



September 29, 2011

Project No. 121627

Pacific Gas & Electric Company
 Geosciences
 245 Market Street, Mail Code N4C
 P.O. Box 740000
 San Francisco, California 94177

Attention: Redacted

SUBJECT: Geotechnical Evaluation (Update 1)

Pacific Gas and Electric Company
Gas Transmission Line 132 Redacted
South San Francisco, California

Dear Redacted

Per your request, Kleinfelder evaluated liquefaction hazard near the existing Pacific Gas & Electric Company (PG&E) Gas Transmission Line 132 in the vicinity of Redacted Redacted in South San Francisco, California. Our services were authorized by PG&E Contract Work Authorization (CWA) No. 245, dated August 31, 2011.

A letter report of a less extensive evaluation was submitted on September 7, 2011. In response to input from the PG&E design team, the evaluation reported herein expands upon and supersedes the conclusions contained in the September 7 report.

BACKGROUND INFORMATION

We understand that in the vicinity of the Redacted the top of the 30-inch diameter pipeline is about 3 feet below existing grade. A design team including Redacted and others (under separate contract to PG&E) is evaluating the effects of seismically-induced soil liquefaction on the existing pipeline. To support this evaluation, Redacted and PG&E requested that Kleinfelder review available geotechnical information and evaluate the liquefaction hazard along the pipeline alignment in the immediate vicinity of Redacted. PG&E provided the following information for use in our evaluation.

- Photographic map of the pipeline alignment in the immediate vicinity of Redacted Redacted

- Mapped liquefaction hazard, interpreted by PG&E, in the [Redacted] vicinity with the pipeline alignment superimposed. According to PG&E, the liquefaction hazard map is derived from a geographic information system (GIS) database that is published on the Association of Bay Area Governments (ABAG) website. According to the ABAG website, the liquefaction hazard map is based on United States Geological Survey (USGS) Open-File Report Nos. [Redacted]. The PG&E liquefaction hazard map identifies the [Redacted] to be an area of "moderate to high" liquefaction susceptibility.

Kleinfelder's liquefaction hazard evaluation was based on the pipeline information described above and on geotechnical information presented in reports by other consultants. For this assignment, Kleinfelder did not conduct a subsurface exploration and laboratory testing program to evaluate subsurface conditions. Geotechnical information used in our evaluation is contained in the following geotechnical investigation reports prepared by others for the Bay Area Rapid Transit (BART) system extension to San Francisco International Airport (SFO).

- Harding Lawson Associates (HLA, 1999), "Final Design Phase Submittal – Geotechnical Engineering Design Report, BART Extension to SFO – Module 2, Contract 12YC-120, San Mateo County, California," prepared for HNTB Corporation, March 25, 1999.
- Geotechnical Consultants, Inc. (GTC, 1995), "San Francisco Bay Area Rapid Transit District Proposed SFO Extension – Geotechnical Data Report, Segment No. 1," prepared for Bay Area Transit Consultants, January, 1995.

The above-referenced geotechnical reports include boring logs and the results of cone penetration tests (CPTs) conducted along the alignment of the BART SFO extension. As shown on Plate 1, Line 132 roughly parallels the BART SFO Extension along much of its alignment in the vicinity of the [Redacted] with explorations generally located within 50 to 850 feet of the mapped Line 132 location.

ASSUMPTIONS

Key assumptions employed in our evaluation are summarized below.

- The subsurface conditions (soil stratigraphy and groundwater conditions) along the BART SFO Extension alignment, as shown on the subsurface profile drawings in Appendix A and on the boring logs in Appendix B of this report, adequately represent the subsurface conditions along the Line 132 alignment. Note that the explorations (borings and CPTs) conducted for the BART SFO Extension project are widely spaced (generally about 300 to 500 feet apart) and are located up to 850 feet from the mapped location of Line 132 (see Plate 1).

- The reported “design” groundwater depth, shown on the Appendix B subsurface profile drawings, represents a conservative groundwater depth for liquefaction evaluation purposes.

SUBSURFACE CONDITIONS

Subsurface conditions described in this report are based on information contained in the above-referenced 1999 HLA and 1995 GTC geotechnical reports. It should be noted that most of the HLA and GTC explorations considered in our analyses are far enough away from the pipeline such that our evaluation cannot be considered site-specific. As such, our assumptions of similar soil profile are approximate at best.

According to the 1999 HLA report, the [Redacted] at the time of the 1999 reporting was about 8 to 10 feet deep and lined with rip-rap. Currently, the creek channel is lined with concrete.

The 1999 HLA report includes a geologic map of the site that is based on USGS Open-File Report No [Redacted]. This geologic map identifies the mapped zone of “moderate to high” liquefaction susceptibility (from the PG&E map described above) at [Redacted] [Redacted] as Holocene-age alluvial fan deposits, described as “medium dense to dense, gravelly sand or sandy gravel that generally grades upward to sandy or silty clay.”

Generalized subsurface conditions, including stratigraphy and design groundwater depth, are illustrated on the Plan and Profile sheets in Appendix A. The Appendix A Plan and Profile sheets are taken directly from the 1999 HLA report.

In the vicinity of the pipeline crossing, the HLA report describes localized deposits of artificial fill consisting of clay, silt, sand, and gravel that overlie recent alluvial sediments and [Redacte] formation soils. At our analysis locations in the immediate vicinity of the creek crossing, the fill materials are reported to be up to about 5 feet thick. The alluvium is reported to range in thickness from less than a few feet at the mapped margins of the alluvium to 45 to 55 feet and consists of medium dense silty sand, clayey sand, and poorly-graded sand with silt interlayered with medium stiff to stiff fat clay, sandy lean clay and silt. Underlying the alluvium the HLA and GTC borings and CPTs show dense to very dense sands and stiff to very stiff clays of the Colma formation.

Groundwater depths used in our analyses are based on the design groundwater depths reported in the 1999 HLA geotechnical report. At the boring locations used in our analyses, the design groundwater depth generally varies from about 14 to 22 feet below ground surface. The design groundwater level is based on groundwater observations made during drilling and on long-term measurements in standpipe piezometers (observation wells) by HLA. We note that the “design” groundwater depths reported by HLA and as illustrated in Appendix A, are up to 5 to 10 feet higher than the high water level measurements from borings and observation wells reported in the 1999 HLA report.

LIQUEFACTION ANALYSIS METHODOLOGY AND RESULTS

In the past decade, several concentrated efforts have been made to establish a uniform guideline for field-based, simplified liquefaction analyses. Youd et al. (2001)¹ published general guidelines for liquefaction analyses, which presented the consensus of a task committee comprising more than 20 members from all over the country. Subsequent earthquakes in Turkey and Taiwan provided additional data to researchers, especially for low plasticity clays and silts, which resulted in significant modifications to liquefaction evaluation methods, especially for soils with higher fines contents. Two of the most widely used methods have been presented by Seed et al. (2003)² and Idriss and Boulanger (2008)³. Based on the above discussions, liquefaction potential analyses were performed using the methods proposed by Seed et al. (2003) and Idriss and Boulanger (2008) using the standard penetration test (SPT) data and CPT data reported in the 1995 GTC and 1999 HLA reports. It should be noted that these methods of analyses are deterministic in nature and do not address the probability of liquefaction occurring at the site.

In order to perform liquefaction analyses, estimates of earthquake magnitude and peak ground acceleration (PGA) are needed. Using the USGS interactive deaggregation website⁴, a modal earthquake magnitude $M_w = 8.0$ representing a seismic event on the San Andreas fault was estimated and used in the analysis. PGA for our liquefaction analyses was taken as $S_{DS}/2.5$ (0.56g), where S_{DS} was estimated using the USGS Java ground motion parameter calculator⁵ assuming a Site Class D.

The USGS Java calculator is based on USGS 2002 ground motion maps. It should be noted that $S_{DS} = 2/3 \cdot S_{MS}$, where S_{MS} is the spectral acceleration at a period of 0.2 second for the Maximum Considered Earthquake (MCE). According to 2010 California Building Code (CBC), the MCE is defined as the smaller of the probabilistic value and 150% of the median deterministic value from the controlling fault. The probabilistic value corresponds to 2 percent probability in 50 years (return period of about 2,475 years). In order to estimate PGA for other return periods, a site-specific probabilistic seismic hazard analysis (PSHA) should be performed. However, in lieu of site-specific

¹ Youd, T.L., Idriss, I.M. Andrus, R.D. Arango, I., Castro, G., Christian, J.T., Dobry, R., Liam Finn, W.D.L., Harder, L.F., Jr., Hynes, M.E., Ishihara, K., Koester, J.P., Liao, S.S.C., Marcuson, W.F., III, Martin, G.R., Mitchell, J.K., Moriwaki, Y., Power, M.S., Robertson, P.K., Seed, R.B., Stokoe, K.H., II (2001), Liquefaction Resistance of Soils: Summary Report from the 1996 NCEER and 1998 NCEER/NSF Workshops on Evaluation of Liquefaction Resistance of Soils, ASCE, Journal of Geotechnical and Geoenvironmental Engineering, V. 127, No. 10, p 817-833.

² Seed, R.B., Cetin, K.O., Moss, R.E.S., Kammerer, A.M., Wu, J., Pestana, J.M., Riemer, M.F., Sancio, R.B., Bray, J.D., Kayen, R.E., and Faris, A. (2003), "Recent Advances in Soil Liquefaction Engineering: A Unified and Consistent Framework," 26th Annual ASCE Los Angeles Geotechnical Spring Seminar, Long Beach, California, April 30, 2003.

³ Idriss, I. M. and Boulanger, R.W. (2008), "Soil Liquefaction During Earthquakes," Monograph MNO-12, Earthquake Engineering Research Institute, Oakland, California.

⁴ <https://geohazards.usgs.gov/deaggint/2008/>

⁵ <http://earthquake.usgs.gov/hazards/designmaps/javacalc.php>

PSHA, the USGS website for interactive deaggregation may be used for probabilities of exceedance of 1-, 2-, 5-, 10-, 20-, and 50-percent in 30, 50, 75, 100, and 200 years.

Groundwater depths used in our analyses are based on the design groundwater depths reported in the 1999 HLA geotechnical report, and as illustrated in Appendix A. The profile drawings in Appendix A include data from the 1995 GTC report.

The evaluation of liquefaction in response to an earthquake is based on a comparison of a soil's resistance to liquefaction and the cyclic load or demand placed on the soil by the earthquake. A safety factor against liquefaction is commonly defined as the ratio of the cyclic shear stress required to cause liquefaction (cyclic resistance ratio, or CRR) to the equivalent cyclic shear stress induced by the earthquake (cyclic stress ratio, or CSR). Per California Geological Survey Special Publication 117A, if the calculated safety factor against liquefaction (i.e., the ratio CRR/CSR) is less than about 1.3 the soil is considered to be liquefiable for design purposes.

A summary of liquefaction analysis results for PGA = 0.56g is presented in Table 1. The information presented in Table 1 is ordered from north to south, beginning with CPT No. C-16, in the vicinity of the South San Francisco BART station at Sta. 427+90, and ending with C-41, at Sta. 347+75. Table 1 also presents approximate distances from the previous borings and/or CPTs and approximate distance of each boring or CPT from the pipeline. Using the distance between borings/CPTs and difference in total settlements between these borings/CPTs, an estimate of differential settlement over a development length may be estimated.

Table 1. Summary of Liquefaction Settlement Analysis Results (PGA = 0.56g)

Boring or CPT ID	Station (BART SFO Project)	Distance from Previous Exploration (feet)	Approximate Distance from Pipeline 132 (feet) ⁽¹⁾	Exploration Depth (feet)	Liquefiable Depth Interval (feet)	Computed Liquefaction Settlement (inches) and Computed Safety Factor ⁽³⁾
C-16 427+90		--	Not parallel to pipeline	30 ⁽²⁾	18.5 – 21.5 24.5 – 26.5	2" to 3" (FOS < 0.5)
B-15 425+00 140			Not parallel to pipeline	51.5	17 – 23.5	1" to 2" (FOS < 0.5)
B-107 423+80 120			Not parallel to pipeline	61	20 – 23	≤ 1" (FOS < 0.5)
C-24 421+60 220			Not parallel to pipeline	25	--	nil
B-18 421+40		20	300 (L)	81.5	17.5 – 18.5 33.5 – 38	1" to 2" (FOS < 0.5)
C-27 417+80 360			250 (L)	20	--	nil
B-23 414+50 330			200 (L)	51	17 – 21	1" to 2" (FOS < 0.5)
C-29 411+80 270			200 (L)	42	26 – 28 34 – 36	2" to 3" (FOS < 0.5)
B-24 408+25 355			250 (L)	50.5	33 – 40	1" to 2" (FOS < 0.5)
C-30 404+90 335			300 (L)	25	18 – 21	≤ 1" (FOS < 0.5)
C-31 401+75 315			400 (L)	50	19 – 21 30.5 – 31.5 37.5 – 49	3" to 5" (FOS < 0.5)
B-25 401+65		10	400 (L)	51.5	18 – 21.5 25 – 35	2" to 4" (FOS < 0.5)
C-32 398+00 365			450 (L)	50	18 – 21 42 – 43.5	2" to 3" (FOS < 0.5)
B-26 395+00 300			450 (L)	81.5	20 – 26 30.5 – 34	2" to 4" (FOS < 0.5)
B-202 391+90 310			400 (L)	61	20 – 26 40 – 44	1" to 2" (FOS < 0.7)
B-27 388+30 360			300 (L)	51	--	nil

Boring or CPT ID	Station (BART SFO Project)	Distance from Previous Exploration (feet)	Approximate Distance from Pipeline 132 (feet) ⁽¹⁾	Exploration Depth (feet)	Liquefiable Depth Interval (feet)	Computed Liquefaction Settlement (inches) and Computed Safety Factor ⁽³⁾
B-28 38	2+80 550		150 (L)	51	--	nil
C-36 37	9+10 370		< 50	50	21.5 – 25 29 – 33 39.5 – 44 46.5 – 49.5	2" to 6" (FOS < 0.5)
B-29 37	5+30 380		< 50	70	28.5 – 33.5 43.5 – 46.5	2" to 3" (FOS < 0.5)
C-37 37	1+50 380		200 (R)	50	32 – 36 44.5 – 46	1" to 2" (FOS < 0.5)
B-30 36	6+90 460		450 (R)	51.5	--	nil
B-203 364+00	290		600 (R)	56	24 – 28 46.5 – 49	1" to 2" (FOS < 0.8)
B-31 35	8+85 515		850 (R)	515	--	nil
C-39 35	8+65	20	850 (R)	29	--	nil
C-40 355+50	315		Not parallel to pipeline	26	16 – 15	≤ 1" (FOS < 0.5)
B-204 354+00	150		Not parallel to pipeline	60.5 16.5 – 27.5		3" to 4" (FOS < 0.5)
B-32 350+30	370		Not parallel to pipeline	51.5	--	nil
C-41 347+75	255		Not parallel to pipeline	38	32 – 37	≤ 1" (FOS < 0.5)

Notes on Table 1:

- (1) Approximate horizontal distance from pipeline alignment. Offset noted in left (L) or right (R) direction. See Plate 1 for locations.
 (2) Exploration does not fully penetrate alluvium.
 (3) Factor of safety against liquefaction triggering.

Based on our analyses, granular alluvial soils below the design groundwater level tend to be susceptible to liquefaction in the event of the earthquake scenario described above. At a given location along the pipeline alignment the total thickness of granular alluvium is expected to vary. At the HLA and GTC exploration locations that we analyzed, we estimate that up to 2 to 6 inches of total liquefaction-induced settlement can be expected during the earthquake scenario described above. In general,

depending on the pipe location, the differential settlement due to liquefaction could be on the order of 1 to 4 inches over 50 feet. At some locations such as B-18 and C-24, the differential settlements are up to about 2 inches over 20 feet. Similarly, differential settlement between C-31 and B-25 is about 1 inch for 10 feet. Our estimates are based on site conditions and the design groundwater elevations as reported in the 1999 HLA report.

As noted in Table 1, where liquefiable soils are identified for PGA = 0.56g the computed factor of safety against liquefaction is usually less than about 0.5. To investigate the effect of lower PGAs on liquefaction triggering and computed liquefaction settlement, we compared the results of our analyses with PGA = 0.56g at selected locations to analysis results for PGA = 0.2g and PGA = 0.4g. The results of these analyses are summarized below in Table 2.

Table 2. Comparison of Liquefaction Settlement with Variable PGA at Selected Locations

Boring or CPT ID	Station	PGA = 0.56g		PGA = 0.4g		PGA = 0.2g	
		Computed Settlement (inches)	Factor of Safety	Computed Settlement (inches)	Factor of Safety	Computed Settlement (inches)	Factor of Safety
C-31 401+75		3" to 5" < 0.5	3" to 5" < 0.5	2" to 4" < 0.5	2" to 4" < 0.7		
B-25 401+65		2" to 4" < 0.5	2" to 4" < 0.5	1" to 4" 0.5 to 1.1	1" to 4" 0.5 to 1.1		
B-26 395+00		2" to 4" < 0.5	2" to 4" < 0.5	1" to 2" 0.5 to 1.0	1" to 2" 0.5 to 1.0		
B-29 375+30		2" to 3" < 0.5	2" to 3" < 0.5	1" to 3" 0.5 to 0.8	1" to 3" 0.5 to 0.8		
B-204 354+00		3" to 4" < 0.5	2" to 4" < 0.6	1" to 2" 0.5 to 0.9	1" to 2" 0.5 to 0.9		

Based on the results presented in Table 2, the computed safety factor against liquefaction triggering and computed range in liquefaction settlement is largely unchanged when PGA is reduced from 0.56g to 0.4g. However, for PGA = 0.2g the computed safety factor begins to approach or exceed 1.0, and the corresponding liquefaction settlement is reduced.

As noted above, at the locations of our analyses the design groundwater depth generally varies from about 14 to 22 feet below ground surface. Liquefaction hazard is not a design issue at depths above the design groundwater depth. If the Redacted channel invert is 8 to 10 feet deep in the vicinity of the pipeline crossing, as described above, then the top of liquefiable soils is estimated to be 8 to 11 feet below the channel invert. We consider this depth interval to be too great for lateral spreading caused by liquefaction to occur.

LIMITATIONS

This work was performed in a manner consistent with that level of care and skill ordinarily exercised by other members of Kleinfelder's profession practicing in the same

locality, under similar conditions and at the date the services are provided. Our conclusions, opinions, and recommendations are based on a limited number of observations and data reported by Geotechnical Consultants, Inc. in 1995 and Harding Lawson Associates in 1999. It is possible that conditions could vary between or beyond the data evaluated. Kleinfelder makes no other representation, guarantee, or warranty, express or implied, regarding the services, communication (oral or written), report, opinion, or instrument of service provided.

The borings and CPTs used in our analyses were conducted 13 to 17 years ago and anywhere from about 50 to over 800 feet away from the pipeline alignment. Kleinfelder makes no warranty as to the applicability or usefulness of the information from the 1995 GTC and 1999 HLA reports for the purposes of the pipeline study. Kleinfelder recommends that the analyses and conclusions developed during this study be confirmed with site-specific subsurface information collected during a subsurface exploration and laboratory testing program directed toward evaluating liquefaction along the pipeline alignment.

ATTACHMENTS

The following are attached and complete this report:

- Plate 1, Site Plan
- Appendix A, Plan and Profile Sheets by HLA (1999).
- Appendix B, Boring Logs and CPT Results by GTC (1995) and HLA (1999)

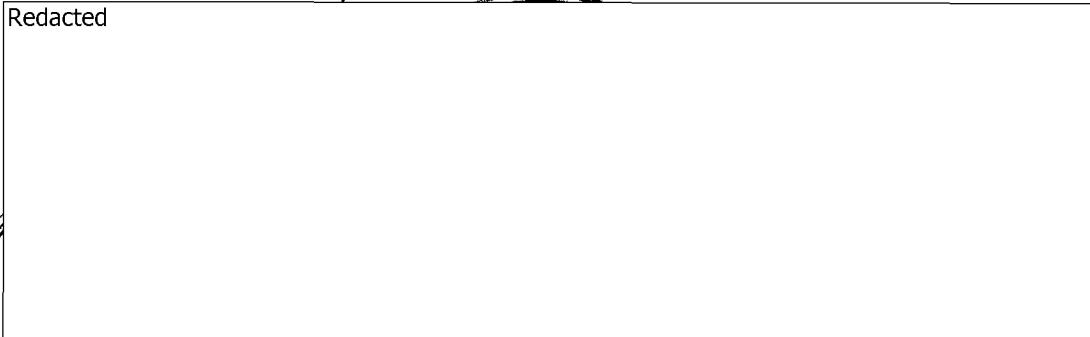
CLOSING

We appreciate the opportunity to be of service to PG&E on this project. If you have questions regarding this report, or if we may be of further assistance, please contact the undersigned.

Sincerely,

KLEINFELDER WEST, INC.

Redacted



Redacted



PLATES

Redacted

APPENDIX A
PLAN AND PROFILE DRAWINGS FROM HLA (1999) REPORT

Redacted

Redacted

Redacted

Redacted

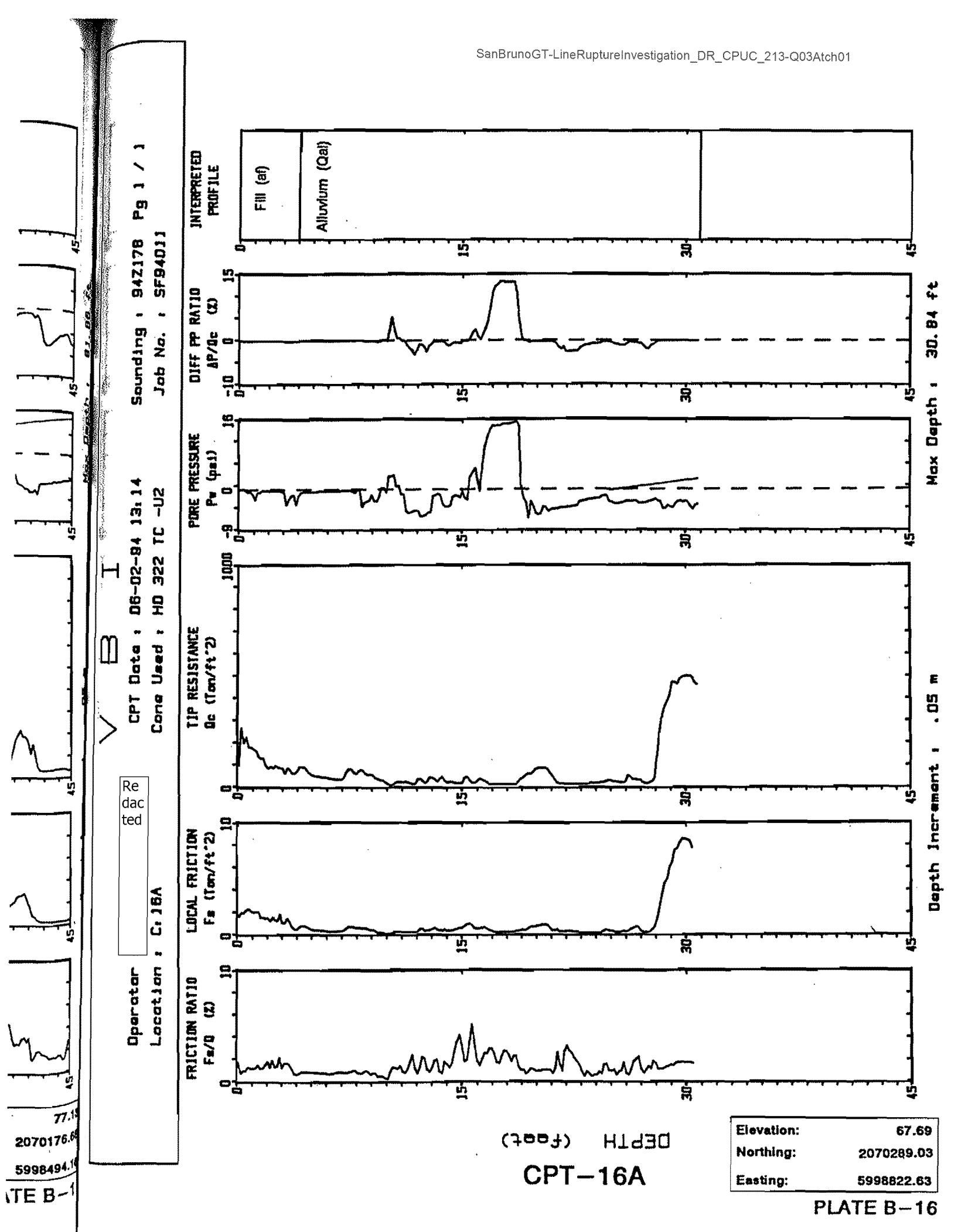
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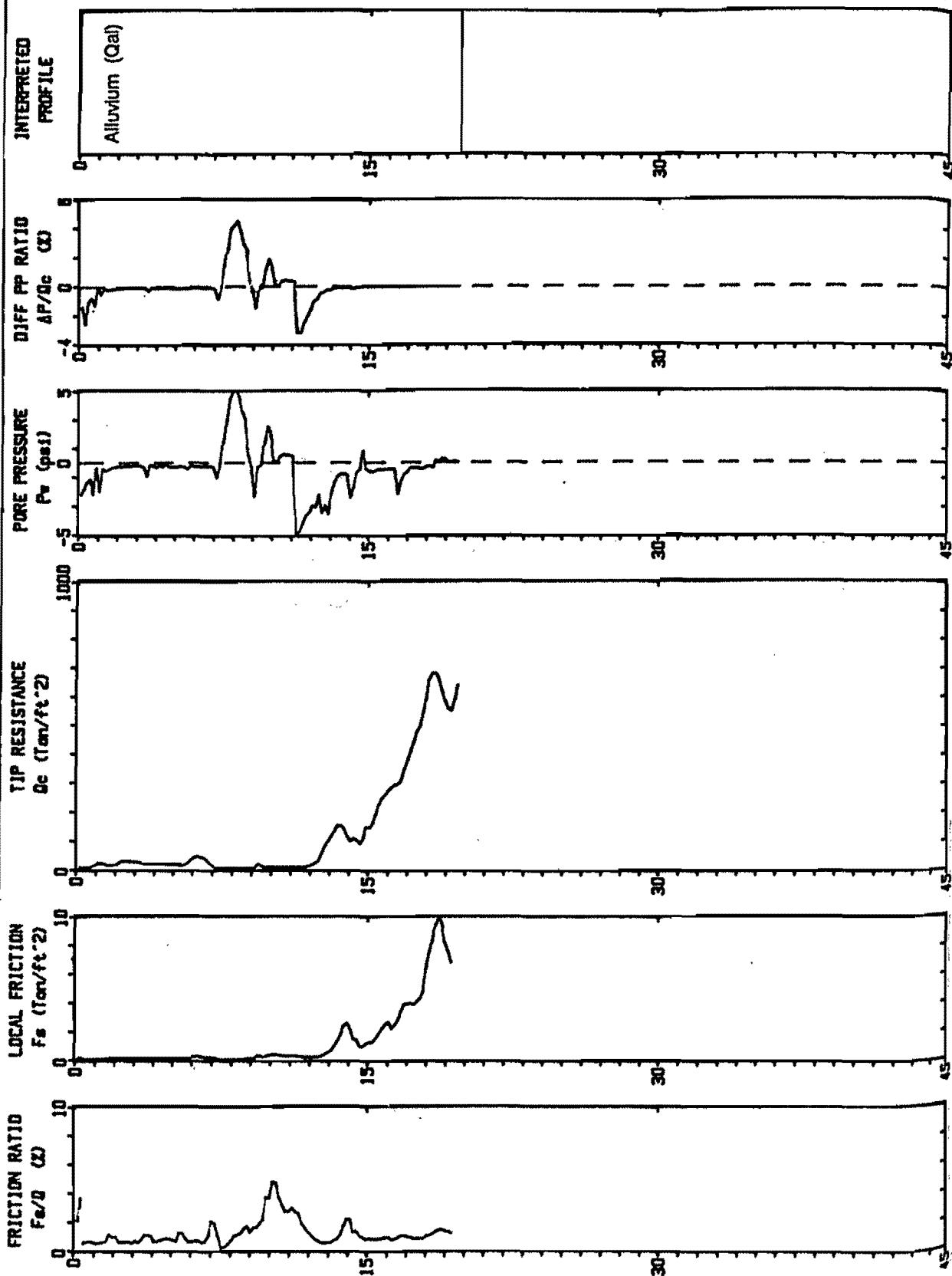
APPENDIX B

LOGS OF BORINGS AND CPTs FROM GTC (1995) AND HLA (1999) REPORTS



77.1
 2070176.6
 5998494.1
 SITE B-1

Operator : Redacted
 Location : C-17
 CPT Date : 05-27-94 12:11
 Cone Used : HD 322 TC -U2
 Job No. : SF84011
 Sounding : 84Z152 Pg 1 / 1



DEPTH (ft)

CPT-17

Elevation:
 Northing:
 Easting:

Redacted

PLATE B-

Operator : Redacted
 CPT Date : 06-01-94 14:57
 Cone Used : HD 322 TC -U2
 Job No. : SF84011
 Sounding : 84Z171 Pg 2 / 2

LOG OF DRILL HOLE

San Bruno Gas Line Rupture Investigation_DR_CPUC_213-Q03Atch01

040II

Line Break Extension

Redacted

LOGGED BY: Redacted

CHECKED BY:

DRILL HOLE NO.: B-15

DRILLING DATE: May 16, 1994

ELEVATION: 64.70 feet

DATUM: NGVD

METHOD: 4 7/8" diameter Rotary Wash with cathead

DEPTH (FT)	BBL COUNT	TORVANE SHEAR STRENGTH (PSF)	POCKET PENETROMETER COMP. STRENGTH (TSF)	PHOTOVAC TIP READING (PPM)	GRAPHIC LOG	GEOTECHNICAL DESCRIPTION AND CLASSIFICATION	ATTERBERG LIMITS		UNCONFINED SHEAR STRENGTH (PSF)	ADDITIONAL TESTS	
							DRY DENSITY (PCF)	MOISTURE CONTENT (%)	LIMIT (%)	PLASTIC LIMIT (%)	
6						"ARTIFICIAL FILL (at)" POORLY GRADED SAND with silt (SP-SM) brown, dry to damp, loose, layer of gravel at 6-inches, fine to coarse grained.					
12						"ALLUVIUM (Qa)" SILTY SAND (SM) brown, moist, medium dense, 20% fines.	97	17			
7						"ALLUVIUM (Qa)" CLAYEY SAND (SC) dark brown, wet, loose, with organics.	98	25			
5	0.8					"ALLUVIUM (Qa)" SANDY LEAN CLAY (CL) black, moist to wet, medium stiff.	19	25	14		
6	1.0					"ALLUVIUM (Qa)" SANDY LEAN CLAY to CLAYEY SAND (CL/SC) dark brown, moist to wet, loose sand to medium stiff to stiff clay.				Corr	
8						"ALLUVIUM (Qa)" CLAYEY SAND (SC) dark gray to bluish-gray, moist lenses of gray-blue, fine gravel, fine grained sand, loose, 34% fines.				GS	
8	.75					"ALLUVIUM (Qa)" LEAN CLAY (CL) black, moist, medium stiff with blue-green speckles.	24	43	15		
80/11"						"ALLUVIUM (Qa)" SANDY LEAN CLAY to CLAYEY SAND (CL/SC) dark gray to black moist medium stiff to loose, fine grained sand.	124	13			
86/10"						Redacted					
71						SILTY SAND (SM) light gray, moist, very dense, fine grained sand, some gravel.					
63						Fine gravel and coarse sand at 32 feet.					
82						Redacted					
						POORLY GRADED SAND with silt (SP-SM) light gray, very moist, very dense, medium to fine grained sand, some black veins and occasional red stains.					
						"COLMA FORMATION (Qc)" SILTY SAND (SM) orange-brown, moist, very dense, weakly cemented.					
						Light orange-brown at 46 feet.					
						Orange-brown with black speckles and dark orange bands, 2-inch layer of sandy lean clay (CL) light gray.					
						Bottom of drill hole at 51 1/2 feet. No water measured to a depth of 45 feet on 6/13/94. Installed piezometer. Perched groundwater measured at 18.3 feet in adjacent Auger boring on Sept. 15, 1994, after 24 hours.					

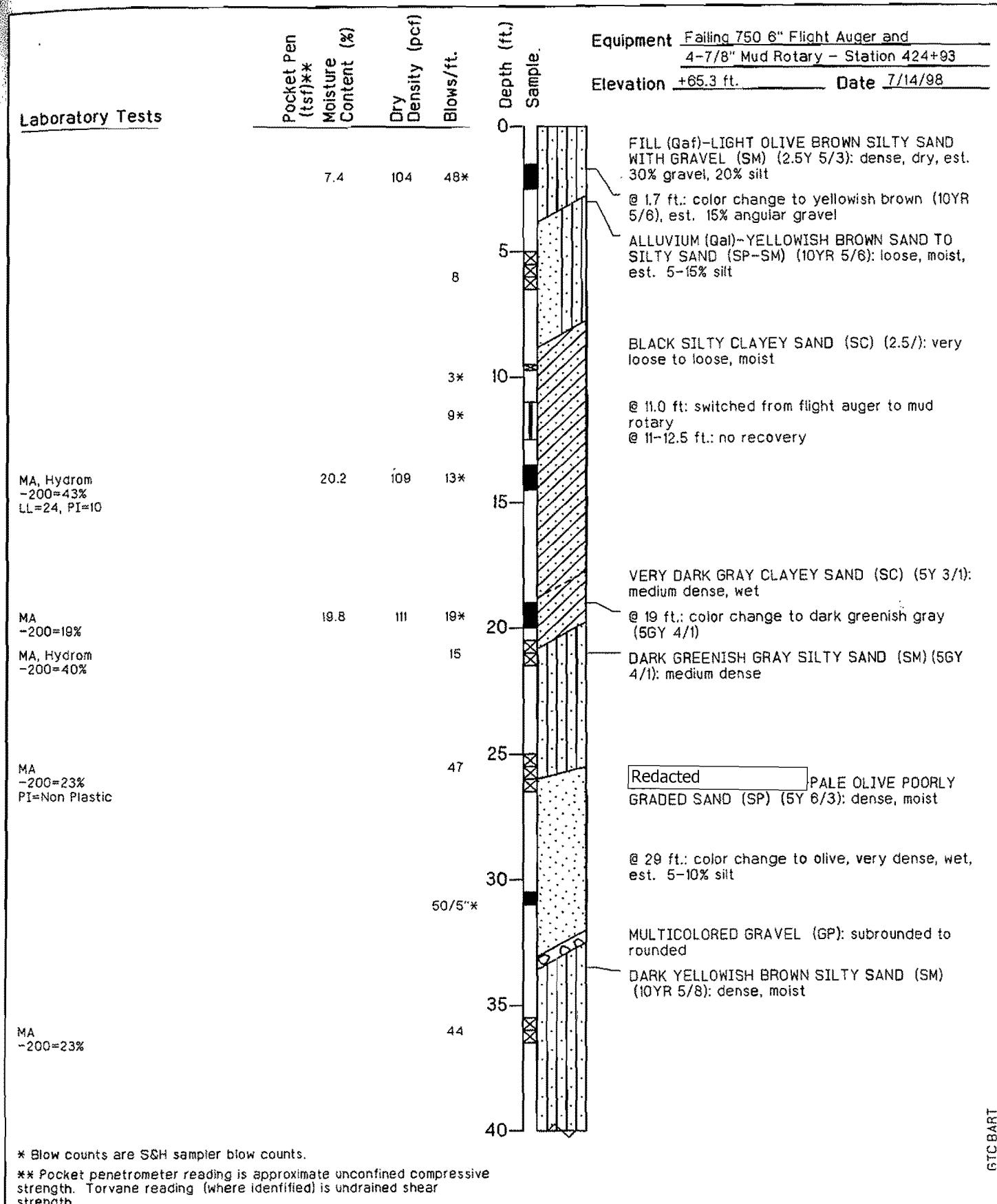
ATE A-2

HEET 1 of 1

boring on Sept. 15, 1994, after 24 hours.

LEGEND TO LOGS ON PLATE A-10

PLATE A-2.15



Herding Lawson Associates
Engineering and Environmental Services

DRAWN
CEG

JOB NUMBER
40646 3E

Log of Boring B-107

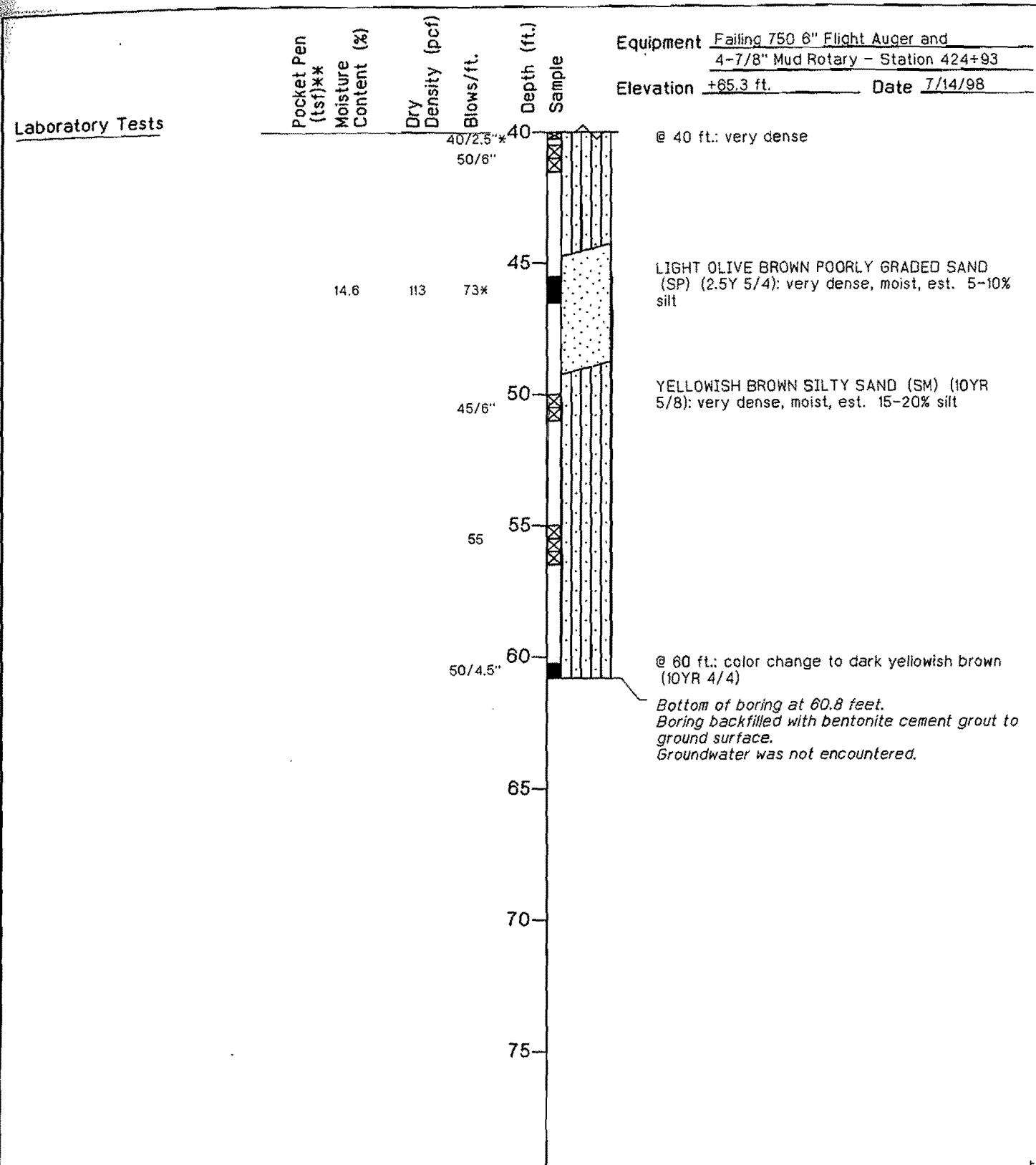
Module 1 - BART Extension to SFO
San Mateo County, California

APPROVED

DATE
8/98

A-7

REVISED DATE



* Blow counts are S&H sampler blow counts.

** Pocket penetrometer reading is approximate unconfined compressive strength. Tovane reading (where identified) is undrained shear strength.



Harding Lawson Associates
Engineering and
Environmental Services

DRAWN
CEG

JOB NUMBER
40646 3E

Log of Boring B-107

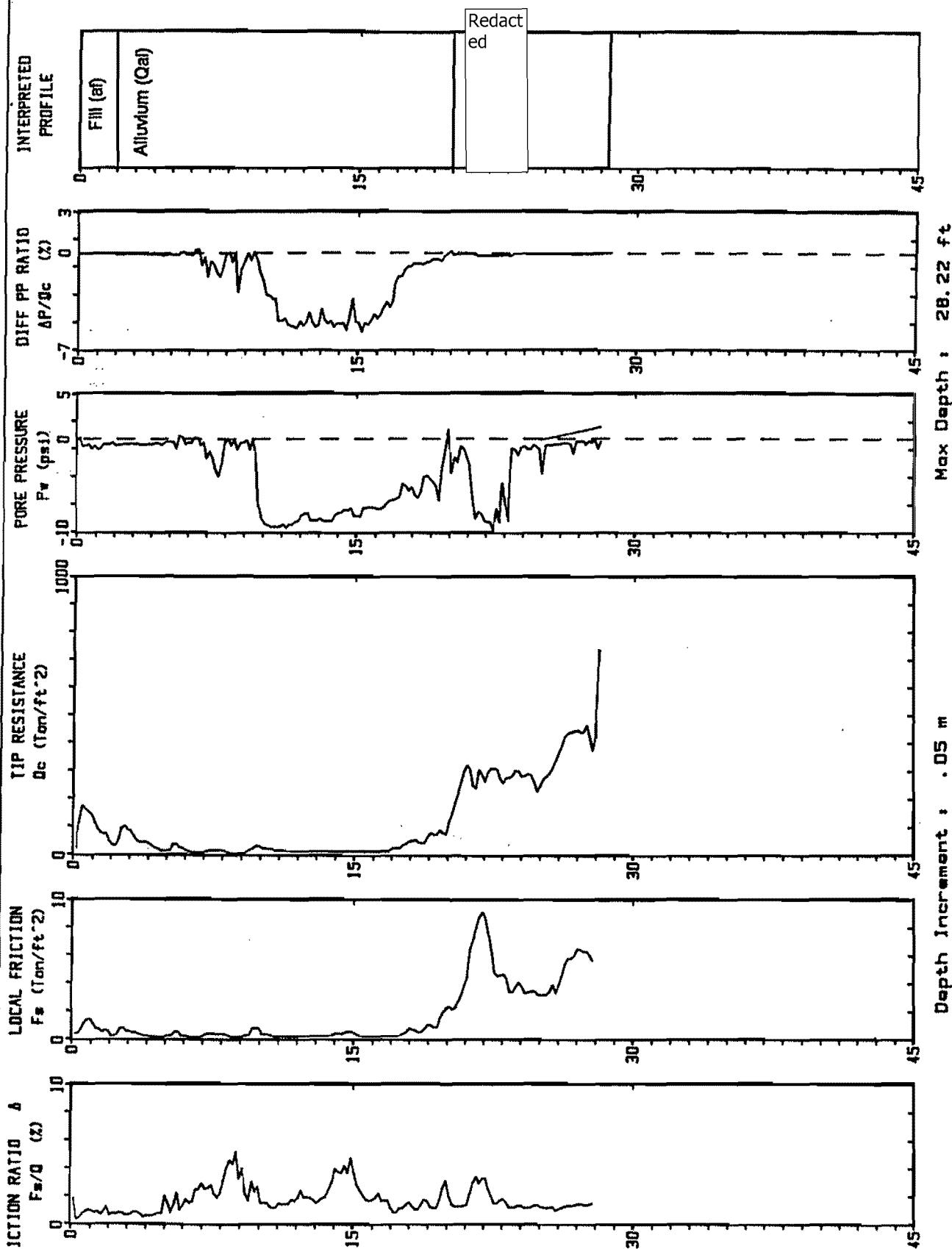
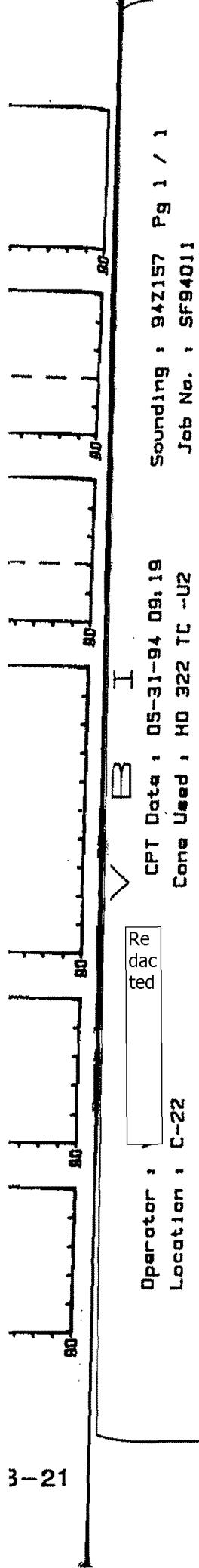
Module 1 – BART Extension to SFO
San Mateo County, California

APPROVED

DATE
8/98

A-7

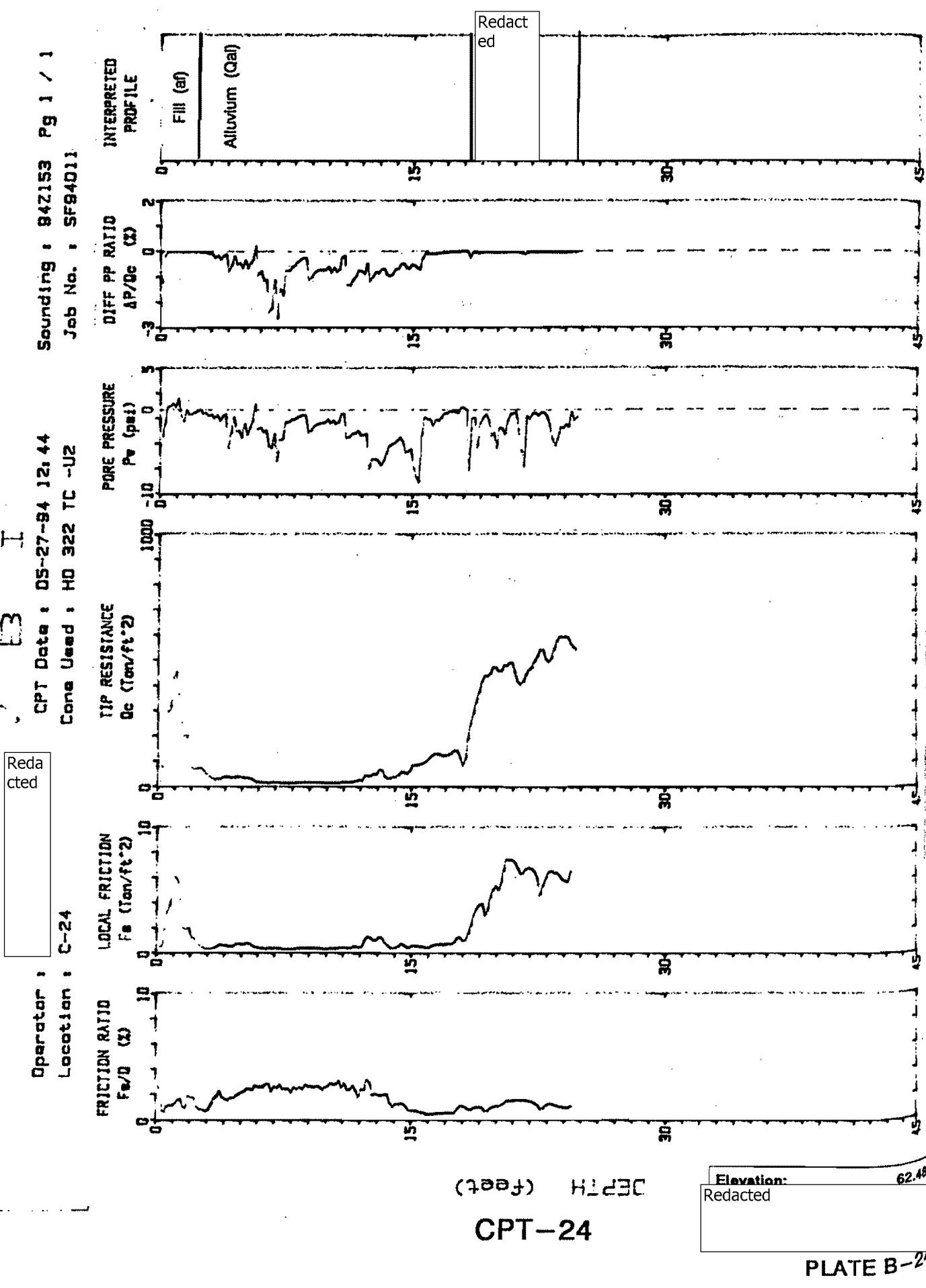
Figur



CPT-22

Elevation: 64.41
Redacted

PLATE B-22



CPT Date : 06-01-84 10:47
 Cone Used : HD 322 TC -U2
 Operator : Redacted
 Location : SF94011

Sounding : 84Z168 Pg 1 / 1

Redacted

Operator : Redacted
 Location : C-25

SanBrunoGT-LineRuptureInvestigation_DR_CPUC_213-Q03Atch01
LOG OF DRILL HOLEP040II
MART SFO Airport Extension
Northing: RedactedLOGGED BY: Redacted
CHECKED BY: RedactedDRILL HOLE NO.: B-18
DRILLING DATE: May 16, 1994
ELEVATION: 62.50 feet
DATUM: NGVD

THOD: 4 7/8" diameter Rotary Wash with cathead

DEPTH (FT)	UNCONFINED SHEAR STRENGTH (PSF)	BLK COUNT	TORVANE SHEAR STRENGTH (PSF)	POCKET PENE TROMETER COMP. STRENGTH (PSF)	PHOTOVAC TIP READING (PPM)	GRAPHIC LOG	GEOTECHNICAL DESCRIPTION AND CLASSIFICATION		ATTERBERG LIMITS	ADDITIONAL TESTS	
							DRY DENSITY (PCF)	MOISTURE CONTENT (%)	LIQUID LIMIT (%)	PLASTIC LIMIT (%)	
16											
18											
12											
9											
19	2.0										
16											
82/10"											
77/10"											
82/9"											
27											
90/11"											
76											
80/10"											

"ARTIFICIAL FILL (af)"
SILTY SAND (SM) with layers of gravel.

"ALLUVIUM (Gal)"
SILTY SAND (SM) light brown, dry, dense.

"ALLUVIUM (Gal)"
SILT (ML) light brown, moist, loose to medium dense, some fine grained sand.

"ALLUVIUM (Gal)"
CLAYEY SAND (SC) light red-brown, moist, medium dense, 40% fines.

"ALLUVIUM (Gal)"
LEAN CLAY (CL) black, moist, stiff to very stiff, some coarse red-brown sand, slightly organic.

"ALLUVIUM (Gal)"
CLAYEY SAND (SC) medium gray-brown and red-brown, moist, medium dense, fine grained sand, weakly cemented, 30% fines.

Redacted

SILTY SAND (SM) medium orange-brown, moist, very dense, fine to medium grained sand, weakly cemented, 14% fines.

Gray-brown and orange-brown, thin layers of fine gravel and coarse sand.

Weakly cemented.

Redacted

CLAYEY SAND (SC) medium orange-brown, moist, medium dense, fine and medium grained sand, some coarse angular gravel, very clayey.

Very dense.

Redacted

SILTY SAND (SM) orange, moist, very dense, fine to medium grained sand, locally weakly cemented, 14% fines.

Dark orange mottling.

LOG OF DRILL HOLE

San Bruno GT Line Rupture Investigation_DR_CPUC_213-Q03Atch01

JOB NO.: SF940H

PROJECT: BART SFO Airport Extension

LOCATION: Redacted

DRILLING METHOD: 4 7/8" diameter Rotary Wash with cathead

LOGGED BY: Redacted

CHECKED BY:

DRILL HOLE NO.: B-18

DRILLING DATE: May 16, 1994

ELEVATION: 62.50 feet

DATUM: NGVD

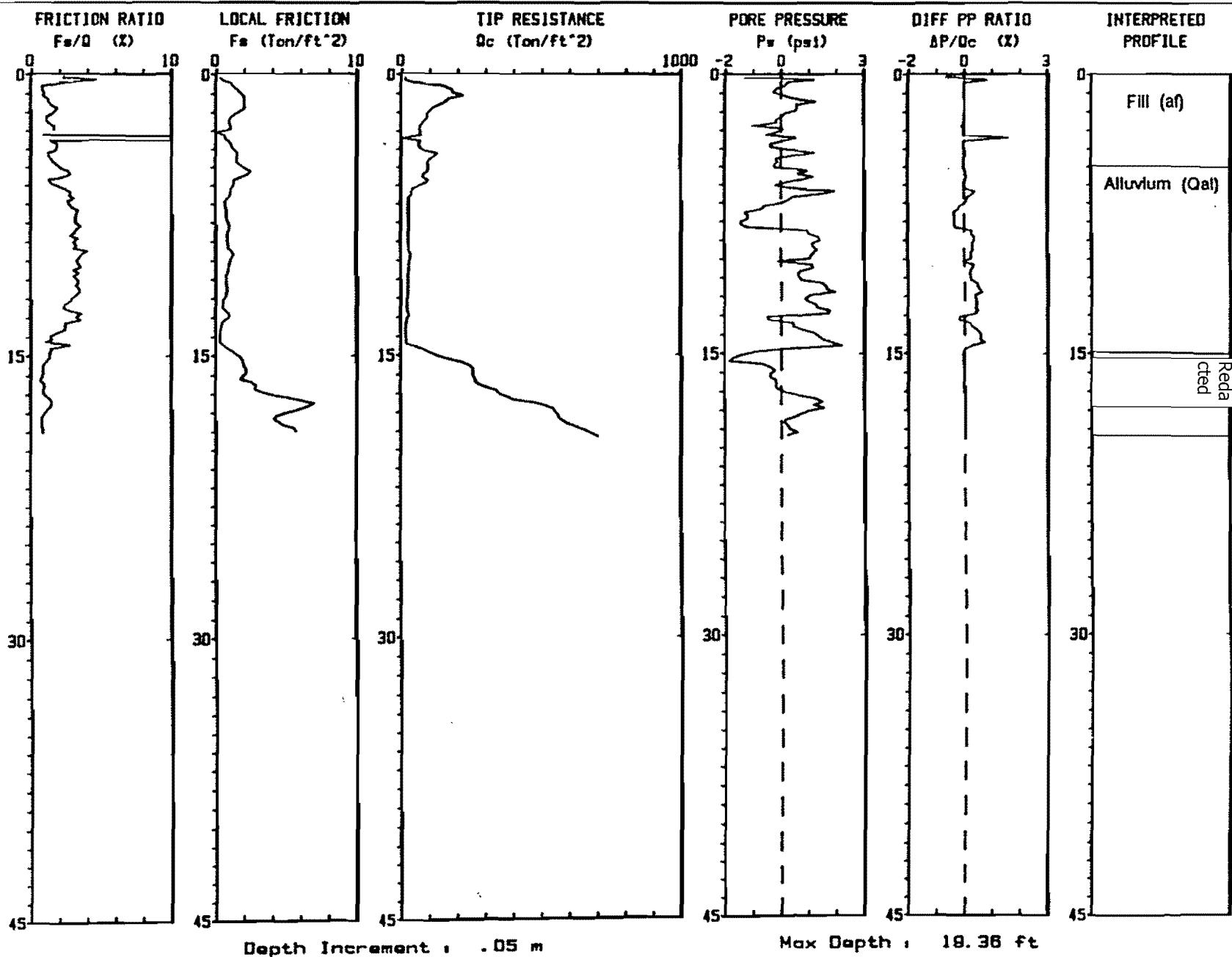
DEPTH (FEET)	SAMPLE	BLOW COUNT	TOVANE SHEAR STRENGTH (PSF)	POCKET PENETROMETER COMP. STRENGTH (PSF)	PHOTOVAC TIP READING (PPM)	GRAPHIC LOG	GEOTECHNICAL DESCRIPTION AND CLASSIFICATION						ADDITIONAL TESTS	
							DRY DENSITY (PCF)	MOISTURE CONTENT (%)	LIMIT (%)	PLASTIC LIMIT (%)	UNCONFINED SHEAR STRENGTH (PSF)			
50/5"														
50/5"														
78/II"														GS
65														
75														
98/II"														
85														
95														
105														

Bottom of drill hole at 81 1/2 feet.
Backfilled hole with soil cuttings and grouted uppermost 5 feet.

Operator : Redacted
Location : C-27

CPT Date : 05-27-84 13:24
Cone Used : HD 322 TC -U2

Sounding : 942154 Pg 1 / 1
Job No. : SF94011



LOG OF DRILL HOLE

San Bruno GT-Line Rupture Investigation_DR_CPUC_213-Q03Atch01

JOB NO.: SF040II

PROJECT: BART SFO Airport Extension

LOCATION: Redacted

LOGGED BY: Redacted

CHECKED BY: Redacted

DRILL HOLE NO.: B-23

DRILLING DATE: May 17, 1984

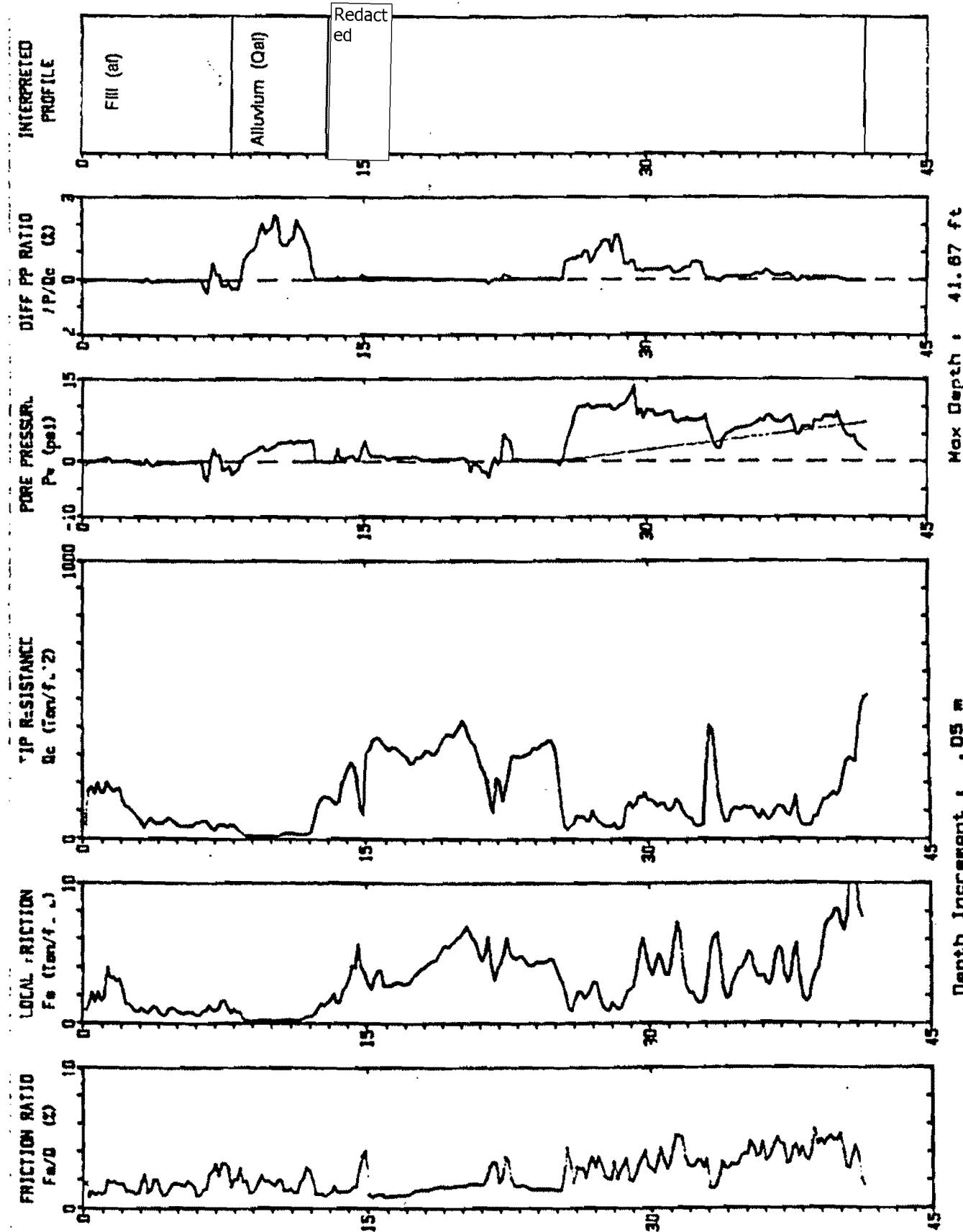
ELEVATION: 58.04 feet

DATUM: NGVD

DRILLING METHOD: 4 7/8" diameter Rotary Wash with cathead

DEPTH (FEET)	SAMPLE	BLOW COUNT	TORVANE SHEAR STRENGTH (PSF)	POCKET PENETROMETER CONE STRENGTH (TSF)	PHOTOVAC TIP READING (PPM)	GRAPHIC LOG	GEOTECHNICAL DESCRIPTION AND CLASSIFICATION	ATTERBERG LIMITS			ADDITIONAL TESTS
								DRY DENSITY (PCF)	MOISTURE CONTENT (%)	LIMIT (%)	
										LIQUID PLASTIC UNDEFINED SHEAR STRENGTH (PSF)	
4							"ARTIFICIAL FILL (af)" SILTY SAND (SM) brown, damp, loose, some fine gravel, some clay locally. Aluminum foil at 3 feet.				
12							"ARTIFICIAL FILL (af)" CLAYEY SAND (SC) dark brown, moist, medium dense, fragments of burnt wood and roots, fine gravel throughout, fine to coarse sand.				
18							Gravel at 7 feet.				
10		8	0.5				Black, moist.	107	22	28	15
							"ALLUVIUM (Gal)" LEAN CLAY (CL) black, moist, soft, some fine grained sand.				
							Increasing clay.				
20							"ALLUVIUM (Gal)" SILTY SAND (SM) dark blue-gray, loose, fine grained sand, 19% fines.				
13			0.5				"ALLUVIUM (Gal)" LEAN TO ORGANIC CLAY (CL/OL) black, moist, soft to medium stiff.	31	47	28	GS
18							"ALLUVIUM (Gal)" SILTY SAND with gravel (SM) light gray-brown with orange veins, moist, fine grained sand, fine gravel, medium dense, 35% fines.	88	25		GS
30		82					Redacted SILTY SAND (SM) light orange-brown, with veins of dark orange, moist to wet, very dense.	111	19		
							Redacted SILTY SAND to CLAYEY SAND (SC/SM) light orange-brown, moist, very dense, some orange veins, weakly cemented.				
68											
40		80/11"					Redacted SILTY SAND (SM) orange, moist, very dense. With light gray-brown patches.				
78/10"							Orange-brown, friable.				
50		77					Bottom of drill hole at 51 feet. Backfilled hole with soil cuttings and grouted uppermost 5 feet.				

Sounding : 842159 Pg 1 / 1
 Job No. : SF84011



(CPT) H13E

CPT-29

Elevation:	54.66
Redacted	

PLATE B-29

SB_GT&S_0037420

LOG OF DRILL HOLE

San Bruno Gas Line Rupture Investigation_DR_CPUC_213-Q03Atch01

JOB NO.: SF840II

PROJECT: BABY SFO Airport Extension

LOCATION: Redacted

DRILLING METHOD: 4 7/8" diameter Rotary Wash with cathead

LOGGED BY: Redacted

CHECKED BY: Redacted

DRILL HOLE NO.: B-24

DRILLING DATE: May 17, 1994

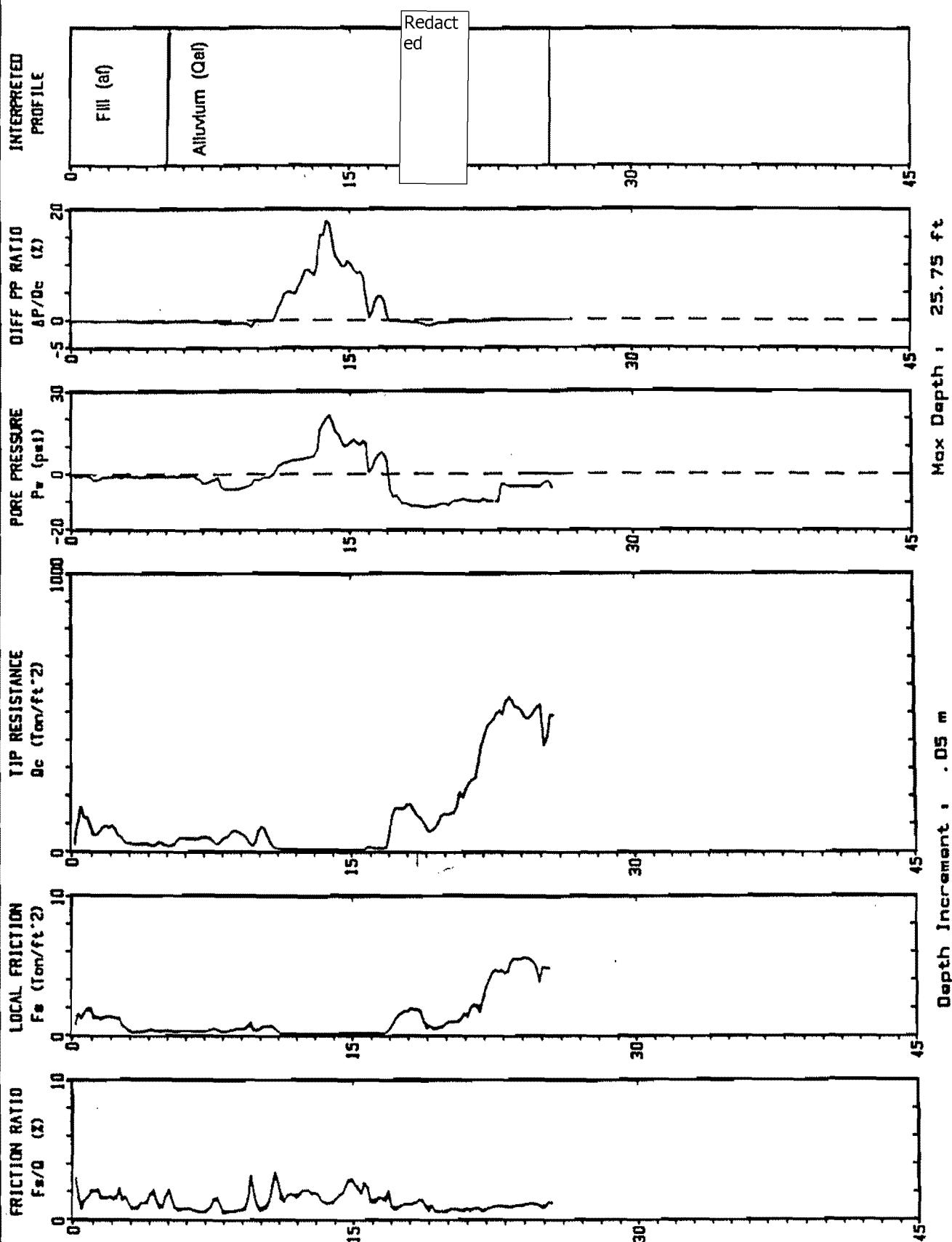
ELEVATION: 52.01 feet

DATUM: NGVD

DEPTH (FEET)	SAMPLE	BLOW COUNT	TORSION SHEAR STRENGTH (PSF)	POCKET PENETROMETER (TSF)	COMP. STRENGTH (TSF)	PHOTOVAC TIP READING (PPM)	GRAPHIC LOG	GEOTECHNICAL DESCRIPTION AND CLASSIFICATION		ATTERBERG LIMITS		UNCONFINED SHEAR STRENGTH (PSF)	ADDITIONAL TESTS
								DRY DENSITY (PCF)	MOISTURE CONTENT (%)	Liquid Limit (%)	Plastic Limit (%)		
18													
10													
8													
75													
50													
65													
21		3.25											
40													
56													
45													
50		50/10											
50		50/6"											
								Bottom of drill hole at 50 1/2 feet. Backfilled hole with soil cuttings and grouted uppermost 5 feet.					

CPT Date : 05-31-94 10:04
 Cone Used : HD 322 TC -U2
 Location : C-30
 Operator : Redacted

Sounding : 942158 Pg 1 / 1
 Job No. : SF94011



DEPTH (feet)

CPT-30

Elevation: 49.25
 Redacted

PLATE B-30

LOG OF DRILL HOLE

JOB NO: SF840II
 PROJECT: BART SFO Airport Extension
 LOCATION: Redacted
 DRILLING METHOD: 4 7/8" diameter Rotary Wash with cathead

San Bruno GTRI Gas Rupture Investigation_DR_CPUC_213-Q03Atch01

LOGGED BY: Redacted
 CHECKED BY:

DRILL HOLE NO.: B-25
 DRILLING DATE: May 18, 1994
 ELEVATION: 47.00 feet
 DATUM: NGVD

DEPTH (FEET)	SAMPLE	BLOW COUNT	TORVANE	SHEAR STRENGTH (PSF)	POCKET PENETROMETER	COMP. STRENGTH (TSF)	PHOTOVAC TIP	READING (PPM)	GRAPHIC LOG	GEOTECHNICAL DESCRIPTION AND CLASSIFICATION				ATTERBERG LIMITS	UNCONFINED SHEAR STRENGTH (PSF)	ADDITIONAL TESTS
										DRY DENSITY (PCF)	MOISTURE CONTENT (%)	LIMIT (X)	PLASTIC LIMIT (%)			
5		5														
10		20	-	-												
20		15	-	-												
30		21	-	-												
31		1.25	-	-												
40		50/6"	-	-												
50		20	-	-												
50		33	-	-												

"ARTIFICIAL FILL (af)"
 SILTY SAND (SM) brown, damp, loose, with gray gravel, pile of broken concrete blocks from 6-inches to 2 feet.
 2 feet: Golf ball, cobbles, rocks to 4 feet.
 No samples at 2 1/2 feet, concrete blocks in hole.

"ALLUVIUM (Gal)"
 SILTY SAND (SM) blue-gray, moist to wet, loose, fine grained sand, roots.

"ALLUVIUM (Gal)"
 SILTY SAND (SM) blue-gray, moist to wet, medium dense, fine grained sand, roots, 2-inch thick layer of clayey silt (ML) at 10 1/2 feet.

Dense, black at 17 feet.
 18 1/2 feet: Blue-gray.
 Medium dense.

"ALLUVIUM (Gal)"
 SANDY LEAN CLAY (CL) dark gray, moist, stiff, fine grained sand, green-blue and orange lenses, occasional fine gravel.
 25 feet: Green-blue gray with white speckles.

"ALLUVIUM (Gal)"
 CLAYEY SAND (SC) dark gray, moist, medium dense, fine grained sand, some roots, 28% fines.

"ALLUVIUM (Gal)"
 SANDY LEAN CLAY (CL) gray-brown, moist, stiff, sandy/silty lenses.

"ALLUVIUM (Gal)"
 SILTY SAND (SM) gray, moist, dense, fine grained sand, some brown veins.
 Redacted
 POORLY GRADED SAND with silt and gravel (SP-SM) light gray, moist, very dense, medium to fine grained sand, fine gravel.

Redacted
 SILTY CLAY (CL-ML) dark brown, moist, very stiff, veins of gray sand, fine grained sand, sulfur odor, organic content 15%.

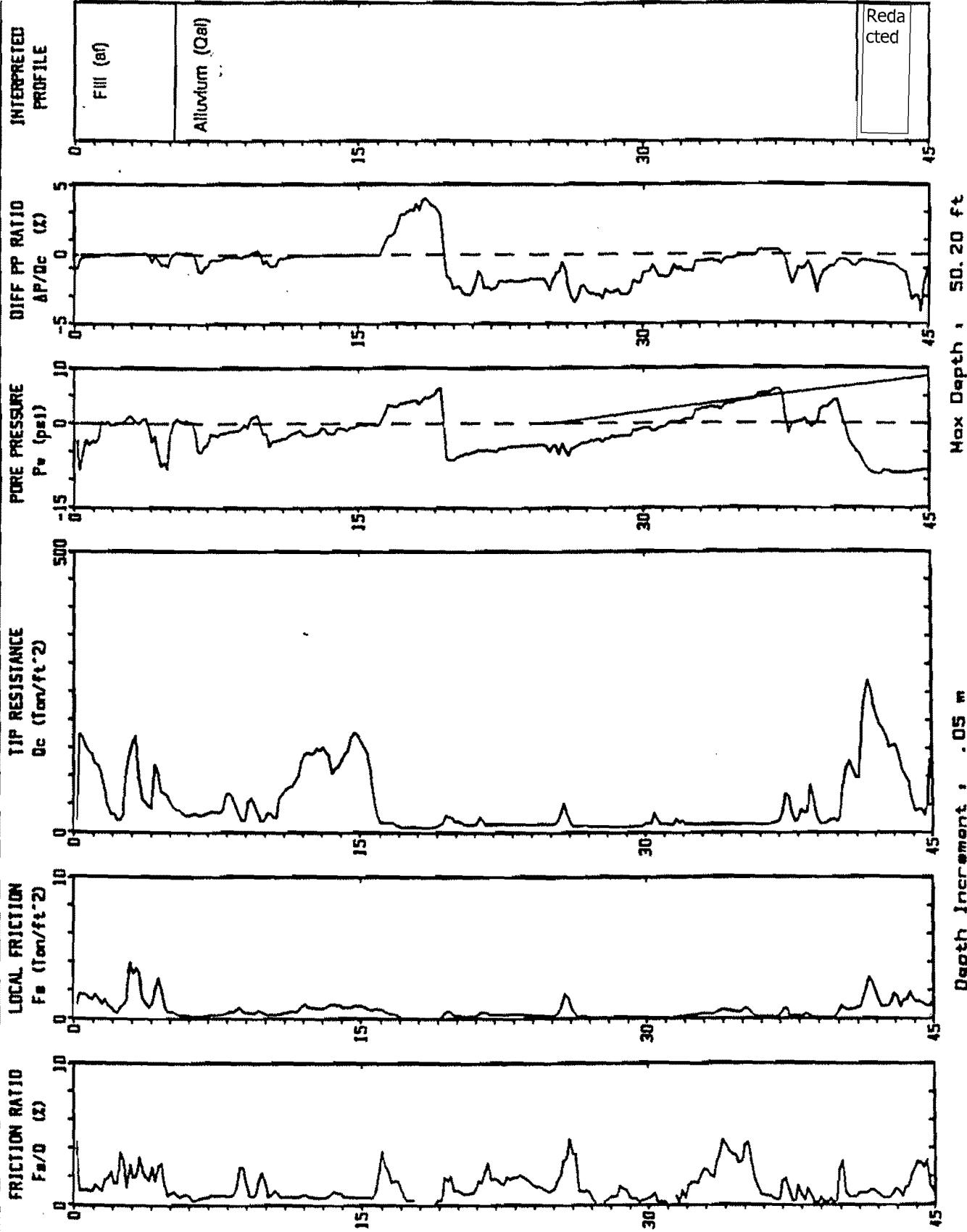
Redacted
 SILTY SAND (SM) gray and gray-brown, moist, dense.

Bottom of drill hole at 51 1/2 feet.
 Groundwater measured at 27.5 feet depth on 6/13/94.
 Piezometer installed.

Sounding : 842159 Pg 1 / 2
Job No. : SF94011

CPT Date : 05-31-84 11:06
Cone Used : HD 322 TC - U2

Operator : Redacted
Location : C-31



DEPTH (feet)

CPT-31

Elevation: 46.96
Redacted

PLATE B-31

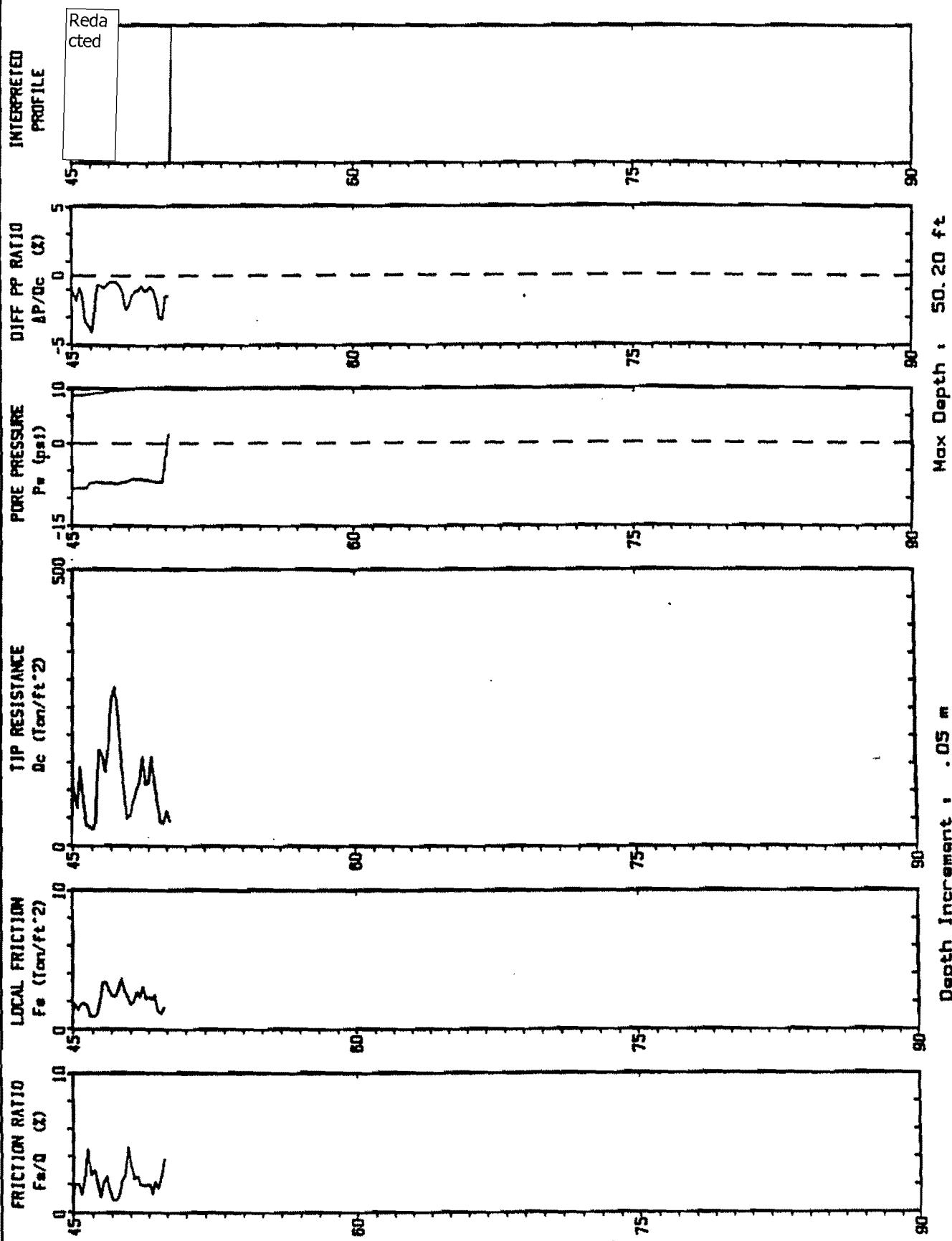
SB_GT&S_0037424

V E I

Operator : Redacted
 Location : C-31

CPT Date : 05-31-84 11:06
 Cone Used : HD 322 TC -U2

Sounding : 942159 Pg 2 / 2
 Job No. : SF94011



DEPTH (feet)

CPT-31 (Cont.)

PLATE B-31

SB_GT&S_0037425

V B I

Operator : Redacted
 Location : CPT Date : 05-31-84 12:43
 Cone Used : HQ 322 TC -U2

Sounding : 94Z180 Pg 1 / 2
 Job No. : SF94011

Redacted

Location : C-32

INTERPRETED PROFILE

FILL (a)
 Alluvium (Qaf)

TIP RESISTANCE
 q_c (Ton/ft²)

LOCAL FRICTION
 f_a (Ton/ft²)

FRICITION RATIO
 f_a/q (Z)

PURE PRESSURE
 P_v (psi)

DIFF PP RATIO
 $\Delta P/\rho g_c$ (Z)

DEPTH (feet) : 05 m

Max Depth : 50.20 ft

15 30 45

15 30 45

15 30 45

15 30 45

15 30 45

15 30 45

DEPTH (feet)

CPT-32

Elevation: 44.31
 Redacted

PLATE B-32

SB_GT&S_0037426

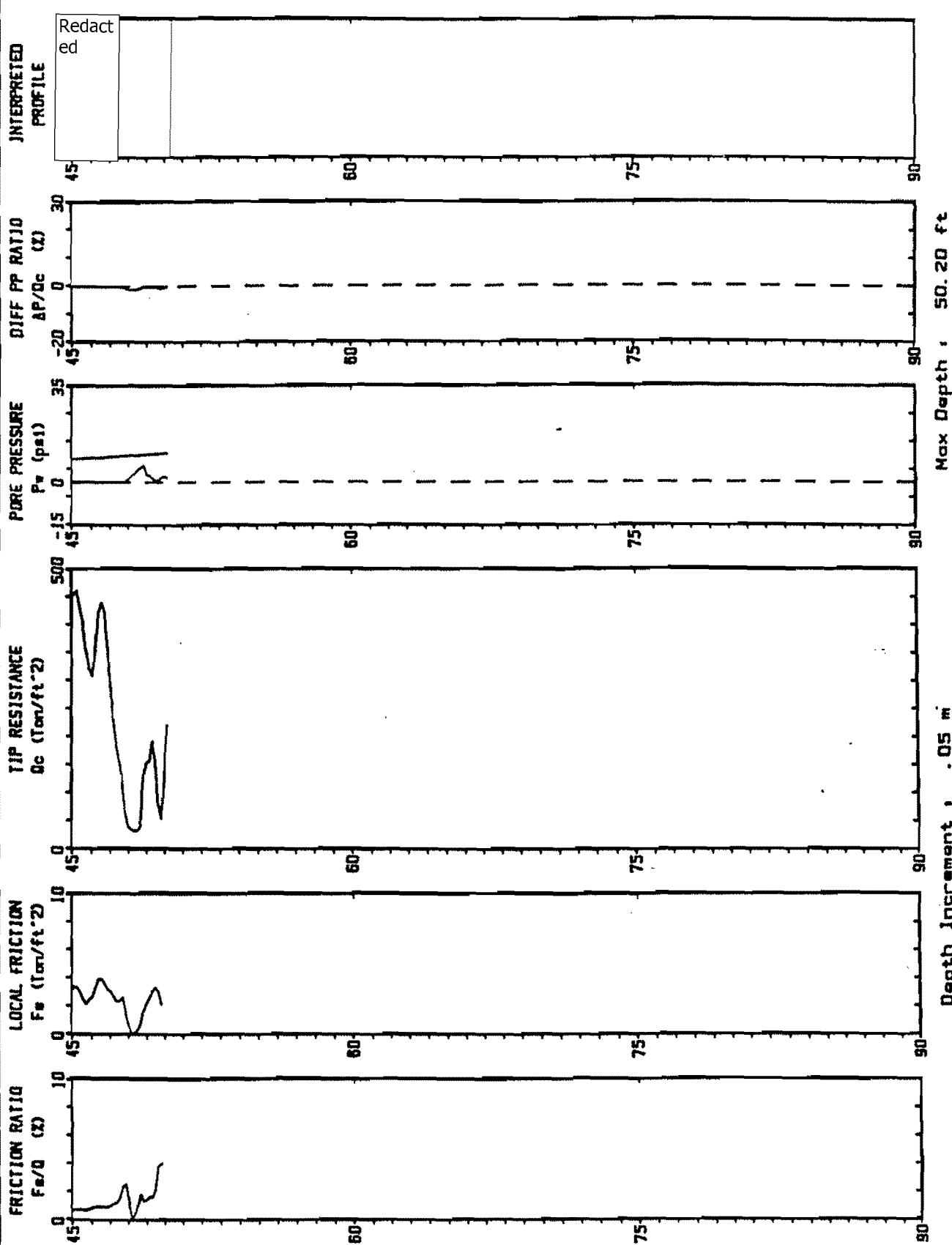
V B I

Redacted

Operator :
 Location : C-32

CPT Date : 05-31-84 12:43
 Cone Used : HQ 322 TC -U2

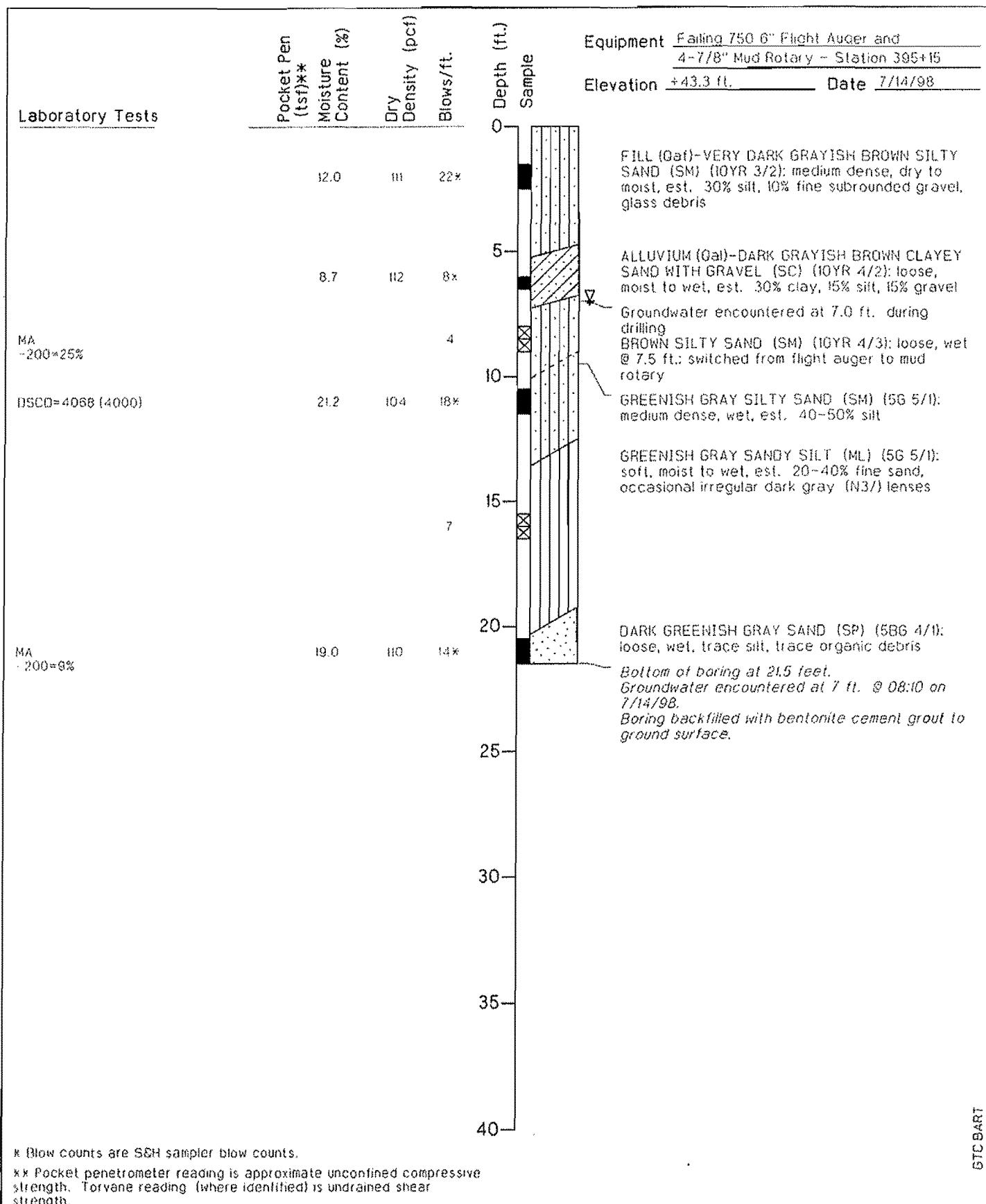
Sounding : 942160 Pg 2 / 2
 Job No. : SF94011



DEPTH (feet)

CPT-32 (Cont.)

PLATE B-32



GTC BART



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Engineering and
Environmental Services

DRAWN JOB NUMBER
CEG 40646 4E

Log of Boring B-201
Module 2 - BART Extension to SFO
San Mateo County, California

APPROVED
Redact

DATE
8/98

A-1

Figure

LOG OF DRILL HOLE

San Bruno GT-Line Rupture Investigation DR_CPUUC_213-Q03Atch01

JOB NO.: SF94011
PROJECT: BART SFO Airport Extension

LOCATION: Redacted

DRILLING METHOD: 4 1/8" diameter Rotary Wash with cathead

LOGGED BY: Redacted

CHECKED BY:

DRILL HOLE NO.: B-28
ELEVATION: 43.50 feet
DATUM: NGVD

DEPTH (FEET)	SAMPLE	BLOW COUNT	TORVANE SHEAR STRENGTH (PSF)	POCKET PENETROMETER COMP. STRENGTH (TSF)	PHOTOVAC TIP READING (PPM)	GRAPHIC LOG	GEOTECHNICAL DESCRIPTION AND CLASSIFICATION			ATTERBERG LIMITS	DRY DENSITY (PCF)	MOISTURE CONTENT (%)	LIQUID LIMIT (%)	PLASTIC LIMIT (%)	UNCONFINED SHEAR STRENGTH (PSF)	ADDITIONAL TESTS
							GEOTECHNICAL DESCRIPTION	AND CLASSIFICATION	TESTS							
4			"ALLUVIUM (Gal)" SILTY SAND (SM) brown, damp to moist, loose.								100	22				
4			"ALLUVIUM (Gal)" SANDY SILT (ML) brown, moist, loose, fine grained sand, 52% fines.													GS
9			"ALLUVIUM (Gal)" POORLY GRADED SAND (SP) dark gray, moist to wet, loose, 2X fines.													GS
10			"ALLUVIUM (Gal)" SANDY SILT (ML) dark gray, moist to wet, loose to medium, dense, 6X fines.													GS
15			"ALLUVIUM (Gal)" POORLY GRADED SAND with silt (SP-SM) gray, moist to wet, medium dense, medium to fine grained sand, 1½ fines.													GS
19			"ALLUVIUM (Gal)" FAT CLAY (CH) black, moist, soft to medium stiff, organic content 1.4%.													GS
20			"ALLUVIUM (Gal)" CLAYEY SAND TO SILTY SAND (SC/SM) light blue-gray, moist, medium dense, root fragments.													GS
30			POORLY GRADED SAND with silt (SP-SM) dark blue-gray, moist, very dense, with black staining and a layer of black clayey sand (SC) at 35 feet, some roots, weakly cemented.													GS
35			Redacted													OR
35			Redacted													OR
35			POORLY GRADED SAND with silt (SP-SM) light blue-gray, moist, very dense, 6-inch layer of clay (CL-ML) at 40 1/2 feet, occasional layers of fine grained sand.													
40			Redacted													
40			Redacted													
56			LEAN CLAY (CL) light blue-gray, moist, very dense, fine brown organic bands at 1 to 2-inch spacing.													
56			Redacted													
56			SILTY SAND (SM) light blue-gray, moist, very dense, fine brown organic bands.													
80/ft			Redacted													
80/ft			LEAN CLAY (CL) light orange-brown, moist, very stiff.													

SHEET 1 of 2

LEGEND TO LOGS ON PLATE A-10

PLATE A-2.26

LOG OF DRILL HOLE

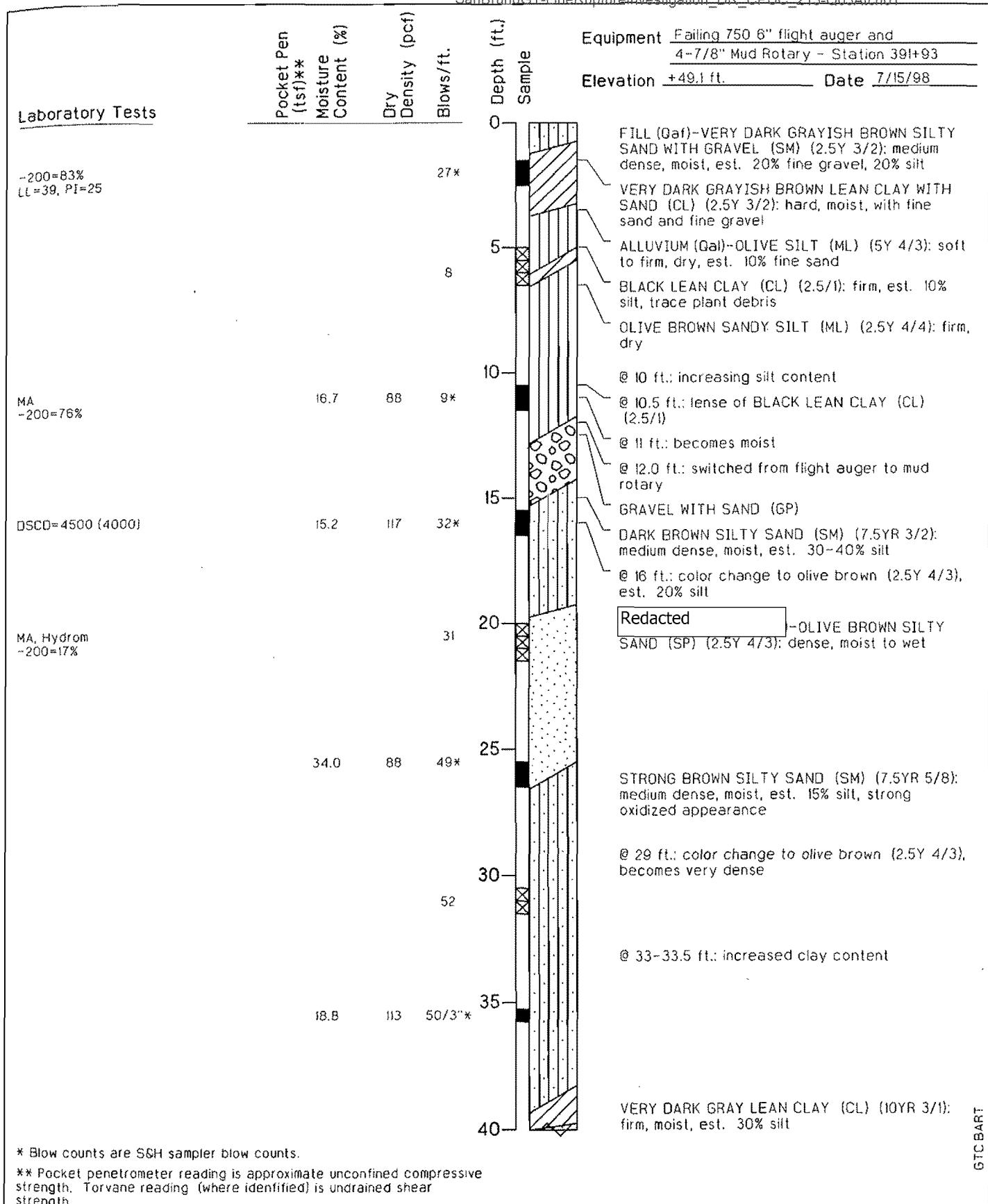
DRILL NO.: SF8401
 PROJECT: BART SEO Airport Extension
 LOCATION: Redacted

LOGGED BY: Redacted
 CHECKED BY: Redacted

DRILLING METHOD: 4 7/8" diameter Rotary Wash with cathead

DRILL HOLE NO.: B-26
 DRILLING DATE: May 18, 1994
 ELEVATION: 43.50 feet
 DATUM: NGVD

DEPTH (FT)	SAMPLE	BLOW COUNT	TORVANE SHEAR STRENGTH (PSF)	POCKET PENETROMETER COMP. STRENGTH (TSF)	PHOTOVAC TIP READING (FPM)	GRAPHIC LOG	GEOTECHNICAL DESCRIPTION AND CLASSIFICATION				DRY DENSITY (PCF)	MOISTURE CONTENT (%)	ATTERBERG LIMITS			UNCONFINED SHEAR STRENGTH (PSF)	ADDITIONAL TESTS
							LIMIT (%)	LIMIT (%)	LIMIT (%)	UNCONFINED SHEAR STRENGTH (PSF)			LIMIT (%)	PLASTIC LIMIT (%)	LIMIT (%)		
82 1/2"			3.5				Redacted	SILTY SAND (SM) light orange, moist, very dense, with light gray and dark orange banding, fine grained sand, some fine gravel in layers.									
50/5"								Some coarse to fine sand in layers and also some fine gravel 1/2 to 1-inch layers.									
65																	
75								Light gray-brown, medium to fine grained sand.									
75								Driller reports hard lens at 78 feet, clay in sand at 78 feet.									
								80 feet: Clay lenses (stiff) light gray, in cuttings.									
								80.5 feet: 7-inch layer of silty sand (SM) gray, fine grained sand.									
85							Redacted	LEAN CLAY (CL) gray, mottled with brown, moist, stiff, appears to be organic (sulfur odor), layer of fine sand.									
								Bottom of drill hole at 81 1/2 feet.									
								Backfilled hole with soil cuttings and grouted uppermost 5 feet.									
95																	
105																	



GTC BART

Figure



Harding Lawson Associates
Engineering and
Environmental Services

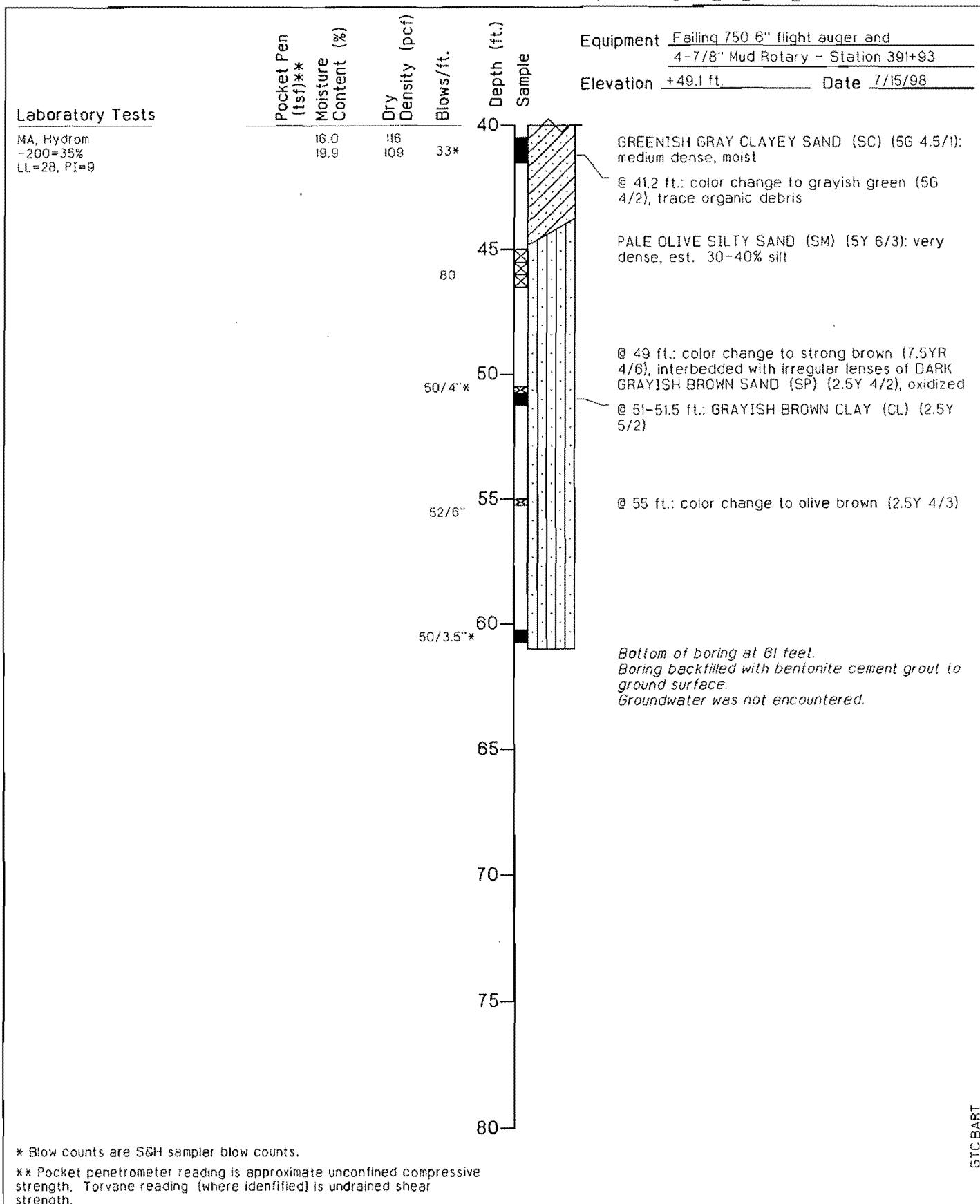
DRAWN JOB NUMBER
CEG 40646 4E

Log of Boring B-202
Module 2 – BART Extension to SFO
San Mateo County, California

APPROVED
Redacte

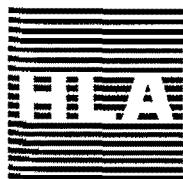
DATE
8/98

A-2



GTC BART

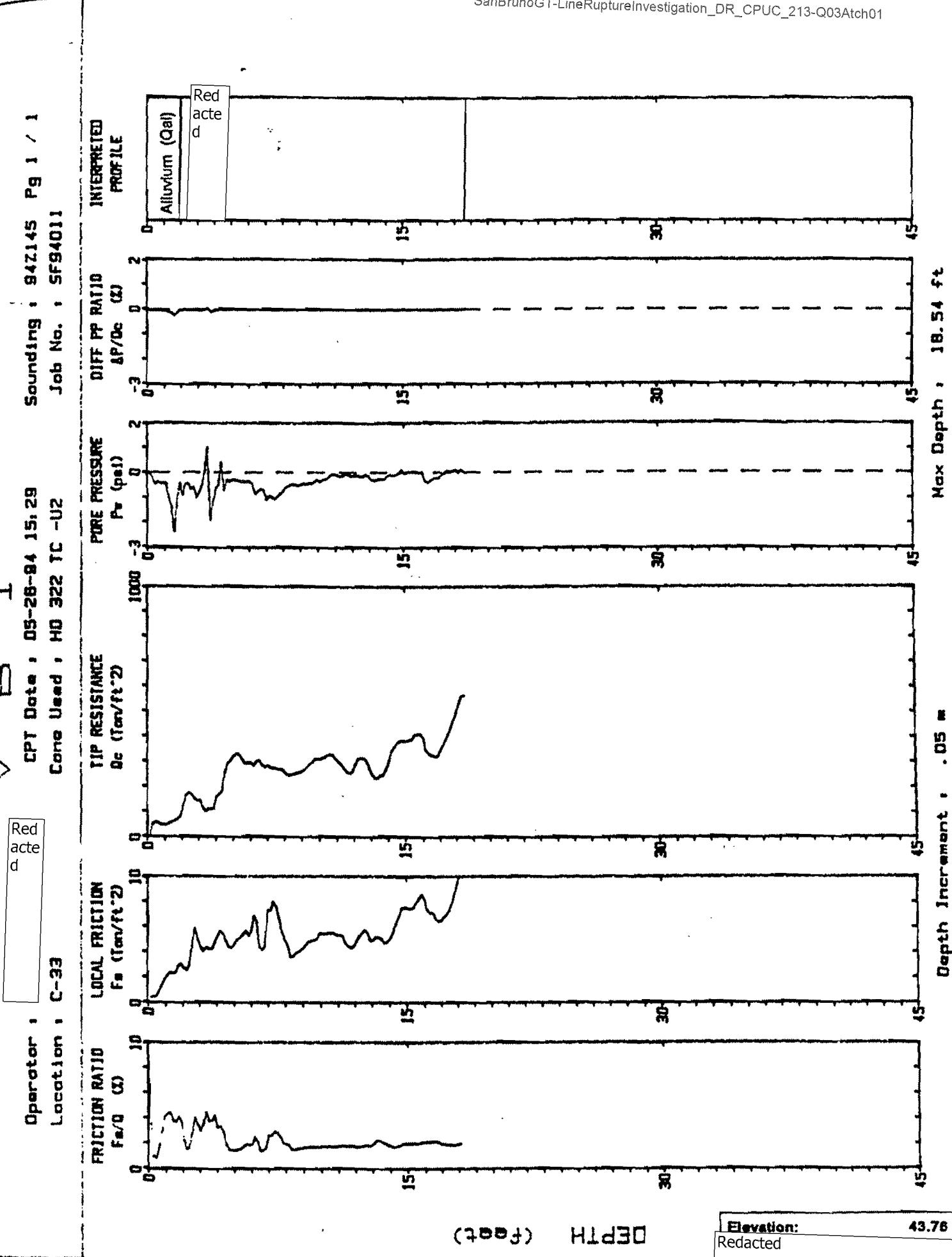
Figure

**Harding Lawson Associates**

Engineering and Environmental Services.

Log of Boring B-202Module 2 – BART Extension to SFO
 San Mateo County, California**A-2**DRAWN
CEGJOB NUMBER
40646 4EAPPROVED
RedactedDATE
8/98

REVISED DATE



DEPTH (feet)

CPT-33

Elevation:	43.76
Redacted	

LOG OF DRILL HOLE

JOB NO.: SF94011
 PROJECT: BART SFO Airport Extension
 LOCATION: Redacted

DRILLING METHOD: 4 7/8" diameter Rotary Wash with cathead

LOGGED BY: Redacted
 CHECKED BY: Redacted

DRILL HOLE NO.: B-27
 DRILLING DATE: May 18, 1994
 ELEVATION: 44.32 feet
 DATUM: NGVD

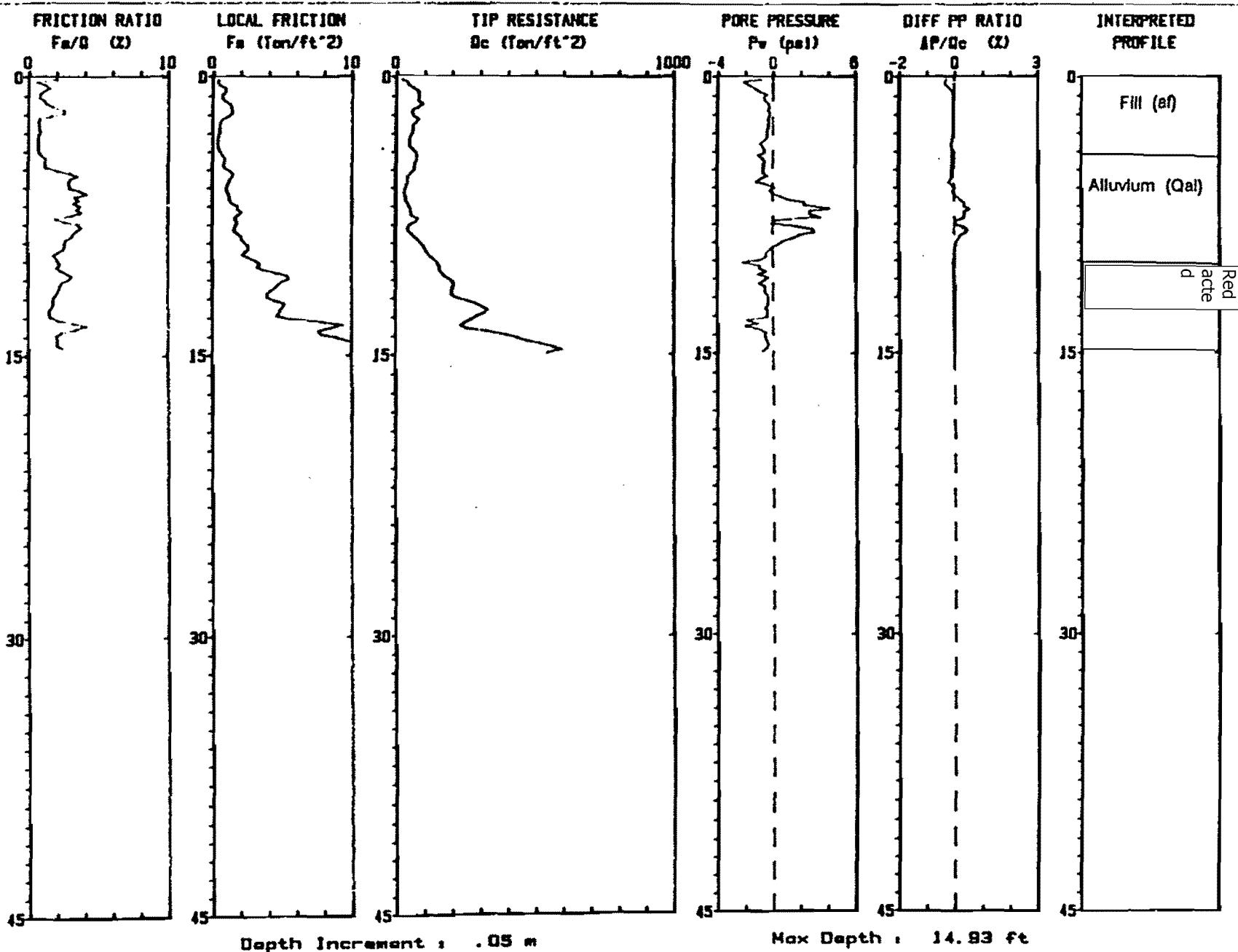
DEPTH (FEET)	SAMPLE	BLOW COUNT	TORVANE SHEAR STRENGTH (PSF)	POCKET PENETROMETER COMP. STRENGTH (TSF)	PHOTOVAC TIP READINGS (PPM)	GRAPHIC LOG	GEOTECHNICAL DESCRIPTION AND CLASSIFICATION		DRY DENSITY (PCF)	MOISTURE CONTENT (%)	ATTERBERG LIMITS		UNDEFINED SHEAR STRENGTH (PSF)	ADDITIONAL TESTS
											LIMIT (%)	PLASTIC LIMIT (%)		
							"ARTIFICIAL FILL (atf)" SILTY SAND with gravel (SM) brown, damp, medium dense.							
48							"ALLUVIUM (Qal)" SILTY SAND with gravel (SM) brown, damp, dense. Redacted							
10	82/1"						Poorly GRADED SAND with silt (SP-SM) light orange-brown with orange bands, damp, dense, fine grained sand. Silt in bands, very dense, 1% fines.							
15	83/1"						15 to 15 1/2 feet: Light gray-brown, wet. 15 1/2 feet: Light gray-brown with thin black stripes, moist, fine grained sand.							
20	83/10"						Light brown, moist, with orange bands, fine grained sand.						GS	
25	78/11"						Dark orange bands, moist to wet.							
30	50/4"						Dark gray-brown with frequent thin layers of organics, no orange coloring.							
35	50/3"						Redacted POORLY GRADED SAND with silt (SP-SM) gray-brown, moist, very dense, fine grained sand and some fine gravel, 1% fines.							
40	50/4"													
45	79						Redacted SILTY SAND (SM) gray-brown, moist, very dense.							
50	77						Redacted SILTY SAND/SANDY SILT (SM/ML) gray-brown, moist, very dense, fine grained sand, bands of coarse and coarse to fine grained sand spaced 3 to 4-inches. Bottom of drill hole at 51 feet.							

Operator : Re
dac
ted
Location : E-34

✓ B I

CPT Date : 05-26-84 15:07
Cone Used : HQ 322 TC -U2

Sounding : 942144 Pg 1 / 1
Job No. : SF94011



CPT-34

PLATE B-34

LOG OF DRILL HOLE

San Bruno GT-Line Rupture Investigation_DR_CPUC_213-Q03Atch01

DRILL NO.: SF04011

NAME (T): BART SFO Airport Extension

LOCATION: [Redacted]

DRILLING METHOD: 4 7/8" diameter Rotary Wash with cathead

LOGGED BY: [Redacted]

CHECKED BY: [Redacted]

DRILL HOLE NO.: B-28

DRILLING DATE: May 18, 1994

ELEVATION: 41.37 feet

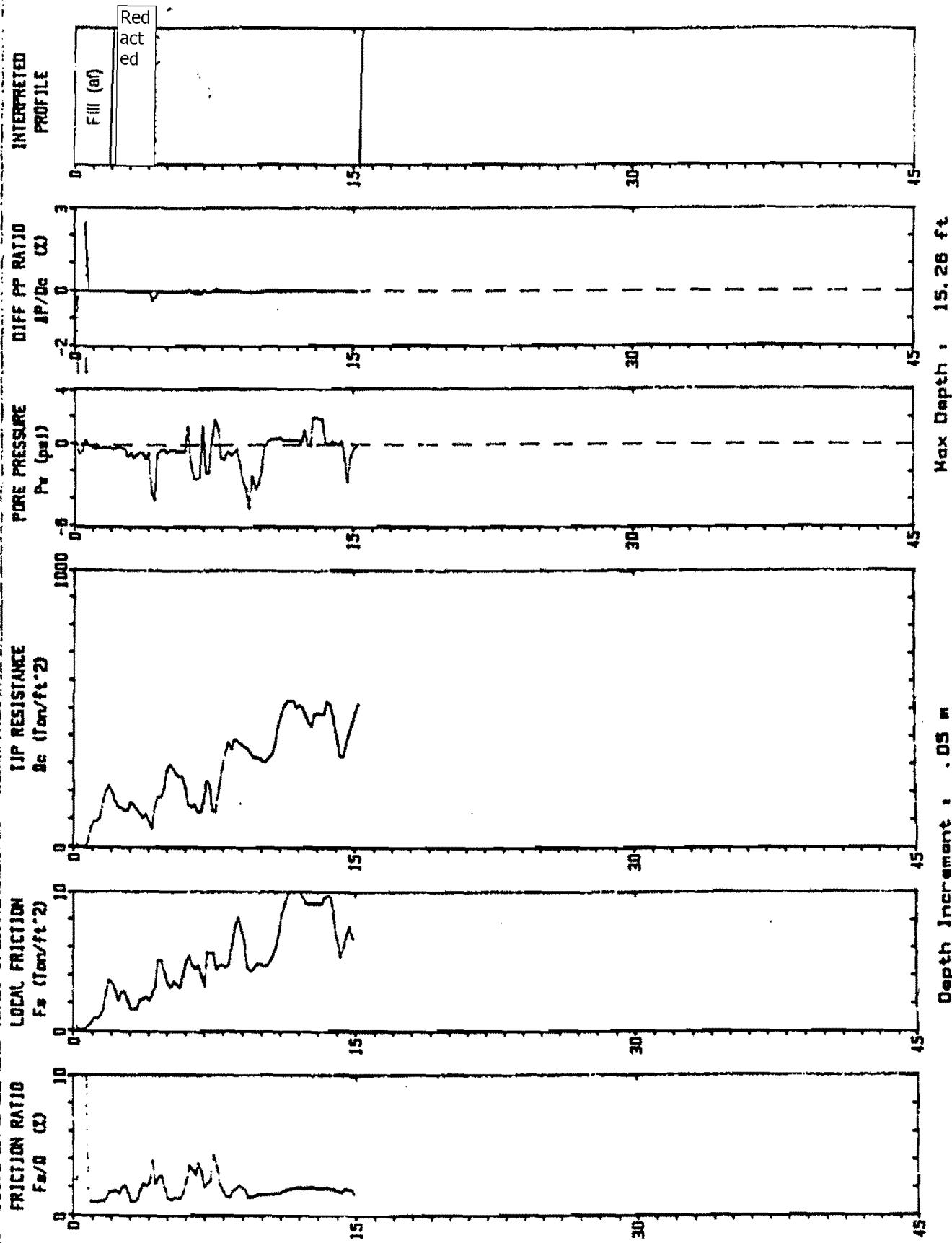
DATUM: NGVD

SAMPLE LEVEL	BLOW COUNT	TORVANE SHEAR STRENGTH (PSF)	POCKET PENETROMETER COMP. STRENGTH (PSF)	PHOTOVAC TIP READING (PPM)	GRAPHIC LOG	GEOTECHNICAL DESCRIPTION AND CLASSIFICATION	ATTERBERG LIMITS		UNCONFINED SHEAR STRENGTH (PSF)	ADDITIONAL TESTS	
							DRY DENSITY (pcf)	MOISTURE CONTENT (%)	LIQUID LIMIT (%)	PLASTIC LIMIT (%)	
						"ARTIFICIAL FILL (af)" SAND (SP) with cement tailings and gravel.					
47						"ALLUVIUM (Gall)" SILTY SAND (SM) brown, damp, loose. [Redacted] SILTY SAND (SM) light brown, moist, dense, with orange banding, 35% fines. light gray-brown, some orange speckles, very dense, fine grained sand, no apparent cementation, 13% fines.					GS
73										GS	
88						Dark orange bands at 15 1/2 feet, less silty.					
80/8"						[Redacted] SILTY SAND (SM) light gray-brown, moist, very dense, orange and red speckles, some orange mottling in areas, fine grained sand.					
84											
78						Less silt, bands of orange.					
50/5"						[Redacted] POORLY GRADED SAND (SP) brown with some black staining, moist, very dense.					
86						[Redacted] SILTY SAND (SM) gray-brown, moist, very dense, 1-inch thick layer of silty clay at 41 feet.					
84						[Redacted] WELL GRADED SAND with silt (SW-SM) light gray, moist, very dense, white mottling, medium to coarse grained sand, some fine gravel.					
82						Blue-gray at 50 feet. [Redacted] SILT (ML) blue-gray, moist, very dense.					
						Bottom of drill hole at 51 feet. No water measured to a depth of 41 feet on 6/13/94. Piezometer installed.					

Operator : C-35
Location : C-35
Redacted

CPT Date : 05-26-94 14:24
Cone Used : HQ 322 TC -U2
Redacted

Sounding : 94Z143 Pg 1 / 1
Job No. : SF94011



(Top) DEPTH (feet)

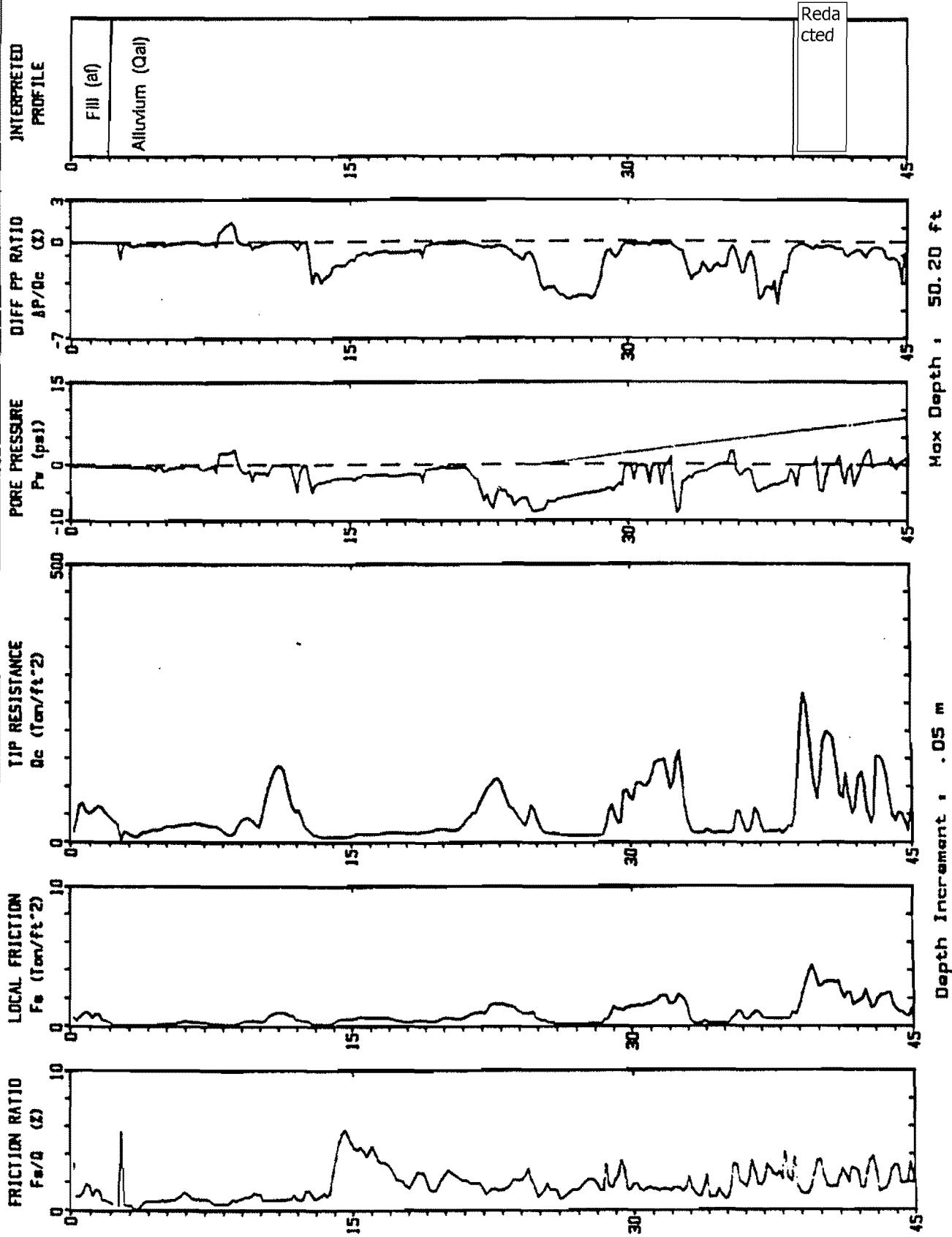
CPT-35

Elevation: 41.26
Redacted

PLATE B-35

Operator : Redacted
 Location : C-36
 CPT Date : 05-26-84 13:00
 Cone Used : HO 322 TC -U2

Sounding : 84Z141 Pg 1 / 2
 Job No. : SF94011



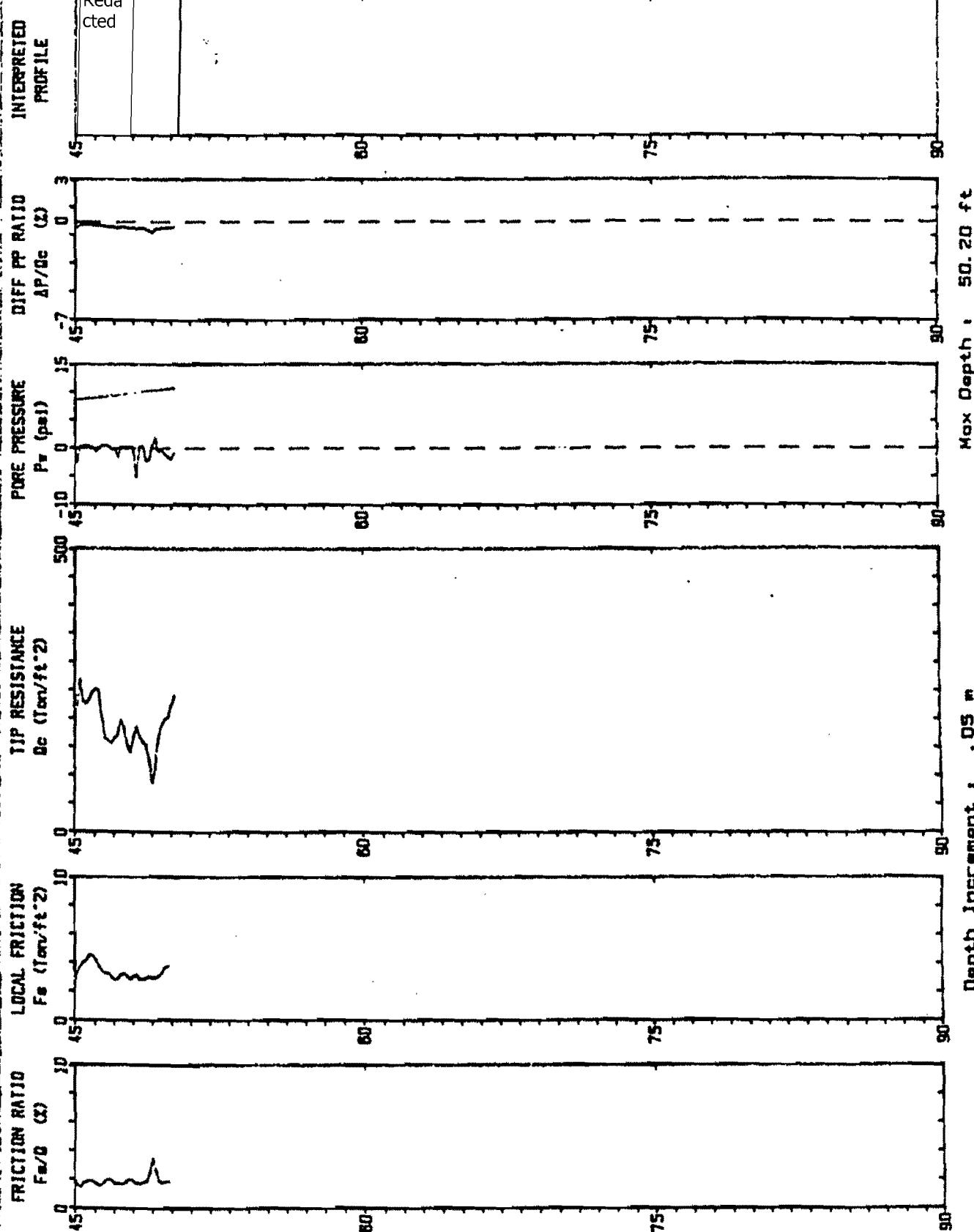
CPT-36

PLATE B-36

Operator : Redacted
 Location : C-36
 Sounding : 84Z141 Pg 2 / 2
 Job No. : SF94011

CPT Date : 05-26-84 13:00
 Cone Used : HD 322 TC -12
 CPT Data : Redacted

Depth Increment : .05 m
 Max Depth : 50.20 ft



DEPTH (feet)

CPT-36 (Cont.)

PLATE B-36

LOG OF DRILL HOLE

DD NO: SF840II

PROJECT: BART SEO Airport Extension

LOCATION: Redacted

MILLING METHOD: 4 7/8" diameter Rotary Wash with cathead

LOGGED BY: Redacted

CHECKED BY:

DRILL HOLE NO.: B-29

DRILLING DATE: May 25, 1984

ELEVATION: 31.74 feet

DATUM: NGVD

DEPTH (FEET)	SAMPLE	BLOW COUNT	TOVANE SHEAR STRENGTH (PSF)	POCKET PENE TROMETER COMP. STRENGTH (TSF)	PHOTOVAC TIP READING (PPM)	GRAPHIC LOG	GEOTECHNICAL DESCRIPTION AND CLASSIFICATION			ATTERBERG LIMITS		ADDITIONAL TESTS
							DRY DENSITY (PCF)	MOISTURE CONTENT (%)	LIMIT (%)	PLASTIC LIMIT (%)	UNCONFINED SHEAR STRENGTH (PSF)	
0												
6						"ARTIFICIAL FILL (af)" POORLY GRADED SAND with gravel (SP) dark brown, dry to damp.						
10						"ARTIFICIAL FILL (af)" SILTY SAND (SM) brown, damp, loose. Piece of glass at 5.2 feet.						
15						"ALLUVIUM (Qal)" POORLY GRADED SAND with silt (SP-SM) light brown, damp, loose, fine to medium grained sand, some roots.						Corr
20						"ALLUVIUM (Qal)" SILTY SAND (SM) dark brown, moist, banded with black and orange, medium dense. Wet, 14% fines.						GS
20		20	1.5			"ALLUVIUM (Qal)" LEAN CLAY (CL) black, moist, stiff, moderately plastic. Marbled blue-green and gray, very stiff.	98	23	48	16	1570	C
32		2.5				"ALLUVIUM (Qal)" SANDY SILT (ML) gray, moist, loose, organic odor, 64% fines.	108	21	36	17	2120	
30		7				"ALLUVIUM (Qal)" FAT CLAY (CH) with interbedded silt (ML), gray-brown, moist, medium stiff clay to medium dense silt. Light blue-green gray, heavy organic odor.	90	32	60	28	600	GS
40		12				"ALLUVIUM (Qal)" SANDY SILT (ML) gray, moist, medium dense, 66% fines.	87	34			820	
23						"ALLUVIUM (Qal)" LEAN CLAY (CL) alternating with layers of silt (ML) dark brown, moist, very stiff clay to medium dense sat. Organic content 1.4%.	84	54				GS
50		12					30	40	33			OR

LOG OF DRILL HOLE

San Bruno G&E-Line Rupture Investigation DR CPUC 213-Q03Atch01

1040

BAUT SEO Airport Extension

Redacted

Method: 4 7/8" diameter Rotary Wash with cathead

LOGGED BY: Redacted

CHECKED BY:

DRILL HOLE NO.: B-29

DRILLING DATE: May 25, 1994

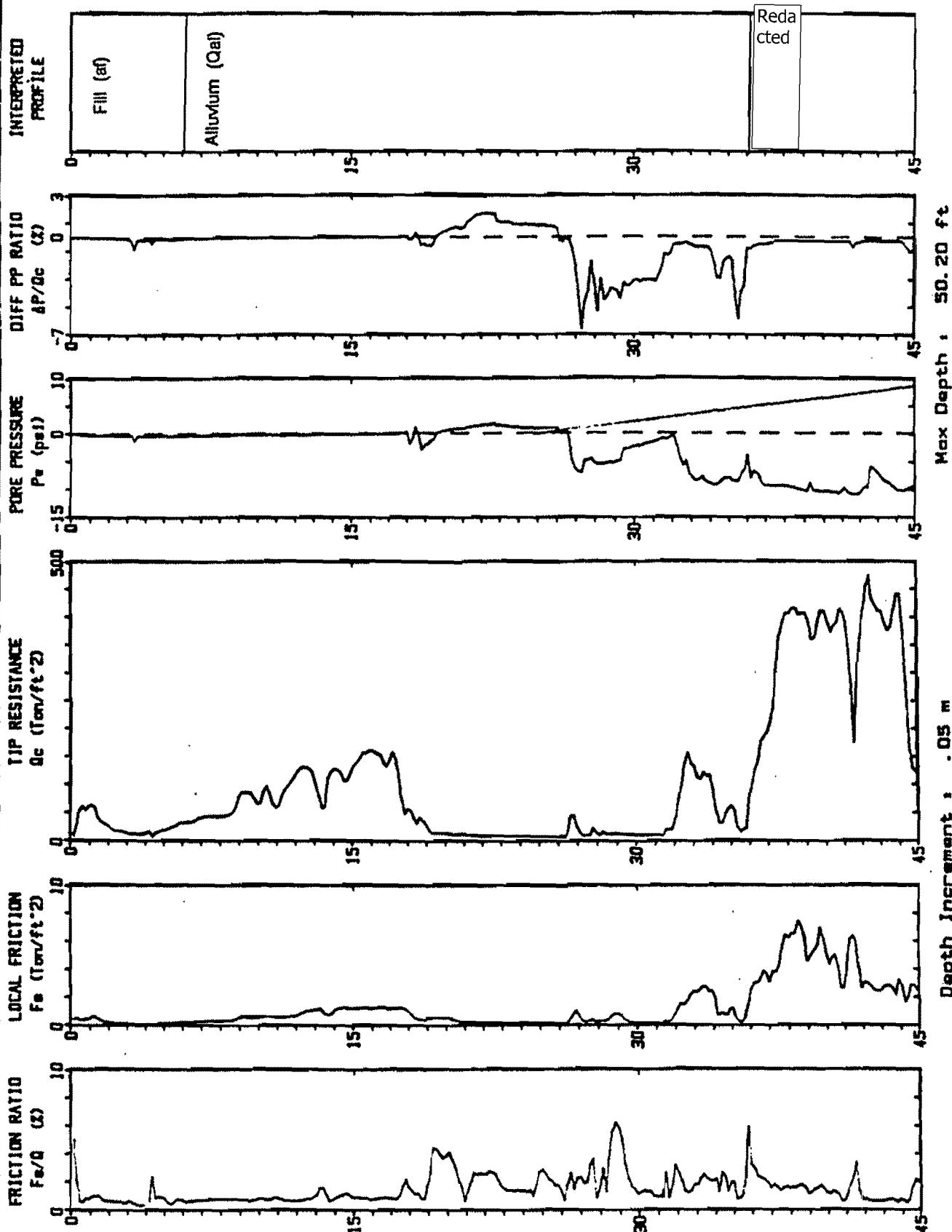
ELEVATION 3174 feet

DATUM: NGVD

V B I

Operator : Redacted

Location : C-37

CPT Date : 05-28-84 10:36
Cone Used : HD 322 TC -U2Sounding : 842139 Pg 1 / 2
Job No. : SF94011

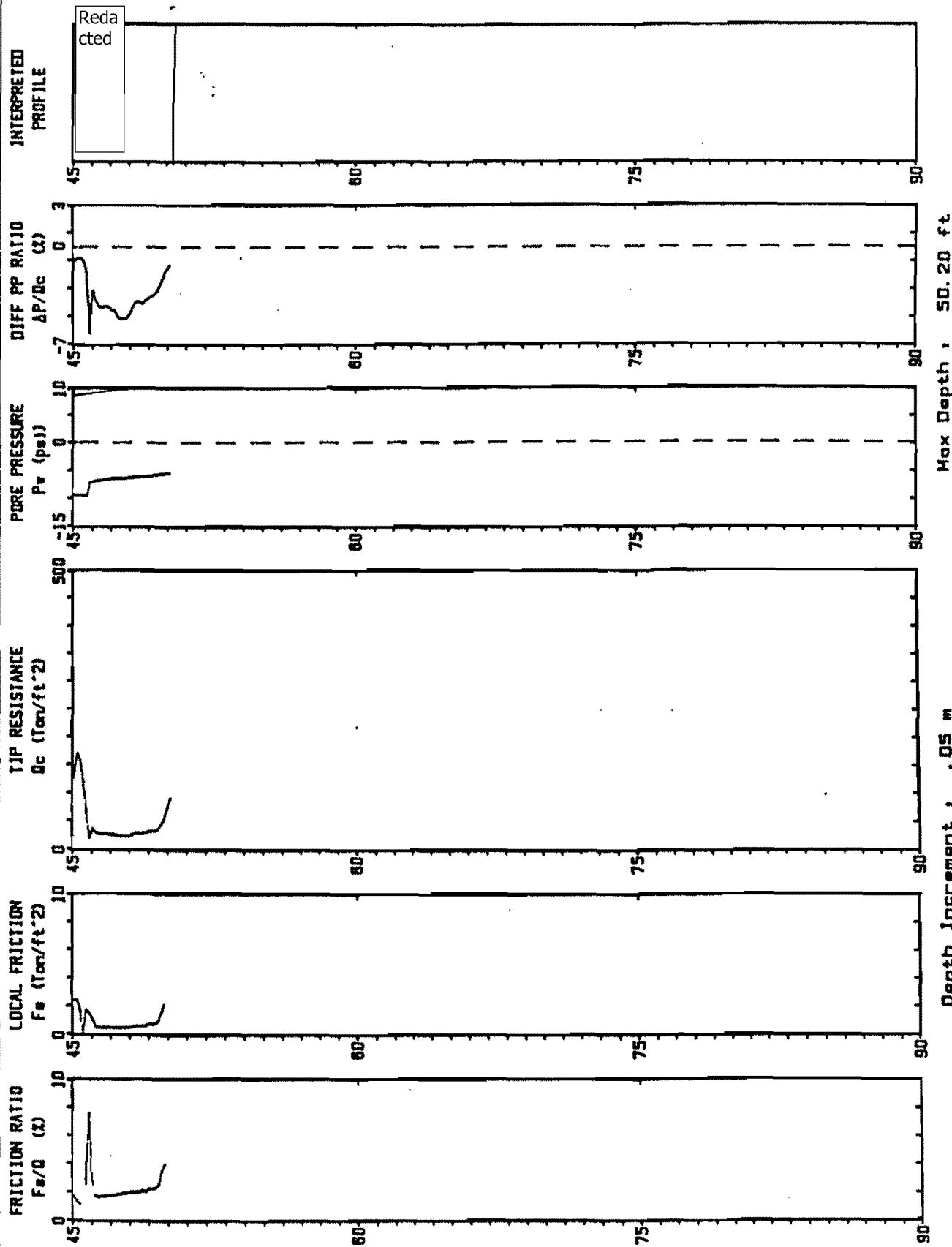
CPT-37

PLATE B-37

Operator : Redacted
 Location : C-37

CPT Date : 05-28-84 10,36
 Cone Used : HD 322 TC -U2

Sounding : 942139 Pg 2 / 2
 Job No. : SF94011



DEPTH (ft)

CPT-37 (Cont.)

PLATE B-37

LOG OF DRILL HOLE

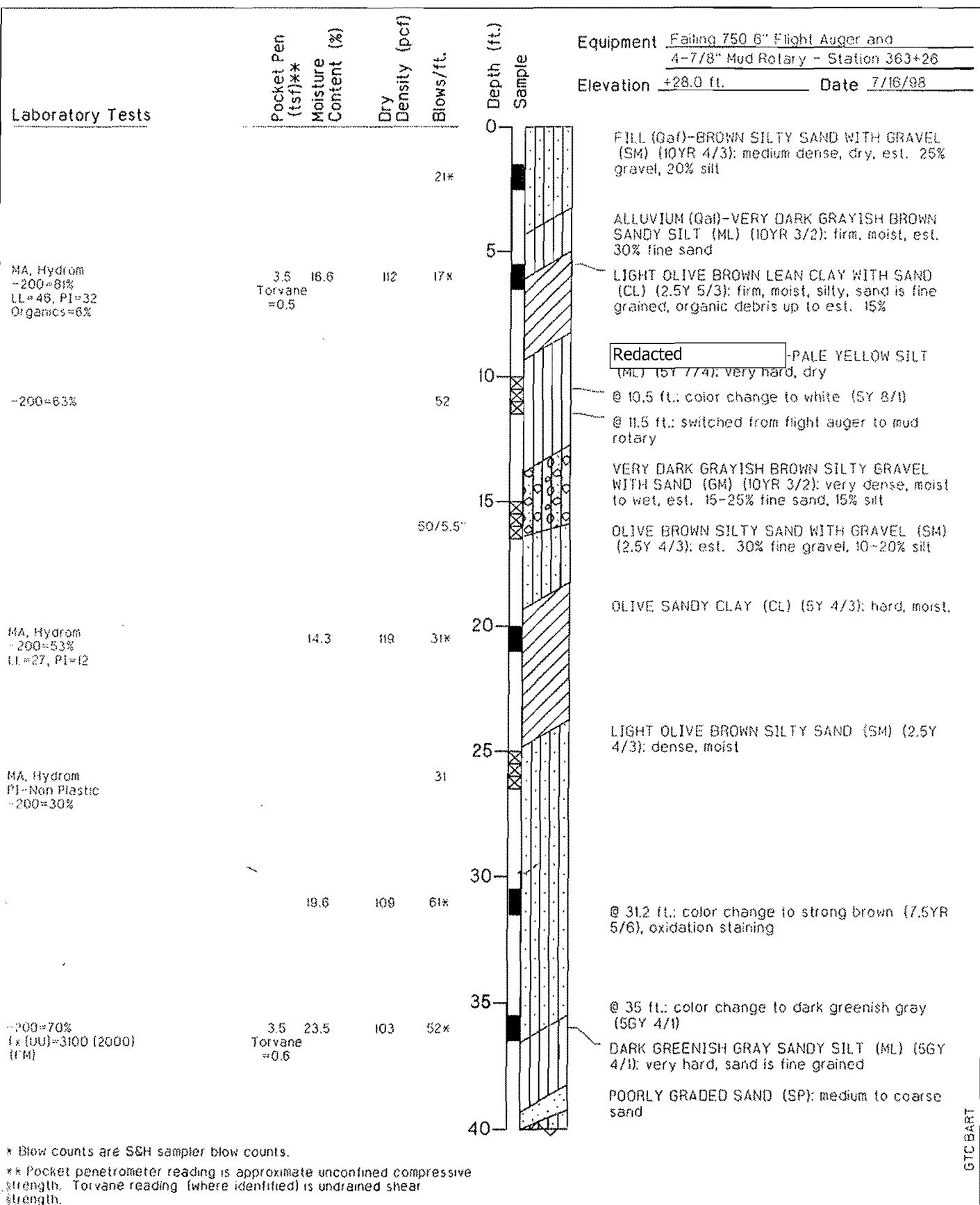
JOB NO.: SF94011
 PROJECT: BART SFO Airport Extension
 LOCATION: Redacted

DRILLING METHOD: 4 7/8" diameter Rotary Wash with cathead

LOGGED BY: Redacted
 CHECKED BY:

DRILL HOLE NO.: B-30
 DRILLING DATE: May 25, 1984
 ELEVATION: 27.48 feet
 DATUM: NGVD

DEPTH (FEET)	SAMPLE	BLOW COUNT	TORVANE SHEAR STRENGTH (PSF)	POCKET PENETROMETER COMP. STRENGTH (IPSF)	PHOTOVAC TIP READING (IPM)	GRAPHIC LOG	GEOTECHNICAL DESCRIPTION AND CLASSIFICATION		DRY DENSITY (PCF)	MOISTURE CONTENT (%)	ATTERBERG LIMITS		UNDEFINED SHEAR STRENGTH (PSF)	ADDITIONAL TESTS	
							LIMIT (%)	PLASTIC LIMIT (%)			LIMIT (%)	PLASTIC LIMIT (%)			
8							"ARTIFICIAL FILL (af)" SILTY SAND with gravel (SM) light brown, dry to damp, loose, roots, angular gravel to 1 1/2-inch diameter.								
16							5 feet: Treated wood timber, old railroad tie? Debris interfering with drilling to 13 feet.								
10							"ARTIFICIAL FILL (af)" LEAN CLAY (CL) brown, moist.								
32							"ALLUVIUM (Qal)" SILT (ML) marbled light brown and gray, damp to moist, dense, bands of fine grained sand.								
20		77					Redacted SILTY SAND (SM) brown, dry, very dense, pink-white mottling (carbonate veins), some fine gravel, weakly cemented.	115	10						
68							Marbled light gray-brown and orange-brown, moist, very fine sand, weakly cemented.								
30		30					Gray-brown, friable, moist to wet, dense, 30% fines.							GS	
44							Redacted SANDY SILT (ML) light blue-gray, moist, dense, with black and brown lenses, fine grained sand.								
54							Very dense, 53% fines.							GS	
27	2.5						Redacted LEAN CLAY (CL) dark brown, moist, very stiff, some silt and fine grained sand.	108	21					2730	
50		24					Redacted SILT (ML) light blue-gray, moist, medium dense. Bottom of drill hole at 51 1/2 feet. Backfilled hole with soil cuttings and grouted uppermost 5 feet.								



Figure

A-3

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Environmental Services

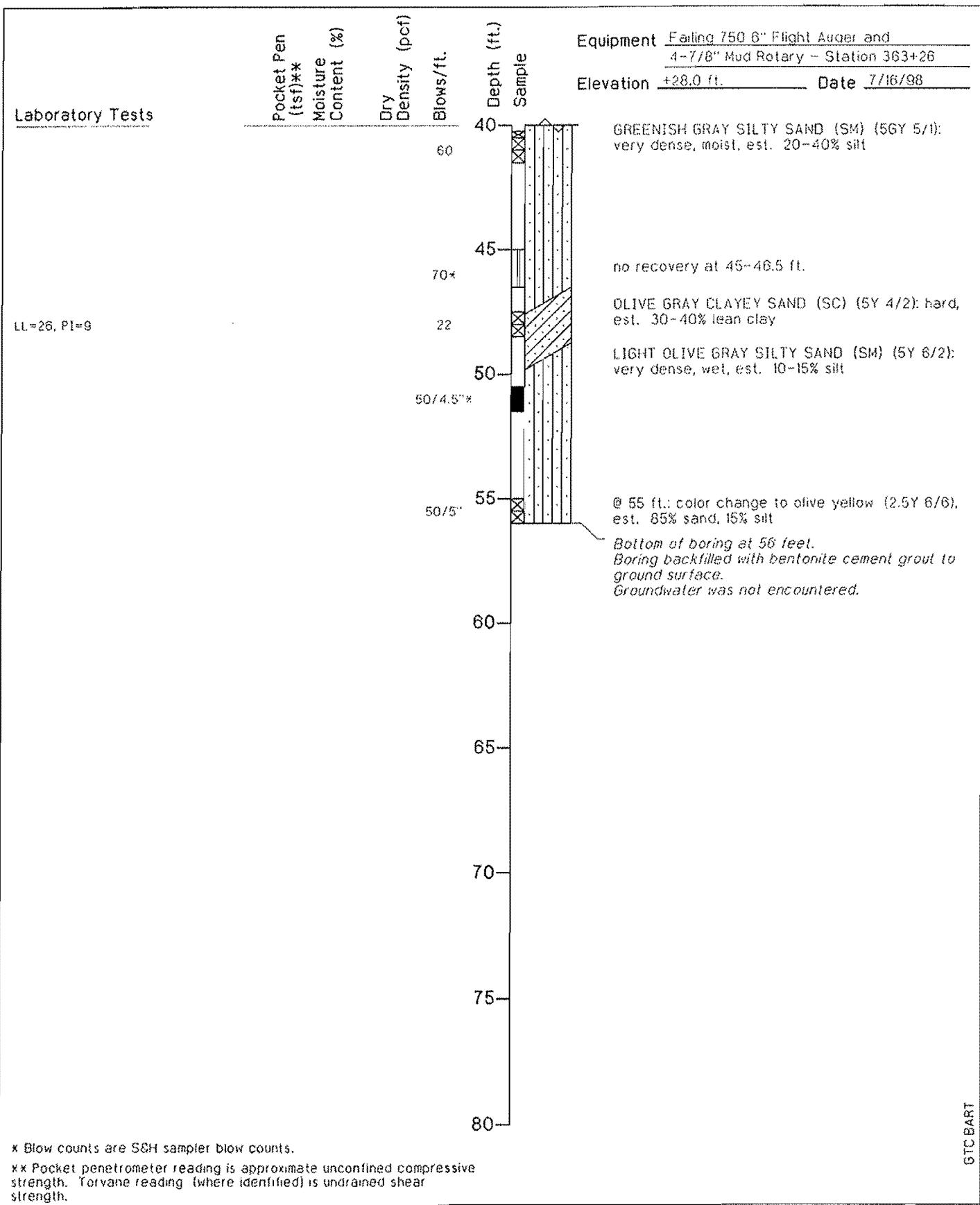
DRAWN JOB NUMBER
CEG 40646 4E

Log of Boring B-203
Module 2 - BART Extension to SFO
San Mateo County, California

APPROVED
Redacte

DATE
9/98

REVISED DATE



* Blow counts are S&H sampler blow counts.

** Pocket penetrometer reading is approximate unconfined compressive strength. Torsvane reading (where identified) is undrained shear strength.

GTC BART

Figure



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Engineering and
Environmental Services

DRAWN
CEGJOB NUMBER
40646 4E**Log of Boring B-203**

Module 2 - BART Extension to SFO
San Mateo County, California

APPROVED
RedactDATE
9/98

REVISED DATE

A-3

LOG OF DRILL HOLE

JOB NO.: SF94DII
 PROJECT: BART SFO Airport Extension
 LOCATION: Redacted
 DRILLING METHOD: 4 7/8" diameter Rotary Wash with cathead

LOGGED BY: Redacted

CHECKED BY: [Redacted]

DRILL HOLE NO.: B-3I
 DRILLING DATE: May 24, 1994
 ELEVATION: 24.40 feet
 DATUM: NGVD

DEPTH (FEET)	SAMPLE	BLOW COUNT	TORVANE SHEAR STRENGTH (PSF)	POCKET PENETROMETER COMP. STRENGTH (IPF)	PHOTOVAC TIP READING (IPM)	GRAPHIC LOG	GEOTECHNICAL DESCRIPTION AND CLASSIFICATION				ATTERBERG LIMITS	UNDEFINED SHEAR STRENGTH (PSF)	ADDITIONAL TESTS
							DRY DENSITY (PCF)	MOISTURE CONTENT (%)	LIMIT (%)	PLASTIC LIMIT (%)			
38		3.0				"ARTIFICIAL FILL (a1)" GRAVELLY SAND (SP) brown, dry to damp, medium dense. "ALLUVIUM (Gal)" SANDY CLAY (CL) brown, moist, stiff. 2 feet: Roots, some coarse gravel. Redacted LEAN CLAY (CL) light brown, moist to damp, very stiff, with red and black speckles. Redacted SANDY SILT (ML) light brown, damp, very dense, some orange mottled veins, 40% sand. Redacted SILTY SAND (SM) light brown, damp, very dense, layers of poorly and well graded sand in veins, orange to dark orange, 38% fines.	112	17	41	22	2780	C	GS
69												GS	
70												GS	
55												GS	
76 1/2"												DS	
57													
48													
58													
27													
81													

Bottom of drill hole at 51 1/2 feet.

Groundwater measured at 34 feet depth on 6/13/94.

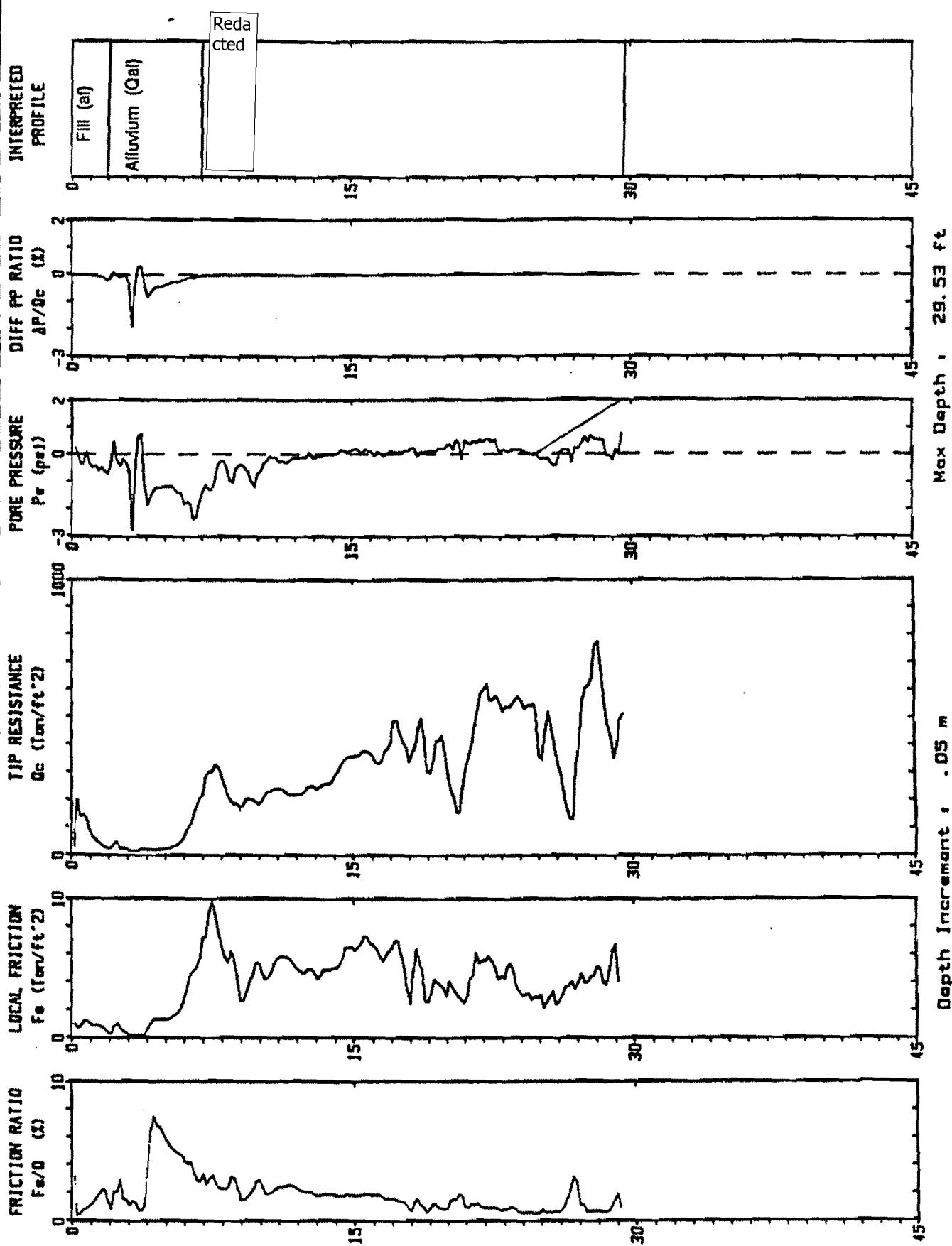
Piezometer installed END TO LOGS ON PLATE A-10

Operator : Redacted
Location : C-39

CPT Date : 05-26-84 09:22
Cone Used : HQ 322 TC -U2

Sounding : 942137 Pg 1 / 1
Job No. : SF94011

Redacted



DEPTH (feet)

CPT-39

Elevation: 24.37
Redacted

PLATE B-39

SB_GT&S_0037449

Operator : C-40
Location : Redacted

CPT Date : 05-26-94 12:17
Cone Used : HD 322 TC -U2
Sounding : 942140 Pg 1 / 1
Job No. : SF94011

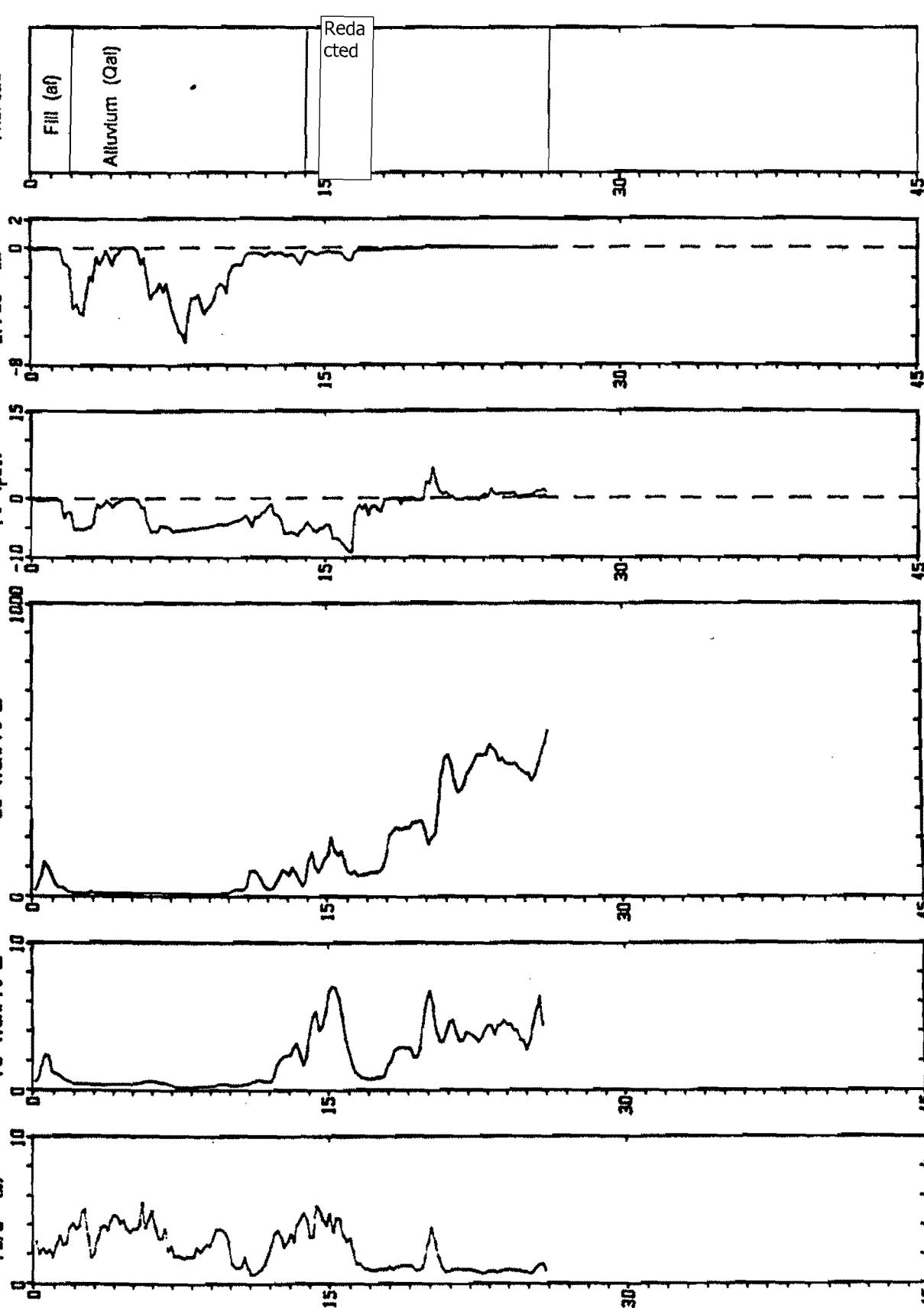
FRICION RATIO
 $F_s/f_s (x)$

TIP RESISTANCE
 $R_c (\text{ton}/\text{ft}^2)$

PURE PRESSURE
 $P_v (\text{psi})$

INTERPRETED
PROFILE

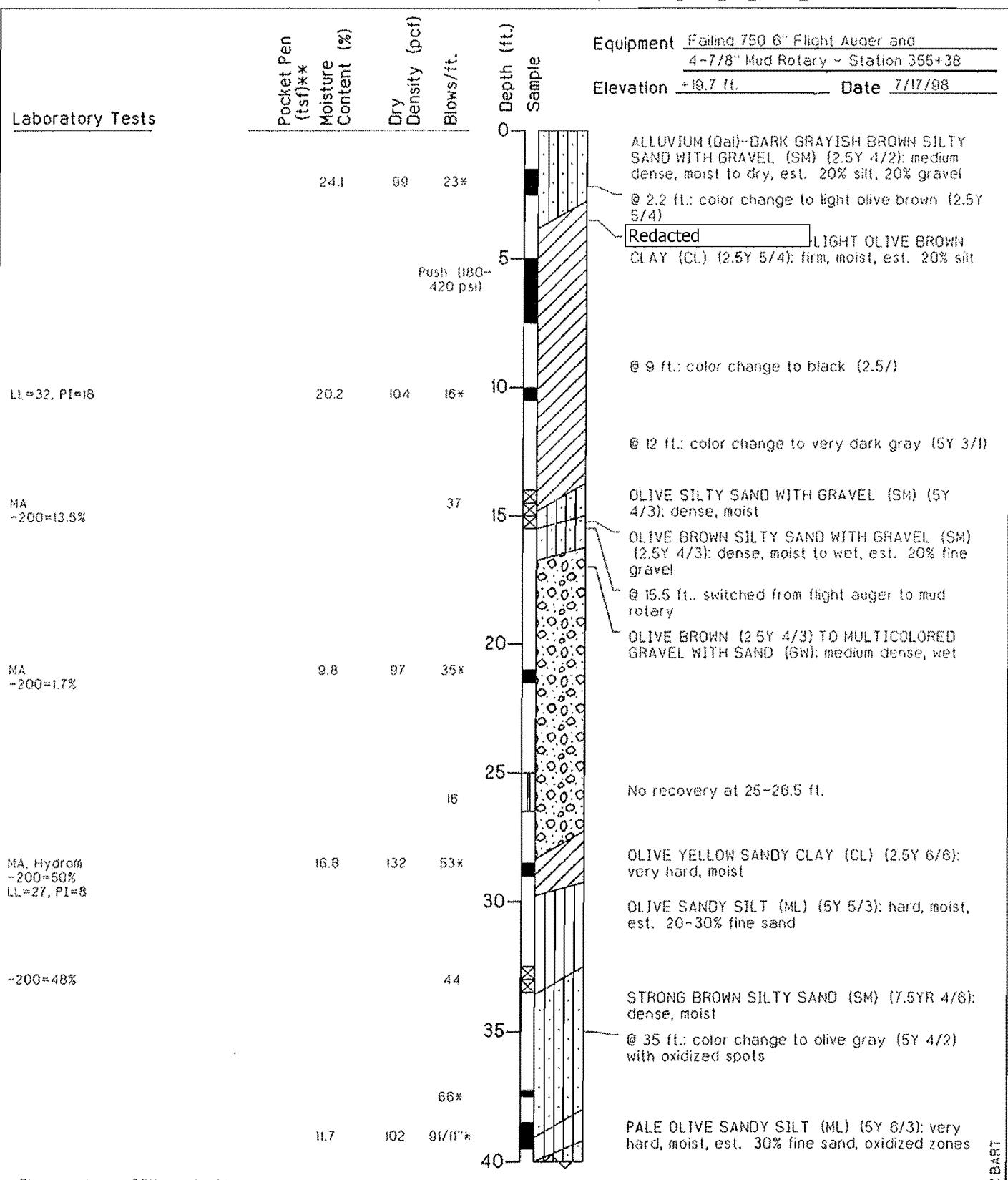
Redacted



(250) DEPTH (ft)

CPT-40

Elevation: 20.62
Redacted
PLATE B-40



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DRAWN JOB NUMBER
CEG 40646 4E

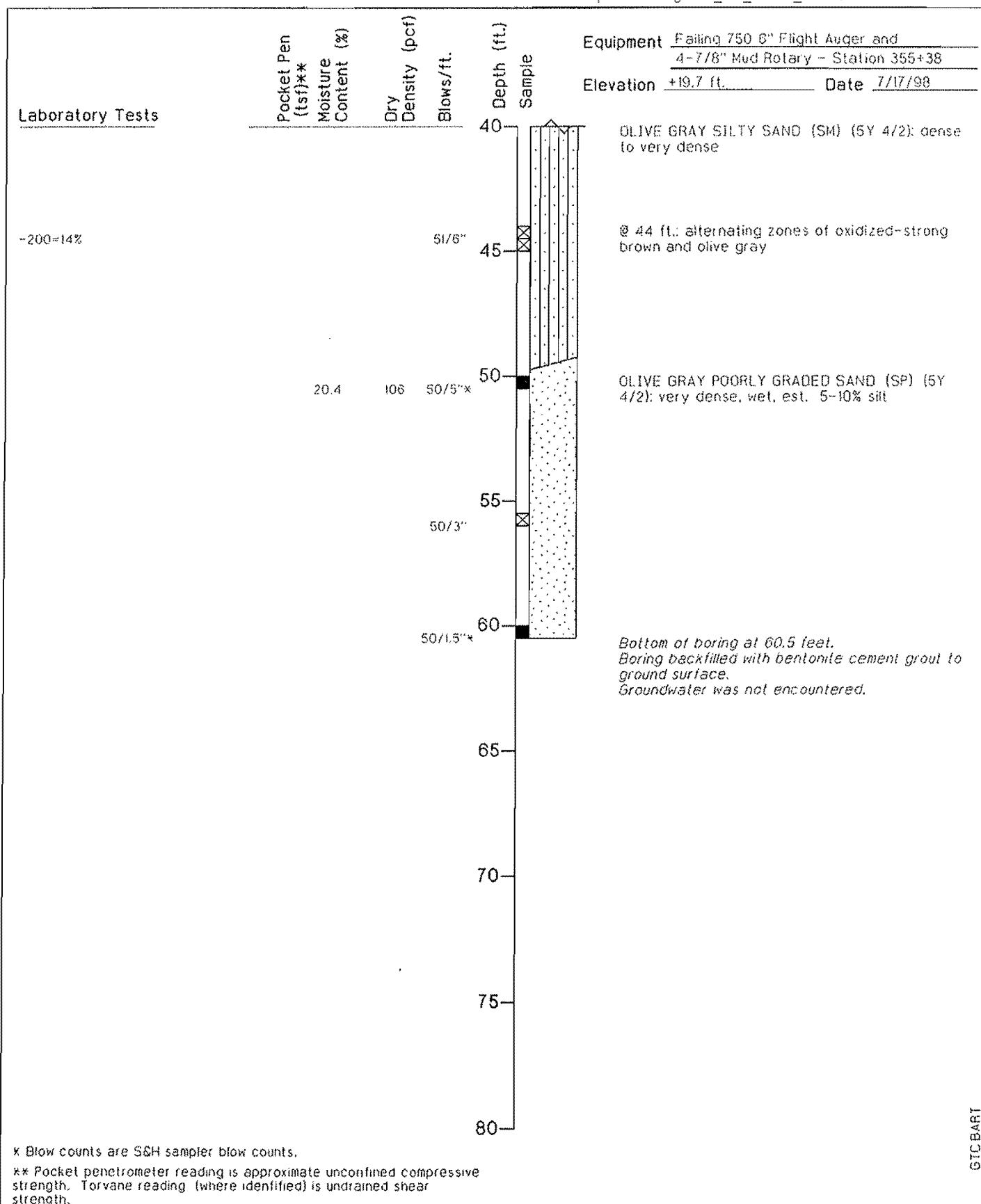
Log of Boring B-204
Module 2 - BART Extension to SFO
San Mateo County, California

APPROVED
Redacted

DATE
8/98

A-4

REVISED DATE



Figure



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DRAWN JOB NUMBER
CEG 40646 4E

Log of Boring B-204
Module 2 – BART Extension to SFO
San Mateo County, California

APPROVED
Redacted

DATE
8/98

REVISED DATE

A-4

LOG OF DRILL HOLE

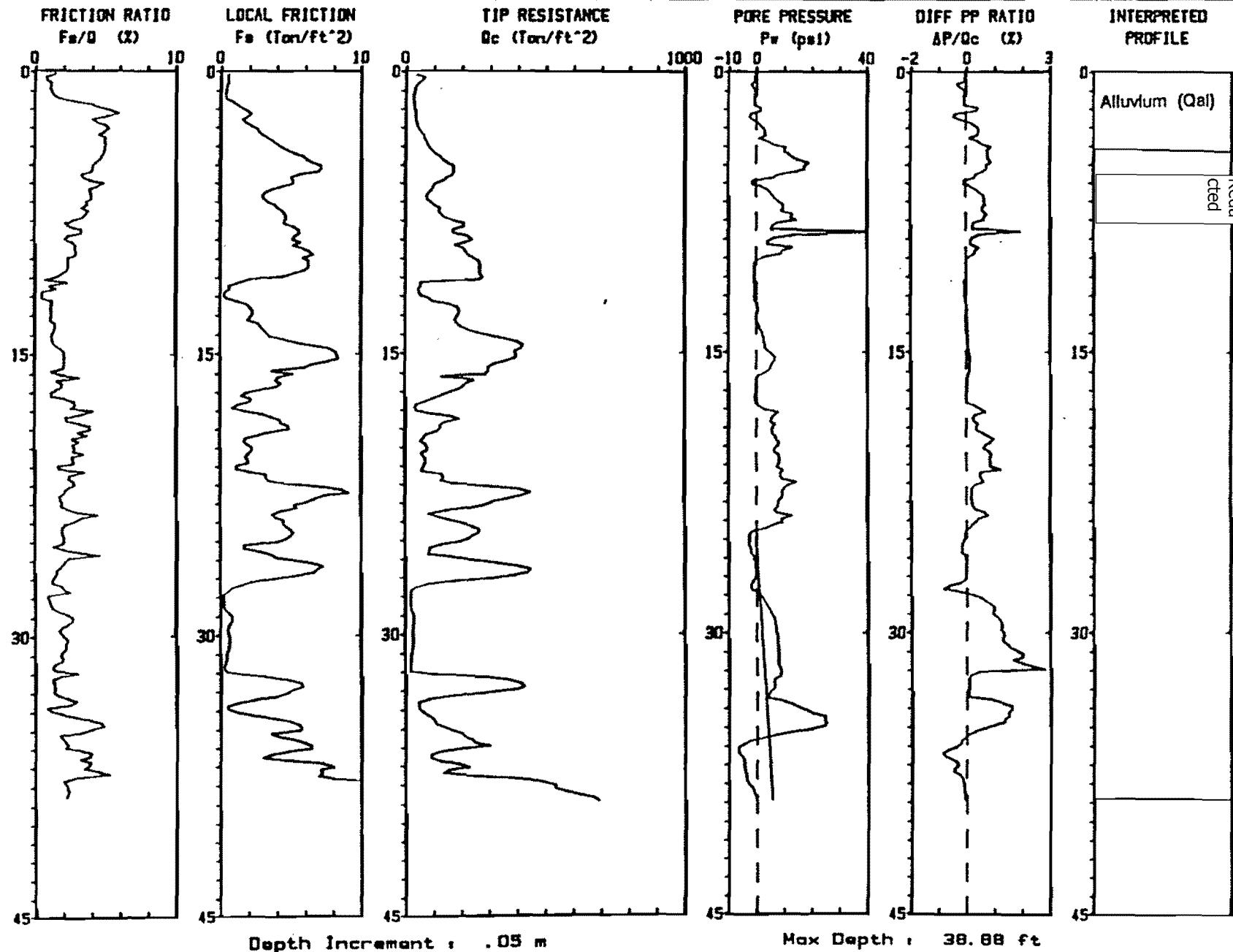
DD NO.: SF940II
 PROJECT: BART SFO Airport Extension
 LOCATION: Redacted
 DRILLING METHOD: 4 7/8" diameter Rotary Wash with cathead

LOGGED BY: Redacted
 CHECKED BY: _____

DRILL HOLE NO.: B-32
 DRILLING DATE: May 24, 1994
 ELEVATION: 32.99 feet
 DATUM: NGVD

DEPTH (FEET)	SAMPLE	BLOW COUNT	TORMEAN SHEAR STRENGTH (PSF)	POCKET PENETROMETER CORR. STRENGTH (TSF)	PHOTOVAC TIP READINGS (PPM)	GRAPHIC LOG	GEOTECHNICAL DESCRIPTION AND CLASSIFICATION		DRY DENSITY (PCF)	ATTERBERG LIMITS		UNCONFINED SHEAR STRENGTH (PSF)	ADDITIONAL TESTS
							LIQUID LIMIT (%)	PLASTIC LIMIT (%)		LIQUID LIMIT (%)	PLASTIC LIMIT (%)		
0							Redacted	LEAN CLAY (CL) light orange-brown, moist, hard, some sand.					
38							5 feet: 2-inch thick layer of orange mottling with medium grained sand.						
10		11					Redacted	SILT (ML) light brown with orange stains, moist, dense.					
20		20	1.5				9 feet: Fine to coarse grained sand with fine gravel in cuttings.						
20		57					10 feet: Medium dense, layers of sand (SP/SW) dark red-brown and orange, 1 to 3-inches thick.						
42							Redacted	LEAN CLAY with sand (CL) light brown, with orange bands and mottling, moist, stiff to very stiff, fine grained sand.					
42							Redacted	SILTY SAND (SM) light gray-brown, with light orange banding, moist to wet, very dense, fine grained sand.					
30		17					Redacted	SANDY SILT (ML) light gray-brown, moist to wet, dense, 52% fines.					
30		82					26 1/2 feet: Fine to medium grained sand.						GS
40		70					Redacted	SILTY SAND (SM) blue-gray, moist, medium dense, fine grained sand, some thin lean clay layers, 38% fines.					DS
40		32	3.5				Very dense.						DS
50		49					Light gray-brown with gray banding, fine grained sand, 13% fines.						GS
							Redacted	LEAN CLAY with sand (CL) light brown with light orange marbling, moist, very stiff, fine grained sand.					
							Redacted	SILTY SAND (SM) light brown to orange, moist, dense, fine grained sand.					
							Redacted	SILTY SAND/SANDY SILT (SM/ML) light brown, moist, dense, fine to coarse grained sand, 50% fines.					GS
							Bottom of drill hole at 51 1/2 feet. Backfilled hole with soil cuttings and grouted uppermost 5 feet.						

Operator : <input type="text"/> Redacted	CPT Date : 05-25-84 15:53	Sounding : 94Z136 Pg 1 / 1
Location : C-41	Cone Used : 347TC U2	Job No. : SF94011



CPT-41

PLATE B-41