT	Grade	Length	Size	Type	Isobore	Type	Radius	Angle	WT	Grade	Chart	Branch Side	WT	Grade	Barrel	Type	Full Port	Size	Length	Reducer Size	Length	WT	Grade	Size	Year Installed	Job Number	Unit Factor		
915			3	0.50	24.0000	Bend														Forged	5 D (LL)	45	0.375	GRB	Left														1/1/1977	185596	1.0	
916			3	0.50	24.0000	Reducer																																1/1/1977	185596	1.0		
611	20.1500	142.3	3	0.50	24.0000	Pipe	795	0.312	X-52	DSAW	XTRUPL																											1/1/1988	4593422	1.0		
340	12.9500	124.3	3	0.50	20.0000	Pipe	3	0.375	X-52	DSAW	TAPE																											1/1/1988	4690605	1.0		
341	12.9500	125	3	0.50	24.0000	Pipe	1171	0.312	X-60	DSAW	TAPE																											1/1/1988	4690605	1.0		
920			3	0.50	20.0000	Bend														Forged	5 D (LL)	22	0.375	GRB	OB														1/1/1952	118626	1.0	
921			3	0.50	20.0000	Bend														Forged	5 D (LL)	22	0.375	GRB	Sag														1/1/1952	118626	1.0	
922			3	0.50	20.0000	Bend														Forged	5 D (LL)	22	0.375	GRB	Sag														1/1/1952	118626	1.0	
923			3	0.50	20.0000	Bend														Forged	5 D (LL)	22	0.375	GRB	OB														1/1/1952	118626	1.0	
924			3	0.50	20.0000	Bend														Forged	5 D (LL)	22	0.375	GRB	OB														1/1/1952	118626	1.0	
925			3	0.50	20.0000	Bend														Forged	5 D (LL)	22	0.375	GRB	Sag														1/1/1952	118626	1.0	
926			3	0.50	20.0000	Bend														Forged	5 D (LL)	22	0.375	GRB	Sag														1/1/1952	118626	1.0	
927			3	0.50	20.0000	Bend														Forged	5 D (LL)	22	0.375	GRB	OB														1/1/1952	118626	1.0	
928			3	0.50	20.0000	Bend														Forged	5 D (LL)	14	0.375	GRB	OB														1/1/1952	118626	1.0	
929			3	0.50	20.0000	Bend														Forged	5 D (LL)	16	0.375	GRB	Sag														1/1/1952	118626	1.0	
930			3	0.50	20.0000	Tap																																1/1/1952	118626	1.0		
918	27.0700	155.6	3	0.50	20.0000	Pipe	14	0.375	X-42	DSAW	TAPE																											1/1/1988	4690605	1.0		
932			3	0.50	20.0000	Bend																																	1/1/1986	7001958	1.0	
1006	28.8300	161.6	3	0.50	20.0000	Pipe	2	0.375	X-52	DSAW	TAPE																											1/1/1988	4690694	1.0		
240.1	10.4000	xx	3	0.50	30.0000	Pipe	14	0.375	X-52	DSAW	TAPE																											1/1/1988	4690583	1.0		
935			3	0.50	20.0000	Bend																																		4/29/1993	4988184	1.0
936			3	0.50	20.0000	Bend																																4/29/1993	4988184	1.0		
937	27.6500	156.5C	3	0.50	20.0000	Casing																																	4/29/1993	4988184	1.0	
938			3	0.50	20.0000	Bend																																	4/29/1993	4988184	1.0	
939			3	0.50	20.0000	Bend														Miter	Other	2	0.375	X-52	Combo															4/29/1993	4988184	1.0
940			3	0.50	20.0000	Bend														Forged	5 D (LL)	60	0.375	X-52	Right															4/29/1993	4988184	1.0
247.5	xx		3	0.50	30.0000	Pipe	7	0.375	X-52	DSAW	TAPE																											1/1/1988	4690563	1.0		
942	27.7000	156.6C	3	0.50	20.0000	Casing																																	1/1/1952	118626	1.0	
248.5	xx		3	0.50	34.0000	Pipe	8	0.380	X-60	DSAW	TAPE																												1/1/1988	4690563	1.0	
945			3	0.50	20.0000	Bend																																	4/4/2003	7043414	1.0	
946			3	0.50	20.0000	Bend																																	4/4/2003	7043414	1.0	
947			3	0.50	20.0000	Bend																																	4/4/2003	7043414	1.0	
478	16.6546	137.2	3	0.50	20.0000	Pipe	26	0.312	X-42	SMLS	TAPE																											1/1/1989	4701553	1.0		
419	14.5200	129.3	3	0.50	20.0000	Pipe	5	0.375	X-52	DSAW	XTRUPL																											1/1/1987	4701553	1.0		
950			3	0.50	20.0000	Bend																																	4/4/2003	7043414	1.0	
951			3	0.50	20.0000	Bend																																	4/4/2003	7043414	1.0	
952			3	0.50	20.0000	Bend																																	4/4/2003	7043414	1.0	
424	14.7800	130.3	3	0.50	20.0000	Pipe	3	0.375	X-52	DSAW	TAPE																												1/1/1989	4701553	1.0	
954	27.7500	157.1C	3	0.50	20.0000	Casing																																	1/1/1952	118626	1.0	
426	14.9000	130.6	3	0.50	24.0000	Pipe	316	0.312	X-52	DSAW	TAPE																											1/1/1989	4701553	1.0		
956	27.7722	157.2C	3	0.50	20.0000	Casing																																	1/1/1952	118626	1.0	
957	27.7800	157.3C	3	0.50	20.0000	Casing																																	1/1/1952	118626	1.0	
958			3	0.50	20.0000	Bend																																		1/1/1952	118626	1.0
959			3																																							

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Project Data				Pipe Data				Sleeve Data				Tap Data				Bend Data				Toe Data				Valve Data				Casing Data				Reducer Data				Date Data									
Ident Number	Milepost	Pipe Segment	C. Use	Design Factor	Main Line Size	Type	Length	W.T.	Grade	Seam Type	Coating Type	Type	W.T.	Grade	Length	Size	Type	Islets to X	Type	Radius	Angle	W.T.	Grade	Orient	branch Size	W.T.	Grade	Barrel Type	Type	Full Port	Size	Length	Reducer Size	Length	Grade	Size	Year Installed	Job Number	Joint Factor						
1032				3	0.50	24.0000	Bend													Miter	Other	1	0.375	X.60	Right														1/1/1986	1941186	1.0				
1033				3	0.50	24.0000	Bend													Miter	Other	1	0.375	X.60	Right															1/1/1986	1941186	1.0			
1034				3	0.50	24.0000	Bend													Miter	Other	1	0.375	X.60	Right															1/1/1986	1941186	1.0			
1035				3	0.50	24.0000	Bend													Miter	Other	1	0.375	X.60	Right															1/1/1986	1941186	1.0			
1036				3	0.50	24.0000	Bend													Miter	Other	1	0.375	X.60	Right															1/1/1986	1941186	1.0			
1037				3	0.50	24.0000	Bend													Miter	Other	1	0.375	X.60	Right															1/1/1986	1941186	1.0			
1038				3	0.50	24.0000	Bend													Miter	Other	1	0.375	X.60	Right															1/1/1986	1941186	1.0			
1039				3	0.50	24.0000	Tap													6	hneck	No																			1/1/1986	1941186	1.0		
1040				3	0.50	24.0000	Tap													6	ake-off	No																			1/1/1986	1941186	1.0		
1041				3	0.50	24.0000	Valve																																		1/1/1986	1941186	1.0		
1165-1	33.4150	167.25		3	0.50	20.0000	Pipe	30	0.312	X.42	OSAW	Tape																												1008/1989	472772	1.0			
1043				3	0.50	24.0000	Tap													6	ake-off	No																			1/1/1986	1941186	1.0		
1044				3	0.50	24.0000	Tap													6	hneck	No																			1/1/1986	1941186	1.0		
1045				3	0.50	24.0000	Bend													Miter	Other	1	0.375	X.60	Right																1/1/1986	1941186	1.0		
1046				3	0.50	24.0000	Bend													Miter	Other	2	0.375	X.60	Right																1/1/1986	1941186	1.0		
1047				3	0.50	24.0000	Bend													Forged	D (LL)	45	0.375	X.60	Left																1/1/1986	1941186	1.0		
1048				3	0.50	24.0000	Bend													Forged	D (LL)	47	0.375	X.60	Right																	1/1/1986	1941186	1.0	
1049				3	0.50	24.0000	Bend													Miter	Other	1	0.375	X.60	Right																1/1/1986	1941186	1.0		
1050				3	0.50	24.0000	Bend													Miter	Other	1	0.375	X.60	Right																1/1/1986	1941186	1.0		
1051				3	0.50	24.0000	Bend													Miter	Other	3	0.375	X.60	Right																1/1/1986	1941186	1.0		
1052				3	0.50	24.0000	Bend													Miter	Other	2	0.375	X.60	Left																	1/1/1986	1941186	1.0	
1053				3	0.50	24.0000	Bend													Forged	D (LL)	45	0.375	X.60	OB																	1/1/1986	1941186	1.0	
1054				3	0.50	24.0000	Bend													Forged	D (LL)	45	0.375	X.60	Sag																	1/1/1986	1941186	1.0	
1055	30.4990	163.55C		3	0.50	24.0000	Casing																																		1/1/1986	1941186	1.0		
1056				3	0.50	24.0000	Bend														Forged	nknow	4	0.375	X.60	Right																1/1/1986	1941186	1.0	
1057				3	0.50	24.0000	Bend													Forged	D (LL)	45	0.375	X.60	Sag																	1/1/1986	1941186	1.0	
1058				3	0.50	24.0000	Bend													Forged	D (LL)	45	0.375	X.60	OB																	1/1/1986	1941186	1.0	
1059				3	0.50	24.0000	Bend													Miter	Other	3	0.375	X.60	Right																	1/1/1986	1941186	1.0	
1060				3	0.50	24.0000	Tap																																			1/1/1986	1941186	1.0	
1061				3	0.50	24.0000	Bend													.75	ake-off																					1/1/1986	1941186	1.0	
1062				3	0.50	24.0000	Bend													Forged	nknow	8	0.375	X.60	Left																		1/1/1986	1941186	1.0
1063				3	0.50	24.0000	Bend													Forged	D (LL)	43	0.375	X.60	Left																		1/1/1986	1941186	1.0
1064				3	0.50	24.0000	Bend													Forged	D (LL)	43	0.375	X.60	Right																		1/1/1986	1941186	1.0
1065				3	0.50	24.0000	Bend													Forged	D (LL)	45	0.375	X.60	Combo																		1/1/1986	1941186	1.0
1066				3	0.50	24.0000	Bend													Forged	D (LL)	60	0.375	X.60	Combo																		1/1/1986	1941186	1.0
1067				3	0.50	24.0000	Bend													Forged	D (LL)	45	0.375	X.60	Sag																	1/1/1986	1941186	1.0	
1068				3	0.50	24.0000	Bend													Forged	D (LL)	45	0.375	X.60	OB																	1/1/1986	1941186	1.0	
1069				3	0.50	24.0000	Bend													Forged	D (LL)	23	0.375	X.60	Left																		1/1/1986	1941186	1.0
1070				3	0.50	24.0000	Bend													Forged	D (LL)	45	0.375	X.60	OB																		1/1/1986	1941186	1.0
1071				3	0.50	24.0000	Bend													Forged	D (LL)	45	0.375	X.60	Sag																	1/1/1986	1941186	1.0	
1072				3	0.50	24.0000	Bend													Forged	D (LL)	32	0.375	X.60	Right																		1/1/1986	1941186	1.0
1073	30.5000	163.50C		3	0.50	24.0000	Casing																																			1/1/1986	1941186	1.0	
1074				3	0.50	24.0000	Tap																																				1/1/1986	1941186	1.0
1075				3	0.50	24.0000	Bend													4	hneck																					1/1/1986	1941186	1.0	
1076				3	0.50	24.0000	Bend													Forged	D (LL)	5	0.375	X.60	Right																		1/1/1986	1941186	1.0
1077				3	0.50	24.0000	Bend													Miter	Other	3	0.375	X.60	Right																	1/1/1986	1941186	1.0	
1078				3	0.50	24.0000	Bend													Miter	Other	2	0.375	X.60	Right																	1/1/1986	1941186	1.0	
1079				3	0.50	24.0000	Bend													Forged	D (LL)	4	0.375	X.60	Left																	1/1/1986	1941186	1.0	
1080				3	0.50	24.0000	Bend													Miter	Other	1	0.375	X.60	Right																				

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Stress Calculations				Strength Test Pressure Reports							
MPYS	WT	WT	%P	Test Job	Test Date	Test Pressure	Test Medium	Test Duration	SIPR Status	SIPR?	
35000	0.281	0.281	38.13								
60000	0.5	0.5	22.50	472772	10/5/1989	650.0	W	8.00	Tested	Yes	
60000	0.576	0.576	19.53								
60000	0.576	0.576	19.53								
60000	0.576	0.576	19.53								
35000	0.281	0.281	38.13	472772	10/5/1989	650.0	W	8.00	Tested	Yes	
0	0	0.25	0.00								
0	0	0.25	0.00								
0	0	0.25	0.00								
0	0	0.25	0.00								
0	0	0.25	0.00								
60000	0.576	0.576	19.53								
60000	0.576	0.576	19.53								
60000	0.576	0.576	19.53								
33000	0.25	0.25	56.62	recon pipe	472772	10/5/1989	650.0	W	8.00	Tested	Yes
60000	0.576	0.576	19.53								
60000	0.576	0.576	19.53								
33000	0.25	0.25	56.62	recon pipe	472772	10/5/1989	650.0	W	8.00	Tested	Yes
35000	0.281	0.281	38.13	STPR on 472772	472772	10/5/1989	650.0	W	8.00	Tested	Yes
60000	0.576	0.576	19.53								
60000	0.576	0.576	19.53								
35000	0.281	0.281	38.13	STPR on 472772	472772		640.0	W	8.00	Tested	Yes
60000	0.576	0.576	19.53								
35000	0.312	0.312	34.34		4690905	10/4/1988	670.0	W	8.00	Tested	Yes
35000	0.312	0.312	34.34		4690905	10/4/1988	670.0	W	8.00	Tested	Yes
60000	0.576	0.576	19.53								
60000	0.576	0.576	19.53								
0	0	0.25	0.00								
60000	0.576	0.576	19.53								
35000	0.312	0.312	34.34		4690905	10/4/1988	670.0	W	8.00	Tested	Yes
60000	0.576	0.576	19.53								
35000	0.312	0.312	34.34		4690905	10/4/1988	670.0	W	8.00	Tested	Yes
60000	0.576	0.576	19.53								
60000	0.576	0.576	19.53								
35000	0.312	0.312	34.34		4690905	10/4/1988	670.0	W	8.00	Tested	Yes
35000	0.312	0.312	34.34		4690954	10/6/1988	640.0	W	8.00	Tested	Yes
52000	0.375	0.375	34.62								
52000	0.375	0.375	34.62								
0	0	0.25	0.00								
35000	0.312	0.312	34.34		4690954	10/6/1988	640.0	W	8.00	Tested	Yes
52000	0.375	0.375	34.62								
52000	0.375	0.375	34.62								
35000	0.312	0.312	34.34		4690954	10/6/1988	640.0	W	8.00	Tested	Yes
0	0	0.25	0.00								
52000	0.35	0.35	37.09								
52000	0.35	0.35	37.09								
52000	0.35	0.35	37.09								
52000	0.35	0.35	37.09								
52000	0.35	0.35	37.09								
42000	0.312	0.312	26.62		4701553	4/20/1989	620.0	W	8.00	Tested	Yes
0	0	0.25	0.00								

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Stress Calculations				Strength Test Pressure Reports								
SMYS	WT	WT	% P	Test Job	Test Date	Test Pressure	Test Medium	Test Duration	SIPR Status	SIPR?		
80000	0.5	0.5	18.75									
80000	0.5	0.5	18.75									
35000	0.312	0.312	34.34	469066	11/15/1988	659.0	W	8.00	Tested	Yes		
35000	0.312	0.312	34.34	469066	11/15/1988	659.0	W	8.00	Tested	Yes		
52000	0.438	0.438	27.90		1/1/1963	1010.0	W	1.00	Missing	Missing		
38000	UNK	0.375	44.74	sleeve unk values								
35000	0.375	0.375	48.57	elbow								
35000	0.375	0.375	48.57	reducer UNK values								
52000	0.438	0.438	29.04	155377	5/1/1965	1010.0	W	1.00	Tested	Yes		
52000	0.375	0.375	34.62	x52, 1963 std 283158								
52000	0.375	0.375	34.62	x52, 1963 std 283158								
52000	0.375	0.375	34.62	x52 1963 std 283158								
52000	0.422	0.422	29.05		1/1/1965	1080.0	W	1.00	Missing	Missing		
38000	unk	0.375	47.37	sleeve unk values								
52000	0.375	0.375	34.62									
38000	unk	0.375	47.37	sleeve unk values								
52000	0.375	0.375	34.62									
52000	0.375	0.375	34.62									
52000	0.375	0.375	34.62									
52000	0.35	0.35	37.09									
52000	0.35	0.35	37.09									
0	0	0.25	0.00	tap								
52000	0.422	0.422	30.76		1/1/1965	1080.0	W	1.00	Missing	Missing		
52000	0.422	0.422	29.05		1/1/1965	1080.0	W	1.00	Missing	Missing		
52000	0.422	0.422	30.76		1/1/1963	1050.0	W	1.00	Missing	Missing		
52000	0.375	0.375	34.62	Not less than .375								
52000	0.375	0.375	34.62	Not less than .375								
52000	0.375	0.375	34.62									
52000	0.375	0.375	34.62									
35000	0.281	0.281	38.13	194793	8/20/1988	660.0	W	8.00	Tested	Yes		
52000	0.5	0.5	25.96									
52000	0.437	0.437	28.05		1/1/1965	1080.0	W	1.00	Missing	Missing		
52000	0.5	0.5	25.96									
48000	0.5	0.5	29.35									
48000	0.5	0.5	29.35									
0	0	0.25	0.00	Valve								
48000	0.5	0.5	29.35									
48000	0.5	0.5	29.35									
52000	0.5	0.5	25.96							Missing		
52000	0.438	0.438	27.90									
52000	0.5	0.5	25.96									
52000	0.489	0.489	27.98	160041	10/1/1965	1080.0	W	1.00	Tested	Yes		
52000	0.5	0.5	25.96									
52000	0.35	0.35	37.09	162548	1/1/1965	976.0	W	12.00	Tested	Yes		
52000	0.375	0.375	34.62									
52000	0.375	0.375	34.62									
0	0	0.25	0.00	tap								
52000	0.375	0.375	34.62									
52000	0.375	0.375	34.62									
0	0	0.25	0.00	tap								
52000	0.375	0.375	34.62									
52000	0.375	0.375	34.62									

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Stress Calculations				Strength Test Pressure Reports						
SMYS	WT	WT	%P	Test Job	Test Date	Test Pressure	Test Medium	Test Duration	SIPR Status	SIPR?
0	0	0.25	0.00	casing						
0	0	0.25	0.00	casing						
52000	0.375	0.375	34.62							
52000	0.375	0.375	34.62							
0	0	0.25	0.00	lap						
52000	0.35	0.35	37.09	162548	1/1/1965	970.0	W	12.00	Tested	Yes
52000	0.375	0.375	34.62							
52000	0.375	0.375	34.62							
52000	0.375	0.375	34.62							
0	0	0.25	0.00	lap						
52000	0.35	0.35	37.09	162548	1/1/1965	970.0	W	12.00	Tested	Yes
52000	0.375	0.375	34.62							
52000	0.35	0.35	37.09	162548	1/1/1965	970.0	W	12.00	Tested	Yes
52000	0.375	0.375	34.62							
52000	0.375	0.375	34.62							
52000	0.375	0.375	34.62							
52000	0.375	0.375	34.62							
52000	0.375	0.375	34.62							
0	0	0.25	0.00	lap						
52000	0.375	0.375	34.62							
52000	0.5	0.5	25.96		1/1/1965	970.0	W	4.00	Missing	Missing
52000	0.375	0.375	34.62							
52000	0.375	0.375	34.62							
52000	0.375	0.375	34.62							
52000	0.375	0.375	34.62							
0	0	0.25	0.00	casing						
52000	0.35	0.35	37.09	162548	1/1/1965	970.0	W	12.00	Tested	Yes
52000	0.375	0.375	34.62							
52000	0.375	0.375	34.62							
52000	0.35	0.35	37.09	162548	1/1/1965	970.0	W	12.00	Tested	Yes
52000	0.35	0.35	37.09	162548	1/1/1965	970.0	W	12.00	Tested	Yes
0	0	0.25	0.00	lap						
52000	0.35	0.35	37.09							
52000	0.35	0.35	37.09	162548	1/1/1965	970.0	W	4.00 12.00	Tested	Yes
52000	0.35	0.35	37.09	162548	1/1/1965	970.0	W	12.00	Tested	Yes
52000	0.35	0.35	37.09	162548	1/1/1965	970.0	W	12.00	Tested	Yes
52000	0.35	0.35	37.09	162548	1/1/1965	970.0	W	12.00	Tested	Yes
0	0	0.25	0.00	lap						
52000	0.35	0.35	37.09							
52000	0.35	0.35	37.09							
52000	0.375	0.375	34.62							
52000	0.375	0.375	34.62							
52000	0.375	0.375	34.62							
52000	0.375	0.375	34.62							
0	0	0.25	0.00	lap						
0	0	0.25	0.00	lap						
52000	0.5	0.5	25.96	162548					Missing	
52000	0.5	0.5	25.96	162548					Missing	
52000	0.375	0.375	34.62							
52000	0.5	0.5	25.96	162548					Missing	
35000	0.5	0.5	38.57							
0	0	0.25	0.00	lap						
35000	0.5	0.5	38.57							
52000	0.35	0.35	37.09	162548	1/1/1965	970.0	W	12.00	Tested	Yes

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Stress Calculations				Strength Test Pressure Reports						
SAV's	WT	WT	% P	Test Job	Test Date	Test Pressure	Test Medium	Test Duration	SIPR Status	SIPR?
35000	0.5	0.5	38.57							
0	0	0.25	0.00							
35000	0.5	0.5	38.57							
35000	0.5	0.5	38.57							
52000	0.35	0.35	37.09	162548	1/1/1965	970.0	W	12.00	Tested	Yes
0	0	0.25	0.00							
52000	0.35	0.35	37.09	162548	1/1/1965	970.0	W	12.00	Tested	Yes
60000	0.576	0.576	19.53							
60000	0.576	0.576	19.53							
60000	0.576	0.576	19.53							
60000	0.576	0.576	19.53							
35000	0.5	0.5	38.57							
52000	0.35	0.35	37.09	162548	1/1/1965	970.0	W	12.00	Tested	Yes
0	0	0.25	0.00							
0	0	0.25	0.00							
0	0	0.25	0.00							
52000	0.375	0.375	34.62							
52000	0.375	0.375	34.62							
52000	UNLK	0.375	34.62	sleeve std >= pipe						
52000	0.35	0.35	37.09	162548	1/1/1965	970.0	W	12.00	Tested	Yes
60000	0.375	0.375	30.00							
60000	0.375	0.375	30.00							
0	0	0.25	0.00							
60000	0.375	0.375	30.00							
60000	0.375	0.375	30.00							
52000	0.35	0.35	37.09	162548	1/1/1965	970.0	W	12.00	Tested	Yes
0	0	0.25	0.00							
0	0	0.25	0.00							
52000	0.375	0.375	34.62							
52000	0.375	0.375	34.62							
0	0	0.25	0.00							
38000	UNLK	0.375	47.37	sleeve unk values						
52000	0.375	0.375	34.62							
46000	0.375	0.375	39.13							
52000	0.35	0.35	37.09	162548	1/1/1965	970.0	W	12.00	Tested	Yes
52000	0.35	0.35	37.09	162548	1/1/1965	970.0	W	12.00	Tested	Yes
52000	0.35	0.35	37.09	162548	1/1/1965	970.0	W	12.00	Tested	Yes
35000	0.375	0.375	42.86							
35000	0.375	0.375	42.86							
35000	0.375	0.375	42.86							
35000	0.375	0.375	42.86							
50000	0.375	0.375	30.00							
52000	0.35	0.35	37.09	162548	1/1/1965	970.0	W	12.00	Tested	Yes
52000	0.375	0.375	28.85							
52000	0.375	0.375	28.85							
52000	0.35	0.35	37.09	162548	1/1/1965	970.0	W	12.00	Tested	Yes
60000	0.5	0.5	18.75							
52000	0.35	0.35	37.09	162548	1/1/1965	970.0	W	12.00	Tested	Yes
52000	0.35	0.35	37.09	162548	1/1/1965	970.0	W	12.00	Tested	Yes
0	0	0.25	0.00							
52000	0.5	0.5	24.52							
52000	0.5	0.5	24.52							
52000	0.5	0.5	24.52							
52000	0.5	0.5	24.52							
52000	0.5	0.5	24.52							
52000	0.5	0.5	24.52							

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Stress Calculations				Strength Test Pressure Reports						
MPYS	WT	WT	%P	Test Job	Test Date	Test Pressure	Test Medium	Test Duration	STPR Status	STPR?
52000	0.5	0.5	24.52							
52000	0.5	0.5	24.52							
52000	0.5	0.5	24.52							
52000	0.5	0.5	24.52							
52000	0.5	0.5	24.52							
52000	0.35	0.35	37.09	162548	1/1/1965	9750	W	12.00	Tested	Yes
52000	0.5	0.5	24.52							
52000	0.5	0.5	24.52							
52000	0.5	0.5	25.96						Missing	
52000	0.5	0.5	24.52							
52000	0.5	0.5	24.52							
485000	0.375	0.375	36.96							
42000	0.375	0.375	23.81							
52000	0.35	0.35	37.09	162548	1/1/1965	9750	W	12.00	Tested	Yes
60000	0.312	0.312	24.64							
52000	0.5	0.5	25.96						Missing	
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
52000	0.5	0.5	25.96						Missing	
60000	0.375	0.375	20.00							
52000	0.35	0.35	37.09	162548	1/1/1965	9750	W	12.00	Tested	Yes
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
52000	0.312	0.312	34.67	4696563	10/21/1988	1200	W	8.00	Tested	Yes
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
0	0	0.25	0.00	lap						
0	0	0.25	0.00	lap						
0	0	0.25	0.00	lap						
0	0	0.25	0.00	lap						
0	0	0.25	0.00	lap						
0	0	0.25	0.00	lap						
0	0	0.25	0.00	lap						
0	0	0.25	0.00	lap						
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
42000	0.375	0.375	35.71	4696563	10/22/1988	8110	W	8.50	Tested	Yes

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Stress Calculations				Strength Test Pressure Reports						
SPMS	WT	WT	% P	Test Job	Test Date	Test Pressure	Test Medium	Test Duration	SIPR Status	SIPR?
60000	0.375	0.375	20.00							
52000	0.312	0.312	34.67	4727772	10/5/1989	650.0	W	8.00	Tested	Yes
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.312	0.312	24.04							
52000	0.312	0.312	23.11	4727772	10/5/1989	650.0	W	8.00	Tested	Yes
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
35000	0.375	0.375	28.57	1937168	12/6/1984	1203.0	W	8.00	Tested	Yes
60000	0.375	0.375	20.00							
0	0	0.25	0.00	casing						
60000	0.375	0.375	20.00	1937168	12/14/1984	1015.0	W	1.00	Tested	Yes
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.38	0.38	27.96	1937168	12/6/1984	1203.0	W	8.00	Tested	Yes
0	0	0.25	0.00	lap						
0	0	0.25	0.00	lap						
0	0	0.25	0.00	lap						
0	0	0.25	0.00	MLV						
0	0	0.25	0.00	lap						
0	0	0.25	0.00	lap						
0	0	0.25	0.00	lap						
52000	0.375	0.375	19.23	1941186	12/6/1985	1155.0	W	4.00	Tested	Yes
60000	0.375	0.375	20.00	1941186	1/15/1986	1198.0	W	8.00	Tested	Yes
60000	0.375	0.375	16.67							
60000	0.375	0.375	16.67							
60000	0.312	0.312	20.03							
60000	0.375	0.375	20.00	1941186	1/15/1986	1198.0	W	8.00	Tested	Yes
60000	0.375	0.375	20.00	1941186	1/15/1986	1198.0	W	8.00	Tested	Yes
35000	0.375	0.375	28.57							
35000	0.375	0.375	28.57							
35000	0.375	0.375	28.57							
35000	0.375	0.375	28.57							
35000	0.375	0.375	28.57							
35000	0.375	0.375	28.57							
35000	0.375	0.375	28.57							
35000	0.375	0.375	28.57							
35000	0.375	0.375	28.57							
0	0	0.25	0.00	casing						
35000	0.375	0.375	28.57							
35000	0.375	0.375	28.57							
35000	0.375	0.375	28.57							
35000	0.375	0.375	28.57							
35000	0.375	0.375	28.57							
35000	0.375	0.375	28.57							
52000	0.375	0.375	19.23	1941186	12/6/1985	1155.0	W	4.00	Tested	Yes
60000	0.375	0.375	16.67							
52000	0.312	0.312	23.11	1941186	8/19/1985	650.0	W	8.00	Tested	Yes
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							

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Stress Calculations				Strength Test Pressure Reports						
SMYS	WT	WT	% P	Test Job	Test Date	Test Pressure	Test Medium	Test Duration	STPR Status	STPR?
35000	0.375	0.375	28.57							
35000	0.375	0.375	28.57							
35000	0.375	0.375	28.57							
0	0	0.25	0.00							
0	0	0.25	0.00							
60000	0.312	0.312	24.04	1944831	9/23/1996	1440.0	W	8.00	Tested	Yes
52000	0.312	0.312	27.74	1945815	8/21/1997	1245.0	W	8.00	Tested	Yes
35000	LNK	0.25	42.86							
35000	LNK	0.25	42.86							
35000	LNK	0.25	42.86							
52000	0.312	0.312	27.74	1945815	8/21/1997	1245.0	W	8.00	Tested	Yes
60000	0.375	0.375	16.67							
52000	0.312	0.312	27.74	1945815	8/21/1997	1245.0	W	8.00	Tested	Yes
60000	0.312	0.312	24.04	1947340	10/30/1996	1433.0	W	8.00	Tested	Yes
60000	0.312	0.312	24.04	1947340	10/30/1996	1433.0	W	8.00	Tested	Yes
60000	0.375	0.375	16.67							
60000	0.375	0.375	16.67							
0	0	0.25	0.00							
0	0	0.25	0.00							
0	0	0.25	0.00							
0	0	0.25	0.00							
0	0	0.25	0.00							
60000	0.375	0.375	16.67							
60000	0.375	0.375	16.67							
60000	0.312	0.312	24.04	1947340	10/30/1996	1433.0	W	8.00	Tested	Yes
35000	0.375	0.375	28.57							
35000	0.375	0.375	28.57							
60000	0.312	0.312	24.04	1947340	11/14/1996	1420.0	W	8.00	Tested	Yes
60000	0.312	0.312	24.04	1947340	11/6/1996	1438.0	W	8.00	Tested	Yes
60000	0.375	0.375	16.67							
60000	0.312	0.312	24.04	1947340	11/6/1996	1238.0	W	8.00	Tested	Yes
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
0	0	0.25	0.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
0	0	0.25	0.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							

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Stress Calculations				Strength Test Pressure Reports						
SMYS	WT	WT	%P	Test Job	Test Date	Test Pressure	Test Medium	Test Duration	STPR Status	STPR?
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
52000	0.312	0.312	27.74	1945815	8/21/1987	12450	W	8.00	Tested	Yes
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
0	0	0.25	0.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
0	0	0.25	0.00							
60000	0.312	0.312	24.04							
60000	0.312	0.312	24.04							
60000	0.312	0.312	24.04							
60000	0.312	0.312	24.04							
60000	0.312	0.312	24.04							
60000	0.312	0.312	24.04							
60000	0.312	0.312	24.04							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.312	0.312	24.04							
60000	0.312	0.312	24.04							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
0	0	0.25	0.00							
0	0	0.25	0.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
0	0	0.25	0.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
60000	0.375	0.375	20.00							
52000	0.375	0.375	19.23	4593331	8/22/1987	10300	W	8.00	Tested	Yes
0	0	0.25	0.00							
0	0	0.25	0.00							
0	0	0.25	0.00							
0	0	0.25	0.00							
0	0	0.25	0.00							
60000	0.375	0.375	20.00							
52000	0.312	0.312	27.74	4593422	11/6/1987	12390	W	8.00	Tested	Yes
35000	0.375	0.375	34.29							
35000	0.375	0.375	34.29							
35000	0.375	0.375	34.29							
35000	0.375	0.375	34.29							
35000	0.375	0.375	34.29							
35000	0.375	0.375	34.29							

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Stress Calculations				Strength Test Pressure Reports						
Stress	WT	WT	% P	Test Job	Test Date	Test Pressure	Test Medium	Test Duration	SIPR Status	SIPR?
35000	0.375	0.375	34.29							
35000	0.375	0.375	34.29							
52000	0.312	0.312	27.74	4593422	10/5/1987	1245.0	W	8.00	Tested	Yes
52000	0.375	0.375	19.23	4690665	11/16/1988	1435.0	W	8.00	Tested	Yes
60000	0.312	0.312	24.04	4690665	11/12/1988	1445.0	W	8.00	Tested	Yes
35000	0.375	0.375	28.57							
35000	0.375	0.375	28.57							
35000	0.375	0.375	28.57							
35000	0.375	0.375	28.57							
35000	0.375	0.375	28.57							
35000	0.375	0.375	28.57							
35000	0.375	0.375	28.57							
35000	0.375	0.375	28.57							
35000	0.375	0.375	28.57							
0	0	0.25	0.00							
42000	0.375	0.375	23.81	1947993	8/19/1988	1425.0	W	8.00	Tested	Yes
52000	0.375	0.375	19.23							
52000	0.375	0.375	19.23	1947993	8/19/1988	1425.0	W	8.00	Tested	Yes
52000	0.375	0.375	28.85	4696663	10/21/1988	1200.0	W	8.00	Tested	Yes
52000	0.375	0.375	19.23							
52000	0.375	0.375	19.23							
0	0	0.25	0.00							
52000	0.375	0.375	19.23							
52000	0.375	0.375	19.23							
52000	0.375	0.375	19.23							
52000	0.375	0.375	28.85	4696663	10/21/1988	1200.0	W	8.00	Tested	Yes
0	0	0.25	0.00							
60000	0.38	0.38	27.96	4696663	10/21/1988	1200.0	W	8.00	Tested	Yes
60000	0.375	0.375	16.67							
60000	0.375	0.375	16.67							
60000	0.375	0.375	16.67							
42000	0.312	0.312	28.82	4701553	4/26/1989	655.0	W	4.00	Tested	Yes
52000	0.375	0.375	19.23		1/1/1989	1420.0	W	8.00	Missing	Missing
60000	0.375	0.375	16.67							
60000	0.375	0.375	16.67							
60000	0.375	0.375	16.67							
52000	0.375	0.375	19.23	4701553	1/13/1989	1222.0	W	8.00	Tested	Yes
0	0	0.25	0.00							
52000	0.312	0.312	27.74	4701553	1/21/1989	1251.0	W	8.00	Tested	Yes
0	0	0.25	0.00							
0	0	0.25	0.00							
35000	0.375	0.375	28.57							
35000	0.375	0.375	28.57							
35000	0.375	0.375	28.57							
35000	0.375	0.375	28.57							
35000	0.375	0.375	28.57							
35000	0.375	0.375	28.57							
35000	0.375	0.375	28.57							
35000	0.375	0.375	28.57							
52000	0.375	0.375	19.23	4701553	1/13/1989	1222.0	W	8.00	Tested	Yes
35000	0.375	0.375	28.57							
35000	0.375	0.375	28.57							
35000	0.375	0.375	28.57							
35000	0.375	0.375	28.57							
35000	0.375	0.375	28.57							
52000	0.375	0.375	19.23	4701553	1/13/1989	1222.0	W	8.00	Tested	Yes
60000	0.312	0.312	20.03							

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Stress Calculations				Strength Test Pressure Reports						
SMYS	WT	WT	% P	Test Job	Test Date	Test Pressure	Test Medium	Test Duration	STPR Status	STPR?
0	0	0.25	0.00							
0	0	0.25	0.00							
0	0	0.25	0.00							
0	0	0.25	0.00							
0	0	0.25	0.00							
60000	0.576	0.576	19.53	7002171	10/6/1997	1767.0	W	1.00	Tested	Yes
60000	0.576	0.576	19.53	7002171	10/6/1997	1094.0	W	8.00	Tested	Yes
35000	0.375	0.375	28.57							
0	0	0.25	0.00							
35000	0.375	0.375	28.57							
0	0	0.25	0.00							
35000	0.375	0.375	28.57							
0	0	0.25	0.00							
60000	0.576	0.576	19.53	7002171	10/6/1997	1767.0	W	1.00	Tested	Yes
0	0	0.25	0.00							
35000	0.375	0.375	28.57							
60000	0.576	0.576	19.53	7002171	10/6/1997	1767.0	W	1.00	Tested	Yes
35000	0.281	0.281	38.13							
35000	0.281	0.281	38.13							
35000	0.281	0.281	38.13							
0	0	0.25	0.00							
60000	0.576	0.576	19.53	7002171	10/6/1997	1767.0	W	1.00	Tested	Yes
60000	0.576	0.576	19.53	7002171	10/9/1997	1785.0	W	1.00	Tested	Yes
52000	0.375	0.375	19.23							
60000	0.576	0.576	19.53	7002171	10/6/1997	1094.0	W	8.00	Tested	Yes
52000	0.375	0.375	28.85							
52000	0.375	0.375	28.85							
0	0	0.25	0.00							
52000	0.375	0.375	28.85							
52000	0.375	0.375	28.85							
60000	0.576	0.576	19.53	7003858	5/14/1997	1756.0	W	1.00	Tested	Yes
60000	0.312	0.312	24.04	7036667	9/17/2001	1440.0	W	1.00	Tested	Yes
60000	0.375	0.375	16.67	7043414	3/25/2003	760.0	W	9.00	Tested	Yes
35000	0.281	0.281	38.13	STPR on 4727772						
60000	0.375	0.375	16.67	7043414	3/25/2003	760.0	W	9.00	Tested	Yes
60000	0.375	0.375	16.67	7043414	3/25/2003	760.0	W	9.00	Tested	Yes
52000	0.35	0.35	37.09	162548	1/4/1985	970.0	W	12.00	Tested	Yes
0	0	0.25	0.00							
0	0	0.25	0.00							
0	0	0.25	0.00							
35000	0.5	0.5	21.43	STPR on 4727772						
0	0	0.25	0.00							
35000	0.5	0.5	21.43	STPR on 4727772						
35000	0.375	0.375	28.57	STPR on 4727772						
35000	0.375	0.375	28.57	STPR on 4727772						
0	0	0.25	0.00							
35000	0.375	0.375	28.57							
35000	0.375	0.375	28.57							
0	0	0.25	0.00							

Attachment 2

Line 101 and Line 132-A MAOP Validation Report

DRAFT

January __, 2011

Draft subject to revision.

MAOP Validation Report

Executive Summary

The MAOP Validation Study reviewed all available design and test records for Lines 101 and 132A in the San Francisco Peninsula. The review enabled PG&E to create a database covering all pressurized mainline components, including pipe, valves, fittings, taps, tees and other appurtenances. Additionally, this database was used to confirm pipeline stress levels at established MAOPs (Maximum Allowable Operating Pressures) and ensure compliance with Class Location requirements in the Federal Code.

Where there are unknowns we have based recommendations on industry practice and sound engineering judgment. Thus, for example, there are a number of pipeline fittings in L-101 and L-132A for which PG&E has not been able to identify full specification. Consistent with the procedures described in ASME B31.8S and PG&E's regular practice, this analysis assumed conservative values where design standards were not fully known. Based upon these conservative assumed values, and PG&E design and construction standards, these fittings are all operating within their design limits, pressure rating and Class Location restrictions.

MAOP Validation Report

1. PURPOSE AND SCOPE

The purpose of this report is to document the Maximum Allowable Operating Pressure (MAOP) Validation Project for the San Francisco Peninsula Pipeline. This draft report covers L-101 and L-132A.

2. SYSTEM DESCRIPTION

L-101:

Line 101 runs from Milpitas Terminal to the San Francisco Gas Load Center. From Milpitas Terminal to San Francisco Airport Tap, the pipeline currently has an MAOP of 400 psig and from the San Francisco Airport Tap to Lomita Park Regulator Station it has an MAOP of 396 psig. The pressure is reduced at Lomita Park to 145 psig (the downstream MOP).

When evaluating L-101, we collected data for the portion of Line 101 that runs from Milpitas Terminal to Lomita Park Border Meter Station, which is 35.1 Miles (185,319 feet) in length. It consists of 20, 24, 30, 34, and 36-inch diameter pipe. Line 101 was originally installed as a 20 inch line in 1929 from Milpitas to San Francisco and operated at less than 275 psi. This is the oldest of the three main pipelines on the Peninsula. However, all portions of the original 1929 pipe have been replaced. The portion of the pipeline from Milpitas (MP 0.00) to Rengstorff Station (MP 9.78) was replaced with 34" and 36" pipe and upgraded to 400 MAOP in 1965. The remainder of the pipeline from Rengstorff Station (MP 9.78) to Lomita Park (MP 33.68) was updated to the current MAOP of 396 psig in 1989. This line generally lies close to the San Francisco Bay in flat ground. The pipeline runs along a right-of-way that roughly follows State Highways 237 and 101.

L-132A:

Line 132A is a pipeline that cross ties Line 101 to Lines 109 and 132. It is 1.5 miles (7,739 ft) long. The MAOP of the pipeline is 400 psig. The pipeline was originally installed in the 1940s. It consists of 12, 16, and 24-inch diameter pipe and lies in flat ground generally along Rengstorff Avenue in Mountain View.

3. DEFINITIONS

Item	Definition
Maximum allowable operating pressure (MAOP)	The maximum pressure at which a pipeline, pipeline segment, or component is qualified to operate in accordance with the requirements of 49 CFR Part 192 based on the design pressure of the weakest element in a pipeline segment. (Ref 8)

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Maximum operating pressure (MOP)	The maximum pressure a gas pipeline system may operate in accordance with the requirements of 49 CFR Part 192 definition of maximum allowable operating pressure for a system . (Ref 8)
OD	Outside Diameter
Specified minimum yield strength (SMYS)	The minimum yield strength in pounds per square inch (psi) prescribed by the specification under which pipe is purchased from the manufacturer or as specified in 49 CFR Part 192. (Ref 8)
Transmission line	A pipeline other than a gathering line, that: 1. Transports gas from a gathering line or storage facility to a distribution center, storage facility, or large volume customer that is not downstream from a distribution center; or 2. Operates at a hoop stress of 20 percent or more of SMYS; or 3. Transports gas within storage field as defined in 49 CFR Part 192.3, "Definitions." Note: A large volume customer may receive similar volumes of gas as a distribution center, and includes factories, power plants, and institutional users of gas. (Ref 8)
Uprate	The process for increasing the MOP or MAOP (uprating) for pipelines according to the requirements of 49 CFR Part 192, Subpart K, "Uprating." (Ref 8)
WT	Wall Thickness of the pipe or fitting.

4. DATA GATHERING

The installed pipe properties and post installation hydrostatic testing data were gathered and reviewed by following a modified process for creating a Pipeline Feature Lists (PFL). PG&E modified that process to address the unique nature of this project and expedited time line. The original process is detailed in "Procedure for Completing Pipeline Features List (PFL) for In-line Inspection Projects", (Ref 1) which was developed for use during the Pre-assessment phase of In-Line-Inspection projects in order to document all known features and define the scope for future pipe changes prior to pigging.

Specifically the following additional items were collected and incorporated into the PFL spreadsheets, along with the items specified in the PFL procedure, in order to allow for a calculation of operating stress for all mainline components.

- Sleeve – Wall thickness and grade
- Bend – Grade
- Tee – Grade
- Reducer – Wall thickness and grade

The pipeline data available in the GIS (Graphical Information System) system was downloaded into a spreadsheet format to form the basis or starting point for the PFL

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spreadsheets. It bears mention that the GIS system only contains information about the main line pipe segments themselves. In contrast, the PFL includes all elbows, reducers, tees, mainline valves, taps, valves, casings and any other individual components or “features” that make up the gas pipeline. Also, please note that in PG&E’s GIS system, setting a value to a negative amount designates that it is an “assumed” value. For example, an assumed value of 0.281 wall thickness for the pipe would be displayed in GIS as “-.281”. Assumed values are conservative values for pipe wall thickness, grade, yield strength or seam type that are based upon minimum pipe specifications purchased by PG&E in the year or era that any given pipe section was originally installed, but for which records do not exist or were not readily available when the GIS system was created in the late 1990s.

Original construction job files were gathered from the following locations:

- San Jose Division
- De Anza Division
- Peninsula Division
- Bayshore & Geneva Records Center
- Walnut Creek GT&D Records Center

These job files were manually reviewed for relevant information. The records for a single construction project were then consolidated, reviewed by an independent two-person team, and entered into the PFL (Pipeline Features List) spreadsheet. The completed spreadsheet was then printed out and manually reviewed again by another two-person team. The corrections identified were made to the PFL and then reviewed a 3rd time. In some areas, the data was reviewed more than three times. This information was used to generate a “discrepancy list” of changes or differences between the PFL data and the original GIS data. Information consolidated onto the discrepancy list was input back to the GIS system. It is important to note that if pipe characteristics could not be verified in the PFL review, they were marked as “unknown”, but if the value existed in GIS and the PFL indicated it was “unknown”, the GIS value was not changed. While the value could not currently be validated, PG&E assumed that the value that existed in GIS originated from a source document that is not currently available.

During the creation of the PFLs, the Strength Test Pressure Reports (STPR) were gathered for all available construction jobs and matched up to the PFL and GIS data. This information was accumulated in a spreadsheet and compared using the job numbers, STPR drawings, pipe size, pipe grade, pipe wall thickness, seam type and approximate footage. The majority of the Strength Test Pressure reports were completed as part of the initial construction process, but some test reports were for later testing and uprating projects. This STPR information will also be incorporated into GIS as part of the GIS Validation portion of this project.

5. DATA INTERPRETATION AND EVALUATION

The resultant data was evaluated to confirm the pipeline components were operating within the percent of yield strength as required by 49 CFR Part 192 based on their Class Location. Thus, after completion and verification of the PFL and STPR data,

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an additional evaluation was performed in order to assign Joint Factors to long seam types, and to calculate the percent stress at a given pressure level.

The STPR data from the most recent records review was added to the spreadsheets. The “STPR Status” column spreadsheet indicates the status of strength test documentation, based on reconciliation of available data with PFL and GIS pipe segments. The following three categories were identified, and each pipe segment was assigned to one of these three categories:

STPR Status	Definition
Tested	<p>“Tested” indicates either of the following scenarios:</p> <ol style="list-style-type: none"> 1) Completed strength test documentation was found and verified that matches segment, footage, and pipe specification (O.D., wall thickness, grade, long seam). 2) This category includes pipe installed prior to State or Federal Code implementation (pre-1961 pipe) that was not tested when originally installed, but was later tested on an uprate job, for which completed strength test documentation was located and verified.
Incomplete	<p>“Incomplete” indicates any of the following scenarios:</p> <ol style="list-style-type: none"> 1) Completed strength test documentation was found that matches other segments or pipe specifications for a given job number, but not for the given segment. (e.g. If a completed STPR is available for the 24” X -60 DSAW 0.312” wall pipe but not for the 24” X-52 DSAW 0.312” pipe on the same job, then the X-52 segments would be listed as “incomplete”.) 2) GIS shows strength test data, but no completed strength test documentation was found. This is the case for some post-1961 jobs which likely were tested but no test records were found during this validation process. 3) This category includes incomplete reports with design criteria but no actual test data.
Untested	<p>No strength test documentation has been located and there is no evidence that any strength testing was conducted. This is generally the case for pre-1961 jobs, prior to State or Federal requirements for strength testing that were not tested later as part of an uprate.</p>

Figure 1 - STPR Status Definitions

The calculation of the pipeline and fitting stress level occasionally encountered “unknown” grades and wall thicknesses that required further review and evaluation. PG&E resolved all “unknown” pipe specifications either through additional records integration or through excavation/inspections. Joint factors as described in Gas Standard A-11 were utilized. For the purposes of fitting stress calculations the PG&E standards applicable to a given era were used. The results of this evaluation for each of the Peninsula Pipelines are described below.

5.1.1. Line 101

All pipeline and fittings in L-101 south of MP 32.17, Millbrae Ave, were confirmed to be operating at less than 50% of SMYS. This conforms with any Class Location up to Class 3. There are no Class 4 sections on this pipeline between Milpitas and Lomita Park Station.

The detailed review of L-101 documentation indicated that approximately 2,448 feet of re-conditioned pipe was installed at two locations between MP 32.17 Millbrae

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Avenue and MP 33.6 Lomita Park Station. PG&E excavated and verified the pipe to be 20" outside diameter x 0.250" wall thickness. The pipe was manufactured by A.O. Smith at 33,000 psi- minimum yield strength or greater.

PG&E confirmed the yield strength of this pipe using the following sources of information: 1) PG&E letter dated December 12, 1962 entitled "History of Pipe Purchases," documenting the purchase of pipe for several pipelines installed in 1929/1930 as having a minimum yield strength of 33,000 psi; 2) The establishment of a 396 psig MAOP following the 1989 uprate: The only possible value for yield strength in the design equation from 49 CFR 92.105 for 20" pipe with .0.250" WT and a 0.80 JT factor in a Class 3 area (operating one class out) is 33,000; 3) PG&E Gas Standard A-11 which indicates that all pipe purchased by PG&E between 1927 and 1930 in 20" or larger diameter had a minimum yield of 33,000; 4) Industry experience based on sample yield tests of 1930 era A.O. Smith pipe provided by Kiefer and Associates as-well-as DNV consultants; and 5) Field measures of yield strength values at two dig sites on the re-conditioned pipe using Advanced Technology Corporation's Automated Ball Indentation technique, confirming a yield of not less than 46,000 psi.

The longitudinal seam of this pipe corresponds to a joint factor of 0.8. Utilizing the data above results in a maximum pipeline pressure of 330 psi at 50% specified minimum yield strength (SMYS) and 396 psig at 60% SMYS. This pipeline was strength tested for eight hours on October 10, 1989 at 650 psig and thus qualified under 49 CFR 192.611 to operate up to 396 psig. In this situation the pipeline is operating, "one class location out" based on the 1989 hydrostatic test as allowed under 49 CFR192.611.

PG&E performed five excavations at MP 2.45, MP 2.49, MP 2.54, MP 10.40 and MP 19.99 in order to validate the pipeline seam type. All of the pipeline segments were confirmed to be DSAW pipe using a combination of radiography, visual examination and ultrasonic examination. Additionally, at MP 10.40, the pipeline was taken out of service and camera inspected for approximately 400 feet to confirm that it was DSAW pipe.

Analysis of the fittings on the pipeline revealed 11 fittings (sleeves, bends or reducers) that were assigned unknown value to at least one of the fitting properties necessary for stress calculations. These 11 fittings were installed in 1963 and 1965. Available job documents do not contain enough information to verify the grade or wall thickness of the fitting. PG&E Gas Standards in place at the time of construction refer to B31.1 and API 5LX and state that the fittings should match the pressure rating of the pipe. Therefore, facilities built to the PG&E Standards would not be operating over 50% SMYS at 375 psig.

There are complete hydrostatic test records for approximately 34.47 miles (98.2%) of pipe in Line 101. Another 0.45 miles (1.3%) of pipe has "incomplete" hydrostatic test records, as test reports could not be definitively matched to the specific pipeline segments, (see definition of "incomplete" above), leaving approximately 0.18 miles (0.5 %) of the pipeline that was installed in 1957, prior to State or Federal Code mandating pressure testing. The minimum hydrostatic test pressure, for the segments with records, is 605 psig or 1.51 times the 400 psig MAOP. All of the pipe

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footage that has not been post construction hydrostatically tested is 34 inch DSAW from Job Number 137560 installed in 1957 and located near Mile Point 2.5.

5.1.2. Line 132A

PG&E confirmed that all pipeline segments and fittings in L-132A were operating at less than 50% of SMYS and thus were commensurate with any class location up to Class 3. There are no Class 4 locations on this pipeline. Additionally, although the 1944 and 1947 segments in this pipeline were not hydro-tested due to its era of construction, this pipe is seamless, based on the original purchase documentation, and thus not subject to the manufacturing threats associated with welded seams in other pipelines of this time.

Analysis of the fittings revealed nine fittings (sleeves and bends) that were assigned unknown values to at least one of the fitting properties required to calculate stress. Two of these fittings are sleeves installed in 1981. PG&E Gas Standards in effect at this time required the wall thickness be a minimum of 0.375. This results in a stress level of 34% of SMYS. The remaining elbows were installed with the original pipe in 1944. The PG&E Gas Standards from 1945 (one year after installation of this pipe) indicate that elbows would be 0.375 wall thickness. However available documentation from the job indicates these are probably bell -end segments that are mostly likely the wall thickness of the pipe and made from similar material. Using the wall thickness of the pipe, 0.281 (the more conservative value), the stress level in these elbows would be 46% of SMYS at 375 psig.

There are complete hydrostatic test records for 0.55 miles (37%) of pipe in Line 132A. Another 0.039 miles (3%) have "incomplete" strength test pressure reports and 0.88 miles (60%) have no hydrostatic test data. All of the un-tested pipe is seamless. All of the pipe footage that has not been post construction hydrostatically tested is 24 and 16 inch seamless pipe from job number 73429 installed in 1944 and job number 85737 installed in 1947.

Appendix– Reference Sources

	Name of Document	Date / Revision	Description	Author / Approval
1	Procedure for Completing Pipeline Features List for In-line Inspection Projects	3 Dec 2009 Revision # 3	Document describes the process of downloading information from GIS and reviewing records to establish a list of features.	Frank Dauby Approved by Frank Dauby 4 Dec 2009
2	Historical Gas Pipe Minimums	17 Feb 2000	Written by 2 long time PG&E engineers to document historical pipe minimums. Note Gas Standard A-11 addresses Joint Factors.	Bill Harris Bob Becken
3	Gas Standard A-11 Drawing Number 085053	9 Jan 1970 Last Revision 5 Feb 1976	Describes how to identify different types of gas pipe. Includes joint factors for longitudinal seams on the last page.	Full names not clear. Approved using initials only.
4	Welding Sleeves for Steel Gas Mains Drawing Number 081439 MS-1102	4 Jan 1945	Document lists specifications for welding sleeves. Including Minimum thickness for various sizes up to 26 inch diameter pipe. Minimum tensile strength 60,000 psi.	Full names not clear. Approved using initials only.
5	Gas Standard A-60 Gas Main Welding Sleeves Drawing Number 283226	26 Mar 1968 Last Revision 18 May 1971	Lists specifications for welding sleeves. Grade must be equal or greater than carrier pipe. Wall thickness not less than .375 and equal or greater than carrier pipe.	R.E. Dyas on original issue. Later revisions initialed.
6	Gas Standard A-60 Gas Main Welding Sleeves Drawing Number 283226	26 Mar 1968 Last Revision 18 May 1976	Lists specifications for welding sleeves. Grade must be equal or greater than carrier pipe. Wall thickness not less than .375 and equal or greater than carrier pipe. Recommended 1.2 times carrier wall thickness.	R.E. Dyas on original issue. Later revisions initialed.
7	Gas Standard A-60 Page 8 Drawing Number 088312	Last Revision 15 Jun 1990	Lists specifications for welding sleeves. Grade must be equal or greater than carrier pipe. Wall thickness calculated by formula, generally 1.42 times carrier wall thickness.	Full names not clear, Revisions initialed.

8	Utility Standard WP 4125S Establishment of MAOP for gas pipelines	March 2010	Describes the standards defining the establishment and maintenance of MAOP and MOP information for gas pipelines	Todd Arnett.
9	Line Pipe Manufacturing in North America	CRTD- Vol 43	ASME research report prepared by Kiefner and Associates for the Gas Pipeline Safety Research Committee	J. F. Kiefner E.B. Clark
10	Integrity Characteristics of Vintage Pipelines	2005	Describes how the technical information on vintage pipelines may be used to comply with ASME B31.8S, created under contract to the Interstate Natural Gas Association of America.	Battelle Memorial Institute
11	Gas Standard Drawing 081465	8-8-1945	Gives standard sizes, dimensions and properties for 45 degree long radius elbows	Signed and approve with initials.
12	Gas Standard Drawing 281992	10-8-1952	Gives standard sizes, dimensions and properties for 90 degree long radius elbows	Signed and approve with initials.
13	Gas Standard Drawing 283158 MS 1051	9-20-1962	Gives standard sizes, dimensions and properties for 90, 45 degree elbows. Tees and reducers	Signed and approve with initials.
14	Gas Standard MS 1050	6-1-1964	Gives standard sizes, dimensions and properties for tees	Signed and approve with initials.
15	PG&E Letter “History of Pipe Purchases”	12-12-1962	Describes the PG&E pipe purchases from 1920s through 1962 in order to identify unknown pipe.	R.D. Smith, Manager of Gas System Design Dept.

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